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NASA TN D-4431

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LOW VARIABLE THRUST INTERPLANETARY TRAJECTORY DATA

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Cleveland, Ohio



NATIONAL AERONAUTICS AND SPACE ADMINISTRATION . WASHINGTON, D. C. . APRIL 968



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SUMMARY

The Newton-Raphson algorithm method is used to generate a large number of low-thrust trajectories between Earth and the other planets in the solar system. These paths assume the use of an ideal, variable-thrust rocket that operates at constant jet power. Trajectories include planet flyby, or capture from Earth, and Earth flyby from the other planets. In all cases, the heliocentric travel angle is varied between 30° and 330° for seven different trip times.

The data presented include the performance parameter $J = \int_0^T a^2 dt$ and all the initial values needed to recompute the path. Several terminal conditions, such as velocity components for the flyby cases, are also included.

Analytical techniques with numerical examples are presented which consider the application of the data to a variety of manned and unmanned missions and mission profiles.

INTRODUCTION

One of the major drawbacks to a detailed mission analysis of electrical propulsion systems is that optimal trajectory data for a wide range of different missions has been unavailable. Such optimal trajectories are needed because simplified thrust control such as tangential thrusting may cause a large increase in characteristic velocity increment ΔV over the optimal thrusting trajectory. The optimal ΔV values, however, are only about 30 percent above the high-thrust values. Even if high-thrust ΔV values are used directly, all such data which are readily available are not minimized with respect to the number and placement of impulses. Reference 1, for example, shows some three-impulse transfers which reduce ΔV for Earth-Mars round trips.

While it would be more realistic to present only constant thrust or at least constant acceleration data, the problem of generating, let alone presenting, such a volume of data for all the planets, travel times, and travel angles of possible interest is presently dis-

couraging. This leaves only the variable-thrust case as a likely candidate for data presentation of such a broad scope. Unfortunately, even optimal variable-thrust trajectories can be very difficult to obtain numerically, and the large number needed for a complete mission survey can require an excessive amount of computer time. However, recent improvements in the solution methods for variable-thrust trajectories have made it possible to generate large volumes of such solutions for a relatively small amount of computer time (about 10 sec of IBM 7094 time per solution). The details of this method, known most recently as the Generalized Newton-Raphson Operator Algorithm, can be found in reference 2. This report will present only the operational experiences gained with this method during the generation of the data presented herein.

Current interest in the hybrid high- and low-thrust propulsion systems (e.g., see refs. 3 to 5), unfortunately, introduces two more parameters into each calculation: the initial and final values of the hyperbolic excess velocity (velocity at sphere of influence). The presentation of sufficient data for all the planets including a range of values for the two hyperbolic velocities is also prohibitive because of computer time and volume of data that must be presented.

In this report, the hyperbolic velocity problem is overcome by computing two-dimensional planet capture probes, planet flyby probes, and Earth flyby probes. Performance numbers for other values of hyperbolic velocities are then estimated by interpolation. The data are presented for all planets in the form of sets. Each set consist of the results for seven travel times and 11 polar travel angles. The polar travel angle is the heliocentric angle subtended in the given travel time.

For the capture mission, it is necessary that the vehicle match the direction and magnitude of the heliocentric velocity of the planet. The flyby heliocentric trajectory requires only that the vehicle encounter the target planet with no specific restriction on the approach velocity.

All the planets are assumed to move about the Sun in coplanar circular orbits at their mean distance from the Sun.

In order to assist the reader in using the data, a variety of mathematical conditions for optimal relations between the planetary and heliocentric parts of one-way and round-trip missions are presented. These conditions are intended to help the user solve such problems as choosing the best Earth escape and interplanetary paths for one-way trips or the best outbound and return legs of a round trip. Numerical examples which illustrate the use of the mathematical conditions are also presented.

Although none of the preferred constant thrust data are presented, it is possible to make rather good estimates of such performance numbers from the variable thrust results using the method of reference 6. If the propellant fractions obtained directly by this method are not accurate enough - although they should be more than adequate for preliminary design purposes - then the method can be used to compute excellent first

estimates for trajectory starting conditions for the numerical solution of an optimum constant-thrust trajectory.

The data, which are presented in tabular form, consist of the starting conditions needed to reproduce the trajectories and the pertinent performance numbers for the various flights. These data are available on cards upon request from Mr. MacKay, who is now at the Ames Research Center.

SYMBOLS

acceleration, m/sec² a energy to mass ratio, m^2/sec^2 \mathbf{E} thrust, N \mathbf{F} transversality function, $\sqrt{2\dot{a}_H(T)} \cdot [\overline{V}(T) - \overline{V}_E]$ G Earth surface gravity, 9.80665 m/sec² g I specific impulse, sec performance parameter, $\int_0^T a^2 dt$, m^2/sec^3 J K mass ratio across planetary phase, m_5/m_2 k m_4/m_3 mass, kg m \mathbf{P} power, kW_e \mathbf{R} distance from Sun, m radius, m \mathbf{r} \mathbf{T} terminal time or a time interval, sec or days t time, sec velocity, m/sec \mathbf{v} ΔV characteristic velocity increment, m/sec Cartesian coordinates x, y general state variable \mathbf{z} specific electric powerplant mass, kg/kW α

β angle between vectors $\overline{\Delta V}_H$ and \overline{V}_E , rad γ Lagrange multiplier λ gravitational constant, m^3/sec^2 thrust angle relative to the x-axis, rad polar travel angle, rad or deg Subscripts: atmospheric entry a circular orbital C \mathbf{E} Earth engine eng H heliocentric \mathbf{L} payload mission m P propellant planet р pp powerplant structure S wait phase w in the x and y directions x, y

ANALYSIS

The results presented in this report were obtained by an analysis based on a two-body inverse square force field model of two dimensions; they present a fairly accurate estimate of the upper limit of the payload capabilities of advanced propulsion vehicles. In missions utilizing variable low-thrust power-limited propulsion systems, the criterion of merit of the resulting trajectory is its value of $J = \int_0^T a^2 \, dt$. This quantity is analogous to the concept of characteristic velocity of chemical rockets, and it is an index of

the propellant requirement for the particular mission (ref. 7).

Variational Problem

The minimization of $\int_0^T a^2 dt$ for a specified mission is a calculus of variations problem in which this integral is minimized subject to certain constraints, that is, the equations of motion and the specified kinematic conditions of the vehicle to be satisfied at the initial and terminal points of the trajectory.

The equations of motion of the vehicle are:

$$\ddot{z}_i + \frac{\mu z_i}{R^3} = a_i$$
 $i = 1, 2$ (1)

where

$$\frac{d^2z}{dt^2} = \ddot{z}$$

$$R^2 = z_1^2 + z_2^2 = x^2 + y^2$$

 μ is the gravitational constant, and a_i is the acceleration component due to thrust. The minimization of $\int_0^T a^2 dt$ subject to the constraints represented by equation (1) necessitates the formation of the functional

$$J = \int_{0}^{T} \left[\sum_{i=1}^{2} a_{i}^{2} + \sum_{i=1}^{2} \lambda_{i} \left(\ddot{z}_{i} + \frac{\mu z_{i}}{R^{3}} - a_{i} \right) \right] dt$$

$$= \int_{0}^{T} f(a_{i}, z_{i}, \ddot{z}_{i}) dt$$
(2)

Euler's equations become

$$\frac{\partial f}{\partial z_i} - \frac{d}{dt} \left(\frac{\partial f}{\partial \dot{z}_i} \right) + \frac{d^2}{dt^2} \left(\frac{\partial f}{\partial \ddot{z}_i} \right) = 0$$
 (3)

From equation (2),

$$\frac{\partial f}{\partial a_i} = 0 = 2a_i - \lambda_i + 2a_i = \lambda_i$$

$$\frac{\partial f}{\partial z_i} = \lambda_i \frac{\mu}{R^3} - z_i \frac{3\mu}{R^5} \sum_{j=1}^2 2a_j z_j$$

$$\frac{\partial f}{\partial \ddot{z}_{i}} = \lambda_{i} \rightarrow \frac{d^{2}}{dt^{2}} \frac{\partial f}{\partial \ddot{z}_{i}} = 2\ddot{a}_{i}$$

Substituting into equation (3), yields

$$\ddot{a}_{i} + \frac{\mu a_{i}}{R^{3}} - z_{i} \sum_{i=1}^{2} \frac{3\mu}{R^{5}} a_{j} z_{j} = 0 \qquad i = 1, 2$$
(4)

Hence, the added set of differential equations (4) must be solved with equation (1) between the desired initial and terminal states of the trajectory.

Solution Method

Since an analytical solution to the previously defined nonlinear two-point boundary value problem does not exist, numerical integration methods must be utilized. The usual method of solving the two-point boundary value problem has been to guess the unknown boundary values at the initial point and to numerically integrate to the terminal point of the trajectory. Almost certainly, the required terminal conditions will not be met, so corrections must be made on the guessed values of the unknown initial conditions and a new solution obtained. Iterative guessing techniques should be employed until the complete set of initial point variables and the required thrust-control program necessary to meet the specified terminal conditions are determined. When this method is applied to a nonlinear system of equations, a solution is often difficult to obtain.

A completely different method has been developed to solve the nonlinear two-point boundary value problem. This method, an application of the Generalized Newton-Raphson Operator, was first suggested by R. Bellman (ref. 8). The method departs from the usual method of successively correcting unknown initial boundary conditions until the terminal conditions are satisfied. Instead, the system of nonlinear differential equations is first linearized by the Generalized Newton-Raphson Operator and then the linearized system of equations is solved. Under appropriate conditions, the linearized system of equations converges quadratically to the solution of the original nonlinear system of equations. In using this method, the given initial and terminal boundary conditions are satisfied at all times and a sequence of solutions is generated which converges rapidly to the solution of the original set of nonlinear equations. The solution of the linear problem can be obtained either by a finite difference approximation or by integrating the equations with any high-order method. Both methods were used to obtain solutions so that relative speed and accuracy could be evaluated. The linearized equations were first solved by using a fourth order Runge-Kutta integration scheme. Also, the linearized equations were solved by finite differences. Solutions obtained by the two methods were compared for a random sample of similar cases. The comparison showed an agreement of within 0.5 percent. Hence, we decided to use only the finite difference approach in obtaining the desired solutions, because this method of solution was about three times as fast as the integration using a fourth order Runge-Kutta scheme.

To determine how closely the solutions of the linearized equations agreed with the desired solutions, 60 trajectories (as presented in ref. 7) were solved by the finite difference code. Both capture and flyby trajectories were obtained and the values of J were compared with the values presented in reference 8. The average disagreement was less than 0.5 percent and the maximum disagreement was approximately 1 percent. In this same reference, there are a few trajectories, presented in tabular form, for which no value of J was obtained. Using the Generalized Newton-Raphson Operator method, solutions to these trajectories were obtained without any difficulty.

Trajectory and Mission Types

The two types of missions for which data are presented in this report are capture and flyby missions. For the capture mission, the vehicle must match the direction and magnitude of the heliocentric velocity of the target planet. The flyby heliocentric trajectory requires only that the vehicle encounter the target planet with no specific restriction on the approach velocity. Optimum performance for this mission is achieved by having a trajectory with $a_{\mathbf{x}}(T) = a_{\mathbf{y}}(T) = 0$.

Because the terminal velocity is not specified for the flyby mission, the thrust pro-

gram is usually simpler and has a lower propellant requirement than for the corresponding capture mission. For the data presented in this report, all the planets are assumed to move about the Sun in coplanar circular orbits at their mean distance from the Sun.

The data presented in this report have been selected with a view toward the analysis of a variety of different mission profiles or modes. To begin with, the presentation of nonoptimum polar angles (in the sense of minimum J) for the various transfer times is essential to the composition of either minimum J or maximum payload round trips. The best polar angle cases, which are of interest for probe type missions, are also in the range covered. Secondly, the planetary flyby cases (also presented for optimum and non-optimum polar angles) are of interest as cases representing the unlimited use of atmospheric braking at either planet or Earth arrival.

Following the pattern set by reference 8, many other trajectory parameters such as the initial and final values of the adjoint variables (which, in the special case of variable thrust, are proportional to the thrust acceleration components) have also been included for all cases. It will be the purpose of this section to show how these data may be used to estimate optimal trajectories for several different mission modes.

All electric case. - The traditional mission mode for electric propulsion systems is the one in which the electric thrustor is used exclusively for all the propulsive phases of the mission (fig. 1). One of the basic problems in this profile is the combination of the heliocentric and planetocentric paths such that the total value of J is minimized for total time used; for example, consider the mission trajectory between t_0 and t_2 .

The problem is to minimize the expression

$$J_{\rm m} = J_{0.1} + J_{1.2} \tag{5}$$

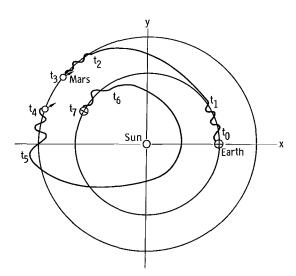


Figure 1. - Typical mission profile.

with respect to the time t_1 , while maintaining a constant total mission time $T_m = t_2 - t_0$ (fig. 1). Differentiating equation (5) with respect to t_1 ,

$$dJ_{m} = \left(\frac{\partial J_{0,1}}{\partial t_{1}} + \frac{\partial J_{1,2}}{\partial t_{1}}\right)dt_{1}$$

Therefore, the optimum combination must have

$$\frac{\partial J_{0,1}}{\partial t_1} = -\frac{\partial J_{1,2}}{\partial t_1}$$

In reference 9, it was shown that

$$\frac{\partial J_{1,2}}{\partial t_{1}} = +a_{H}^{2}(t_{1})$$

$$\frac{\partial J_{1,2}}{\partial t_{2}} = -a_{H}^{2}(t_{2})$$
(6)

where $J_{1,\,2}$ is the value of J for the heliocentric path. These equations are deduced from the fact that the adjoint variables are also sensitivity coefficients expressing the rate of change of $J_{1,\,2}$ with respect to the initial and terminal state variables (i.e., position and velocity components). Thus, knowledge of similar sensitivity coefficient for the Earth departure path will allow a solution for that escape path which gives

$$\frac{\partial J_0, 1}{\partial t_1} = -a_H^2(t_1) \tag{7}$$

A more detailed expression for $\partial J_{1,\,0}/\partial t_1$ will now be developed. Relations (6) were derived from an examination of the transversality condition of the heliocentric flight using the planetary orbits about the Sun as boundary conditions. For the electric escape path, it is common to use escape energy (relative to the planetary field) as a terminal condition to be achieved in the best way possible in a given time. The transversality relation for this kind of problem is

$$dJ_{0, 1} = \left[\left(a^2 - \sum_{i=1}^4 \lambda_i \dot{z}_i \right) dt + \sum_{i=1}^9 \lambda_i dz_i \right]_{t=t_1}$$
 (8)

subject to the terminal condition that the energy, relative to Earth, be equal to the escape energy; that is,

$$E = 0 = \frac{(\dot{x})^2 + (\dot{y})^2}{2} - \frac{\mu}{r}$$
 (9)

where

$$r = \sqrt{x^2 + y^2}$$
, $z_i = x$, y, \dot{x} , \dot{y}

and the coordinates are measured relative to Earth. Differentiating equation (9) yields

$$0 = \dot{x} \, d\dot{x} + \dot{y} \, d\dot{y} + \frac{\mu}{r^2} \, \frac{x \, dx}{r} + \frac{\mu}{r^2} \, \frac{y \, dy}{r}$$
 (10)

Using equations (10) in (8) to eliminate dx yields

$$dJ_{0,1} = \left[\left(a^2 - \sum_{i=1}^4 \lambda_i \dot{z}_i \right) dt + \left(\lambda_2 - \lambda_1 \frac{\dot{y}}{\dot{x}} \right) d\dot{y} + \left(\lambda_3 - \frac{\lambda}{\dot{x}} \frac{\mu}{r^2} \frac{x}{r} \right) dx + \left(\lambda_4 - \frac{\lambda_1}{\dot{x}} \frac{\mu}{r^2} \frac{y}{r} \right) dy \right]_{t=t_1}$$

For arbitrary changes in dy, dx, and dy,

$$\lambda_2 \dot{x} = \lambda_1 \dot{y}$$

$$\lambda_3 \dot{x} = \lambda_1 \frac{\mu}{r^3} x$$

$$\lambda_4 \dot{x} = \lambda_1 \frac{\mu}{r^3} y$$

Also,

$$\lambda_4 \dot{y} = \lambda_2 \frac{\mu}{r^3} y$$

Thus, $dJ_{0,1}$ becomes

$$dJ_{0, 1} = \left[\left(a^{2} - \lambda_{1}\ddot{x} - \lambda_{2}\ddot{y} - \lambda_{1} \frac{\mu}{r^{3}} x - \lambda_{2} \frac{\mu}{r^{3}} y \right) dt \right]_{t=t_{1}}$$

However, from the variational problem,

$$\ddot{\mathbf{x}} = -\frac{\mu_{\mathbf{x}}}{\mathbf{r}^3} + \mathbf{a}_{\mathbf{x}}$$

$$\ddot{y} = -\frac{\mu_y}{r^3} + a_y$$

$$\lambda_1 = 2a_x$$

$$\lambda_2 = 2a_y$$

$$\lambda_3 = -\dot{\lambda}_1$$

and

$$\lambda_4 = -\dot{\lambda}_2$$

Thus,

$$dJ_{0,1} = \left\{ a^2 - 2a_x \left(-\frac{\mu_x}{r^3} + a_x \right) - 2a_y \left(a_y - \frac{\mu}{r^3} y \right) - 2a_x \frac{\mu_x}{r^3} - 2a_y \frac{\mu}{r^3} y \right\}_{t=t_1}$$

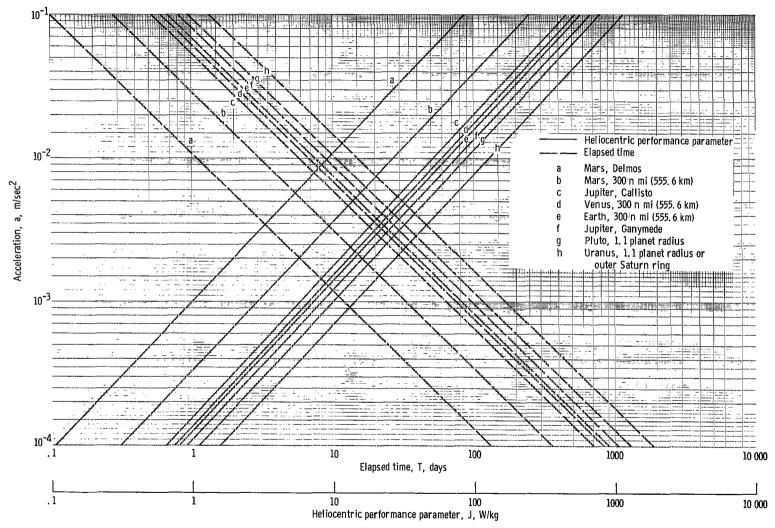


Figure 2. - Elapsed time, heliocentric performance parameter, and acceleration for planetocentric escape spiral trajectories with variable thrust or constant tangential thrust.

or

$$dJ_{0,1} = -a^2(t_1)dt_1$$

Referring back to equation (7) shows that $a_H(t_1)$ and $a(t_1)$ should be equal for minimum total $J_{0,2}$.

In practice, optimal escape paths (minimum $J_{0,1}$) are closely approximated by paths using tangentially directed, constant acceleration. It is therefore possible to find both $T_{0,1}$ and $J_{0,1}$ for any $a(t)=a_{H,1}(t_1)$. The time $T_{0,1}$, however, is a dependent variable and must be added to $T_{1,2}$ to compute the total transfer time. A similar procedure also applies at planet arrival time using $a_H(t_2)$ instead of $a_H(t_1)$ to compute the capture spiral time. Figure 2 shows escape or capture times and J values as functions of a.

The next problem is to take these optimal one-way trips, including their associated spirals, and join two of them together to form either a minimal J or maximum terminal mass round trip. The distinction between these two cases is needed only when some mass is left at the planet. Since a variable thrust escape or capture spiral can be approximated by one using a constant acceleration, it can be shown from further study of equation (8) that

$$\frac{dJ_{0,1}}{dt_{0}} = -\frac{dJ_{0,1}}{dt_{1}} = a^{2}(t_{0}) = a^{2}(t_{1})$$
(11)

If the mission and wait times are held constant.

$$T_{m} = t_{7} - t_{0}$$

$$dT_{m} = dt_{7} - dt_{0} = 0$$

$$T_{w} = t_{4} - t_{3}$$

$$dT_{w} = 0 = dt_{4} - dt_{3}$$
(12)

and the expression for the total change in the mission $\, {\bf J}_m^{} \,$ becomes

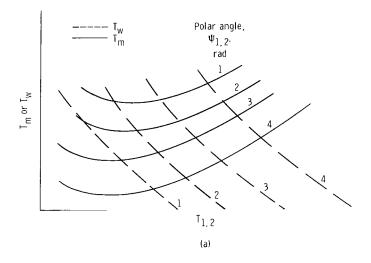
$$dJ_{m} = \left(\frac{\partial J_{6,7}}{\partial t_{7}} + \frac{\partial J_{0,1}}{\partial t_{0}}\right)dt_{0} + \left(\frac{\partial J_{2,3}}{\partial t_{3}} + \frac{\partial J_{4,5}}{\partial t_{4}}\right)dt_{3}$$

Using equations (12) and (11), this equation becomes

$$dJ_{m} = \left[a^{2}(t_{7}) - a^{2}(t_{0})\right]dt_{0} + \left[a^{2}(t_{3}) - a^{2}(t_{4})\right]dt_{3}$$
(13)

For the optimal round trip, $\mathrm{dJ}_{m}=0$ and the accelerations must carry across the wait phase and be equal at the start and end of the trip. This is the same result derived in reference 9 for the case of no planetary spirals.

Minimum J_m round trips can therefore be constructed by choosing any heliocentric trip time and polar angle and determining, through the associated initial and final heliocentric acceleration levels, a total mission time and wait time for which that heliocentric trip is optimal. Since mission and wait times are dependent variables, it is helpful to make a plot such as sketch (a) which relates mission and wait time to outbound trip time and angle.



Introduction of atmospheric braking. - The profile just discussed assumed that the vehicle spiraled down into a low terminal Earth orbit at the end of the mission. To reach the surface from this state would require that the vehicle (or some part of it) be capable of atmospheric braking from approximately circular velocity, such as was done in Project Mercury. In order to simulate atmospheric entry from escape speed, the last spiral may be omitted. No other modifications need be made to the previous procedure in this case.

If entry speeds above escape are considered, a new examination of how a terminal time change affects the mission J must be made. Since different entry speeds have an effect only on $J_{5,6}$ and also since there is no last spiral in this case, the term $\partial J_{5,6}/\partial t_6$ must be examined. As suggested by equation (13), only the very first and last

points on the round trip path need be considered, because an advance in Earth departure date t_0 must be accompanied by an equal advance in Earth arrival date t_7 (t_6 in this case) if mission time is to be constant.

As a pertinent example, consider the flyby case at Earth return. For changes in the Earth arrival date, the transversality relation of the basic variational problem gives

$$dJ_{5,6} = \left[\left(a^2 - \sum_{i=1}^4 \lambda_i \dot{z}_i \right) dt + \sum_{i=1}^4 \lambda_i dz_i \right]_{t=t_6}$$
 (14)

where the \dot{z}_i 's are derivatives taken along the path of the vehicle and the dz_i 's are taken along the path of the Earth. Thus,

$$dx_i = \dot{z}_E dt$$

and

$$dJ_{5,6} = \left(a^2 - \sum_{i=1}^4 \lambda_i z_i + \sum_{i=1}^4 \lambda_i z_{i,E}\right)_{t=t_6} dt_6$$

Because the boundary value problem requires only that the position of the planet be met,

$$dJ_{5, 6} = \left[a^{2} + \lambda_{1}\left(\frac{\mu_{x}}{R^{3}} - \frac{\mu_{x_{E}}}{R_{E}^{3}} - a_{x}\right) + \lambda_{2}\left(\frac{\mu_{y}}{R^{3}} - \frac{\mu_{y_{E}}}{R_{E}^{3}} - a_{y}\right) + \lambda_{3}(\dot{x}_{E} - \dot{x}) + \lambda_{4}(\dot{y}_{E} - \dot{y})\right]_{t=t_{6}} dt_{6}$$

$$\frac{dJ_{5,6}}{dt_{6}} = \left[a^{2} - \lambda_{1}a_{x} - \lambda_{2}a_{y} + \lambda_{3}(\dot{x}_{E} - \dot{x}) + \lambda_{4}(\dot{y}_{E} - \dot{y})\right]_{t=t_{6}}$$

Also, since

$$\lambda_1 = 2a_x$$

$$\lambda_2 = 2a_y$$

$$\lambda_3 = -\dot{\lambda}_1$$

$$\lambda_4 = -\lambda_2$$

the equations become

$$\frac{dJ_{5,6}}{dt_{6}} = \left[a^{2} - 2a^{2} - 2\dot{a}_{x}(\dot{x}_{E} - \dot{x}) - 2\dot{a}_{y}(\dot{y}_{E} - \dot{y})\right]_{t=t_{6}}$$

and

$$\frac{dJ_{5,6}}{dt_{6}} = -a^{2} - 2\left[\dot{a}_{x}(\dot{x}_{E} - \dot{x}) + \dot{a}_{y}(\dot{y}_{E} - \dot{y})\right]_{t=t_{6}}$$
(15)

Finally, since the flyby case requires $a_x = 0 = a_y$,

$$\frac{dJ_{5,6}}{dt_{6}} = -2\left[\dot{a}_{x}(\dot{x}_{E} - \dot{x}) + \dot{a}_{y}(\dot{y}_{E} - \dot{y})\right]$$
(16)

This, then, is the quantity which must equal $a^2(t_0)$ or $a_H^2(t_1)$ for the minimum total J_m case.

Actually, the most general case of atmospheric braking is one in which the entry speed is fixed at some desired or maximum allowable value that is not necessarily equal to that for the flyby case. Here, $a_{\rm H}^2(t_6)$ is not zero and equation (15) is applicable. Although such cases could be generated, they would lead to a prohibitive collection of data. Thus, only the flyby cases have been included in this report as a limiting example. The only way to estimate fixed-entry-speed cases from the data presented would be to interpolate the value of $d_{5,6}/dt_6$ between the two cases presented. More will be said about this problem when the hybrid vehicle system is discussed.

Intermediate mass ejection. - In the usual manned round trip, some amount of mass will be left behind at the target planet. Because there is no change in the parameter \mathbf{J}_m to account for this sharp drop in mass, the problem must be considered in two separate phases.

In the first phase, from Earth to planet arrival, it follows that

$$dm_3 = \frac{r_{m_3}}{r_{J_{0,3}}} \left(\frac{r_{J_{0,3}}}{r_{t_3}} dt_3 + \frac{r_{J_{0,3}}}{r_{t_0}} dt_0 \right)$$

where

$$J_{0, 3} = J_{0, 1} + J_{1, 2} + J_{2, 3}$$

Also, for the return phase

$$dm_7 = \frac{\partial m_7}{\partial J_{4,7}} \left(\frac{\partial J_{4,7}}{\partial t_4} dt_4 + \frac{\partial J_{4,7}}{\partial t_7} dt_7 \right) + \frac{\partial m_7}{\partial m_4} dm_4$$

where

$$J_{4,7} = J_{4,5} + J_{5,6} + J_{6,7}$$

Finally, across the waiting phase,

$$m_4 = m_3 - m_{L, P}$$

$$dm_4 = dm_3 - dm_{L, P}$$

where $m_{L,\,P}$ is the mass left at the planet. Combining all these relations with equations (11) and (12) gives

$$dm_{7} = \left[-\frac{\partial m_{7}}{\partial J_{4,7}} a^{2}(t_{4}) + \frac{\partial m_{7}}{\partial m_{4}} \frac{\partial m_{3}}{\partial J_{0,3}} a^{2}(t_{3}) \right] dt_{3}$$

$$+ \left[\frac{\partial m_{7}}{\partial J_{4,7}} a^{2}(t_{7}) - \frac{\partial m_{7}}{\partial m_{4}} \frac{\partial m_{3}}{\partial J_{0,3}} a^{2}(t_{0}) \right] dt_{0} - \frac{\partial m_{7}}{\partial m_{4}} dm_{L, P}$$
(17)

In addition, there exists the general relation between J, mass, and power

$$\frac{1}{m_f} - \frac{1}{m_0} = \frac{J}{2P}$$

which can be used to show that

$$\frac{\partial m_7}{\partial m_4} = \left(\frac{m_7}{m_4}\right)^2$$

$$\frac{\partial \mathbf{m_3}}{\partial \mathbf{J_{0,3}}} = -\frac{\mathbf{m_3^2}}{2\mathbf{P}}$$

$$\frac{\partial m_7}{\partial J_{4,7}} = -\frac{m_2^2}{2P}$$

Therefore, equation (17) can be written as

$$dm_{7} = \frac{m_{7}^{2}}{2P_{j}} \left[a^{2}(t_{4}) - \left(\frac{m_{3}}{m_{4}} \right)^{2} a^{2}(t_{3}) \right] dt_{3} + \frac{m_{7}^{2}}{2P_{j}} \left[\left(\frac{m_{3}}{m_{4}} \right)^{2} a^{2}(t_{0}) - a^{2}(t_{7}) \right] dt_{0} - \left(\frac{m_{7}}{m_{4}} \right)^{2} dm_{L, P}$$
(18)

For the coefficient of dt_3 to vanish, it can be seen that

$$m_4^a(t_4) = m_3^a(t_3)$$

$$\mathbf{F_4} = \mathbf{F_3}$$

which points out that the thrust F should carry across the wait phase. Also, it is clear that it would be convenient to choose

$$m_4 = km_3$$

where

$$0 < k \le 1.0$$

which leads to

$$ka(t_4) = a(t_3)$$

$$ka(t_7) = a(t_0)$$
(19)

which represents only a slight modification of the case for minimum J_m . Again, in the case of unrestricted atmospheric braking at Earth return, equation (16) is used in place of $a(t_7)$.

Hybrid case. - Recent studies (e.g., refs. 3 to 5) have indicated a possible role for electric rockets when used to reduce the propulsive requirements of typical high-thrust rockets by thrusting during the heliocentric part of the flight. In such mission modes, the high-thrust chemical or nuclear rocket is used to perform the planet centered escape or capture maneuvers by adding velocity in the gravitational field of the planet. Such maneuvers affect the low-thrust mission by changing the initial and final conditions of the heliocentric transfer as follows:

$$\Delta V_{\rm H} = \sqrt{\left(V_{\rm c} + \Delta V\right)^2 - 2V_{\rm c}^2} \tag{20}$$

where ΔV_H is the change in heliocentric velocity, ΔV is the characteristic velocity increment of a high-thrust rocket, and V_C is the circular orbital velocity at planet orbit pericenter. This equation assumes that (1) the high-thrust rocket can effect an instantaneous change in velocity and (2) that the potential energy of the escape hyperbola is negligible at the point of transfer to heliocentric coordinates. The problem, then, is to determine the ΔV 's for which the overall transfer has minimum propellant usage. Unfortunately, this would require the same excessive volume of data needed for the case of atmospheric braking from preselected velocities. Also, trajectories would be required with various values of ΔV_H at both ends of the path, leading to a volume of data at least an order of magnitude larger than that included herein. Again, some interpolation method between the cases presented would be of interest.

Boosting to escape energy. - One simple hybrid case, which can, at times, be better than the all-electric case (see ref. 4), is boosting to a value of $\Delta V_H = 0$. In this instance, the capture data presented in this note may be used directly without attaching the planetary spirals. For one-way trips, we choose, as usual, the minimum J_H travel angle, and account for the planetary maneuvers separately. Considering the mission payload to be the terminal mass minus the mass of the powerplant

$$\frac{m_{L}}{m_{0}} = \left(\frac{m_{1}}{m_{0}}\right) \left(\frac{m_{2}}{m_{1}}\right) \left(\frac{m_{3}}{m_{2}}\right) - \frac{m_{pp}}{m_{0}}$$
(21)

where

$$\frac{\frac{m_{pp}}{m_{0}} = \alpha \frac{P}{m_{0}}}{\frac{P}{m_{0}}} = \frac{1}{1 + \frac{m_{s}}{m_{p}}} \left[e^{-\Delta V_{0}/I_{1}g} - \frac{m_{s}}{m_{p}} - \frac{m_{s}}{m_{p}} \right]_{0}} = \frac{\frac{m_{2}}{m_{1}}}{1 + \frac{\beta_{1, 2}^{2}}{m_{0}}} = \frac{1}{1 + \frac{\beta_{1, 2}^{2}}{m_{0}}} = \frac{\alpha J_{1, 2}}{1 + \frac{m_{s}}{m_{p}}} = \frac$$

Payload is used here, rather than final mass, because these expressions may be maximized with respect to $m_{\rm DD}/m_0$, giving

$$\frac{m_{pp}}{m_0} = \beta_1, 2 \left[\sqrt{\left(\frac{m_1}{m_0}\right) \left(\frac{m_3}{m_2}\right)} - \beta_1, 2 \right]$$

and

$$\frac{\mathbf{m_L}}{\mathbf{m_0}} = \sqrt{\left(\frac{\mathbf{m_1}}{\mathbf{m_0}}\right)\left(\frac{\mathbf{m_3}}{\mathbf{m_2}}\right)} - \beta_{1, 2}$$
 (22)

In the case of manned round-trip missions, it can be recognized that equation (19) is applicable with the following replacements:

$$a(t_{5}) = a(t_{4})$$

$$a(t_{1}) = a(t_{0})$$

$$a(t_{2}) = a(t_{3})$$

$$a(t_{6}) = a(t_{7})$$

$$K = \left(\frac{m_{3}}{m_{2}}\right) \left(\frac{m_{4}}{m_{3}}\right) \left(\frac{m_{5}}{m_{4}}\right)$$
(23)

Equation (23) resolves the problem of maximum m_7 as regards the choices of t_0 and t_3 , but does not indicate the best value of m_{pp}/m_0 . This must be derived from the expression

$$\frac{m_{L}}{m_{0}} = \frac{m_{1}}{m_{0}} \left[\left(\frac{m_{2}}{m_{1}} \right) k \left(\frac{m_{6}}{m_{5}} \right) \left(\frac{m_{7}}{m_{6}} \right) - \frac{m_{pp}}{m_{1}} \right]$$

where

$$\frac{\frac{m_2}{m_1} = \frac{1}{1 + \frac{\beta_{1, 2}^2}{\binom{m_{pp}}{m_1}}}$$

$$\frac{\frac{m_{6}}{m_{5}} = \frac{1}{1 + \frac{K\beta_{5, 6}^{2}}{\binom{m_{pp}}{m_{1}}} \binom{m_{2}}{m_{1}}}$$

Optimization of this form with respect to mpp/m1 gives

$$\frac{\mathbf{m}_{pp}}{\mathbf{m}_{0}} = \left(\frac{\mathbf{m}_{1}}{\mathbf{m}_{0}}\right) \left[\sqrt{\mathbf{K}\left(\frac{\mathbf{m}_{7}}{\mathbf{m}_{6}}\right)} - \beta^{*}\right] \beta^{*}$$

$$\frac{\mathbf{m_L}}{\mathbf{m_0}} = \left(\frac{\mathbf{m_1}}{\mathbf{m_0}}\right) \left[\sqrt{\mathbf{K} \left(\frac{\mathbf{m_7}}{\mathbf{m_6}}\right)} - \beta^* \right]^2$$

where

$$\beta^* = \left(\beta_{1, 2}^2 + K\beta_{5, 6}^2\right)^{1/2} \tag{24}$$

Boosting to small energies beyond escape. - Although the preceding analysis for boosting to escape is exact, it will always pay to go above escape to some degree. This can be seen by noting from equation (20) that $d(\Delta V_H)/d(\Delta V) \rightarrow \infty$ as $\Delta V_H \rightarrow 0$.

If ΔV_H is small but positive, we may compute to the first order the change in J from the transversality relation (eq. (14))

$$dJ_{1,2} = \left[(a^2 - 2a_x\ddot{x} - 2a_y\ddot{y} + 2\dot{a}_x\dot{x} + 2\dot{a}_y\dot{y})dt + 2a_x dx + 2a_y dy - 2\dot{a}_x d\dot{x} - 2\dot{a}_y d\dot{y} \right]_{t_1}^{t_2}$$

$$= dJ_{t=t_2} - dJ_{t=t_1}$$

The changes in the end or starting conditions due to braking or boosting are then computed from

$$\dot{\mathbf{x}} = \dot{\mathbf{x}}_{\mathbf{E}} + \Delta \mathbf{V}_{\mathbf{H}} \cos \gamma$$

$$\dot{y} = \dot{y}_E + \Delta V_H \sin \gamma$$

which gives

$$d\dot{x} = -(\Delta V_H)\sin \gamma \ d\gamma + \cos \gamma \ d(\Delta V_H)$$

$$d\dot{y} = (\Delta V_H)\cos \gamma d\gamma + \sin \gamma d(\Delta V_H)$$

If everything except the velocity components are assumed to be fixed, substitution gives

$$\mathrm{d}J_{\mathrm{H,\,J}} = \left[(-2a_{\mathrm{x}}\,\sin\gamma \,+\,2a_{\mathrm{y}}\,\cos\gamma)\Delta\,V_{\mathrm{H}}\,\,\mathrm{d}\gamma \,+\,2(a_{\mathrm{x}}\,\cos\gamma \,+\,a_{\mathrm{y}}\,\sin\gamma)\mathrm{d}(\Delta\,V_{\mathrm{H}})\right]_{t_{\mathrm{1}}}^{t_{\mathrm{2}}}$$

Thus, the optimum γ must have

$$\tan \gamma = \frac{a_x}{a_y} = \tan \varphi$$

and,

$$\gamma = \varphi \quad \text{or} \quad \gamma + \pi \tag{25}$$

In order to have the best ΔV_H , it follows that

$$\tan \gamma = -\frac{1}{\tan \varphi}$$

 \mathbf{or}

$$\mathbf{a}_{\mathbf{X}} = \mathbf{a}_{\mathbf{y}} = \mathbf{0} \tag{26}$$

The first part of equation (26) is contrary to equation (25) and the second part of equation (26) is precisely the flyby end conditions which are, of course, the best value of ΔV_H . Although we are not concerned herein with the flyby case, we can add in an increment beyond escape ΔV_H in the proper direction. Thus,

$$\Delta J_{1,2} = \pm 2a(t_2)\Delta V_{H,2} \mp 2a(t_1)\Delta V_{H,1}$$

where the choice of sign depends on whether $\gamma = \varphi$ or $\varphi + \pi$. Clearly, both should be negative giving

$$\gamma(t_1) = \varphi(t_1)$$
 (27)
$$\gamma(t_2) = \varphi(t_2) + \pi$$

Now that the appropriate directions for the various ΔV_H are resolved, it is necessary to consider how large ΔV_H can be made before this simple first-order analysis produces serious errors. In figure 3, the approximate and exact values of $J_{1,2}$ are compared for simultaneous addition of ΔV_H values of the same size at both ends of a typical Earth-Mars trajectory. In this particular example, it would seem possible to add about 2000 meters per second in combination before the errors became very large (e.g., about 50 percent at $\Delta V_H = 3000$ m/sec).

All the ΔV_H in the exact curve in figure 3 are added parallel to the original values of a as determined for $\Delta V_H = 0$. Figure 4 shows that the size of ΔV_H has very little effect on the best orientation angle φ , at least for the range covered.

Boosting to high energies beyond escape. - It should be noted that boosting or braking at one end only must include the flyby case as an extreme or minimum value of J. Actually, considering $J_{1,2}$ as a function of $\Delta V_{H,1}$ and $\Delta V_{H,2}$, much knowledge about this function can be extracted from the information presented. Specifically, the values of $J_{1,2}$, $\partial J_{1,2}/\partial \Delta V_{1,2}$, and $\partial J_{1,2}/\partial \Delta V_{H,2}$ are all known for three different combina-

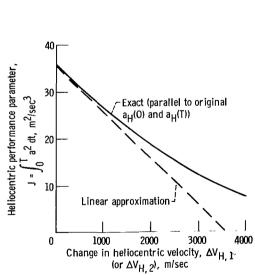


Figure 3. - Effect of change in heliocentric velocity on heliocentric performance parameter. Duration of Earth to Mars trip, 270 days; thrust angle 6.026 radians.

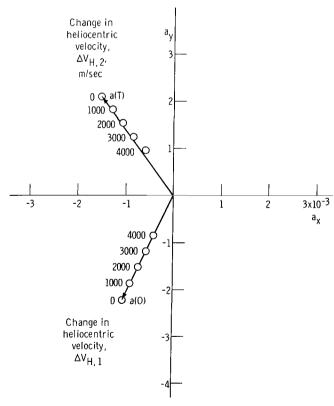


Figure 4. - Shift in initial and terminal thrust accelerations vectors due to addition of changes in heliocentric velocity at departure and arrival. Thrust angle, 6.02 radians. (ΔV_H are added parellel to original value of $a_H(0)$ for $\Delta V_{H,\,1}$ = 0 and $a_H(1)$ for $\Delta V_{H,\,2}$ = 0).

tions of $\Delta V_{H,\,1}$ and $\Delta V_{H,\,2}$. Also, the classical two-impulse transfer, for which $J_{1,\,2}$ is zero, could be added as a fourth and extreme case. It would seem possible to create some sort of interpolation formula for approximation of the function $J_{1,\,2}(\Delta V_{H,\,1},\Delta V_{H,\,2})$. For example, if boosting at one end only is considered, the flyby and orbiter cases together form sufficient information for a cubic curve fit for $J_{1,\,2}(\Delta V_{H,\,1})$.

Whatever methods are used to estimate the function $J_{1,2}$, it will then become important to consider the trade-off problem between the high- and low-thrust parts of the system. To start with, consider a one-way transfer with boosting at the start only. The final mass for such a case is

$$m_{2} = \left(\frac{1}{m_{1}} + \frac{J_{1,2}}{2P}\right)^{-1}$$

$$m_{1} = m_{0} \left[\left(1 + \frac{m_{s}}{m_{p}}\right) e^{-\Delta V/Ig} - \frac{m_{s}}{m_{p}}\right]$$
(28)

where

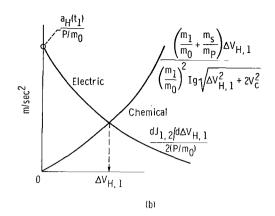
$$\Delta V = \sqrt{\Delta V_{H, 1}^2 + 2V_c^2} - V_c$$

Differentiating with respect to $\Delta V_{H.1}$ yields

$$\frac{dm_{2}}{d(\Delta V_{H, 1})} = -\left(\frac{m_{2}}{m_{0}}\right)^{2} \left[\frac{\left(\frac{m_{1}}{m_{0}} + \frac{m_{s}}{m_{p}}\right) \Delta V_{H, 1}}{\left(\frac{m_{1}}{m_{0}}\right)^{2} \operatorname{Ig} \sqrt{\Delta V_{H, 1}^{2} + 2V_{c}^{2}}} + \frac{\frac{dJ_{1, 2}}{d \Delta V_{H, 1}}}{2\left(\frac{P}{m_{0}}\right)} \right]$$

For an optimum, it is necessary that

$$\frac{\left(\frac{m_{1}}{m_{0}} + \frac{m_{s}}{m_{p}}\right) \Delta V_{H, 1}}{\left(\frac{m_{1}}{m_{0}}\right)^{2} \operatorname{Ig} \sqrt{\Delta V_{H, 1}^{2} + 2V_{c}^{2}}} = -\frac{\frac{dJ_{1, 2}}{d \Delta V_{H, 1}}}{2\left(\frac{P}{m_{0}}\right)} = \frac{a_{H}(t_{1})}{\frac{P}{m_{0}}} \tag{29}$$



Since each side of equation (29) is a function either of the high- or low-thrust stage, a simple graphical procedure shown in sketch (b) can be applied to find the solution. Similar criteria can also be derived for the more complex case of boosting and braking; however, it is clear at this point that a subsidiary iteration must be introduced to find the best values of the various $\Delta V_{H,\,1}$. This greatly complicates the overall optimization problem for such cases as round trips. For this reason, the trajectory data generated in this report have been put on data processing cards to assist those readers interested in developing computer oriented optimization schemes.

RESULTS AND DISCUSSION

As noted previously, the data consists of three different types of flight paths: planet flyby, Earth flyby, and planet capture. For each type and each planet, an array of data are presented for seven different travel times and eleven different travel angles. These are given in tables I to III. In table I, J, $V_x(T)$, $V_y(T)$, $a_x(0)$, $a_y(0)$, $a_x(0)$, $a_y(0)$, $a_x(0)$, $a_x(0)$, and $a_y(T)$ are presented for each T and ψ measured from the planet to Earth flyby. A very similar format is used in table II for the planet captures except that $a_x(T)$ and $a_y(T)$ (which are zero for the flyby) are given instead of $V_x(T)$ and $V_y(T)$ (which are now specified). Table III is identical to table I except that it is for the planet flyby rather than Earth flyby from the planet.

The tables I to III use the SI system of units for most variables; for example, $a_{\chi}(0)$ is given in meters per second square and $\dot{a}_{\chi}(0)$ in meters per second cubed. Also, the travel time T is given in days, and ψ in radians. The E appearing in tables I to III is a standard computer output format meaning exponent. Thus, 1.632 E+05 means 1.632×10^5 , while 1.372 E-03 means 1.372×10^{-3} .

In order to illustrate more fully the use of the data presented in this report, a series of numerical examples are presented herein for the case of various missions from Earth

to Saturn. The selection of Saturn as the target planet has no particular significance other than that it is a difficult mission which may be of interest to low-thrust vehicle designers.

All Electric Case

As a first example, consider a transfer from low Earth orbit to the outer rings of Saturn. Furthermore, consider only the case where electric propulsion will be used for all phases of the mission.

Since a spiral will be used both at Earth and Saturn, it will be convenient to use a series of escape and/or capture trajectory properties (see fig. 2). This data was generated using the semi-empirical method presented in reference 7. The form in which this data is presented (J and T as functions of $a_{\chi}(0)$) is designed to help select the optimal spirals which belong to any heliocentric path.

Since a spiral is to be patched on at each end of the flight path, a capture type heliocentric trajectory is the obvious choice in this case. Also, since this is to be a one-way trip, the heliocentric polar angle ψ_H should be chosen for minimum or near minimum $\mathbf{J_H}$. Accordingly, from table II at a $\mathbf{T_H}$ of 1000 days,

$$T_{\rm H} = 1000 \; {\rm days} = T_{1,\,2}$$

$$\psi_{\rm H} = 3.665 \; {\rm rad} = 210^{\rm O} = \psi_{1,\,2}$$

$$J_{\rm H} = 23.64 \; {\rm m^2/sec^2} = J_{1,\,2}$$

$$a_{\rm x}(0) = -1.758 \times 10^{-4} \; {\rm m/sec^2} = a_{\rm x}(t_1)$$

$$a_{\rm y}(0) = 8.394 \times 10^{-4} \; {\rm m/sec^2} = a_{\rm y}(t_1)$$

$$a_{\rm x}(T) = 8.490 \times 10^{-4} \; {\rm m/sec^2} = a_{\rm x}(t_2)$$

$$a_{\rm y}(T) = 1.781 \times 10^{-4} \; {\rm m/sec^2} = a_{\rm y}(t_2)$$

$$\dot{a}_{\rm x}(0) = -1.332 \times 10^{-10} \; {\rm m/sec^3} = \dot{a}_{\rm x}(t_1)$$

$$\dot{a}_y(0) = 2.994 \times 10^{-11} \text{ m/sec}^3 = \dot{a}_y(t_1)$$

$$\dot{a}_{x}(T) = 1.950 \times 10^{-11} \text{ m/sec}^{3} = \dot{a}_{x}(t_{2})$$

$$\dot{a}_{y}(T) = 4.847 \times 10^{-12} \text{ m/sec}^{3} = \dot{a}_{x}(t_{2})$$

From the acceleration components,

$$a_{H}(t_{1}) = a_{H}(0) = \left[a_{x}^{2}(0) + a_{y}^{2}(0)\right]^{1/2} = 8.57 \times 10^{-4} \text{ m/sec}^{2}$$

$$a_{H}(t_{2}) = a_{H}(T) = 8.67 \times 10^{-4} \text{ m/sec}^{2}$$

Recalling from equations (6) and (7) that the acceleration for the spirals must equal the $a_H(t_1)$ at the extremes of the heliocentric flight path, the following planetocentric data is obtained from figure 2 at $a = 8.57 \times 10^{-4}$.

$$J = 6.1 \text{ m}^2/\text{sec}^3 = J_{0,1}$$

$$T = 94 \text{ days} = T_{0, 1}$$

Also, at $a = 8.67 \times 10^{-4}$ meter per second squared (using the Saturn outer ring curve),

$$J = 12.5 \text{ m}^2/\text{sec}^3 = J_{2,3}$$

$$T = 193 \text{ days} = T_{2,3}$$

Therefore,

$$T_{m} = 94 + 1000 + 193 = 1287 \text{ days}$$

$$J_{m} = 6.1 + 23.64 + 12.5 = 42.24 \text{ m}^{2}/\text{sec}^{3}$$

The natural, and rather simple, extensions of this case to a round trip without any mass ejection at the planet leads to a mirror image trajectory including the spirals. The stay time at the planet is computed as follows:

$$T_{W} = \frac{\psi_{1,2} + \psi_{5,6} - (T_{1,2} + T_{5,6})\omega_{E} + 2N\pi}{(\omega_{E} - \omega_{p})} - (T_{2,3} + T_{4,5})$$

For the particular case of Earth and Saturn,

$$\omega_{\mathbf{p}} = 0.676 \times 10^{-8} \text{ rad/sec}$$

$$\omega_{\rm E}$$
 = 1.99×10⁻⁷ rad/sec

Using the same $T_{0,1}$ and $T_{2,3}$ values computed previously, the value of T_{w} at N=6 is 254 days.

The total mission time then becomes

$$T_{m} = 2T_{2,3} + 2T_{0,1} + T_{w} + T_{1,2} + T_{5,6} = 2828 \text{ days}$$

The value of N = 6 was used here because it was the smallest value that gave a positive value for T_w . Larger values of N will add on an amount of wait time equal to $2\pi/(\omega_E - \omega_p)$, that is, the synodic period between Saturn and Earth.

Intermediate mass ejection. Consider now the more realistic case where a considerable amount of equipment and supplies are used or left at Saturn. For example, assume that 20 percent of the space vehicle mass is expended at Saturn. From equation (19),

$$a_{H}(t_{5}) = a(t_{5}) = \frac{a(t_{3})}{0.80} = 1.084 \times 10^{-3} \text{ m/sec}^{2}$$

$$a_{H}(t_{6}) = a(t_{6}) = \frac{a(t_{1})}{0.80} = 1.072 \times 10^{-3} \text{ m/sec}^{2}$$

At this point, it is helpful to recognize that trajectories having the same initial and terminal accelerations are optimum travel-angle cases in the sense of minimum J_H . This is clear from the data extracted here at 1000 days and can be verified by the reader

either by examination of table II or by algebraic manipulation of the transversality condition (eq. (8)). The other case where the initial and terminal heliocentric accelerations are the same is the case where J_H as a function of ψ_H is a maximum. Clearly, this is not the case of interest here.

From table II, for the minimum J_H as a function of ψ_H cases, the nearest table value other than T_H = 1000 is T_H = 8000 days. For this value of T_H ,

$$J_{5, 6} = 44.63 \text{ m}^2/\text{sec}^3$$
 $a_{\text{H}}(t_6) = 1.361 \times 10^{-3} \text{ m/sec}^2 = a_{\text{E}, 2}$
 $a_{\text{H}}(t_5) = 1.383 \times 10^{-3} \text{ m/sec}^2 = a_{\text{p}, 2}$
 $\psi_{5, 6} = 3.142 \text{ rad}$

Actually, this is a higher acceleration than needed, and the true optimized value of T_H is about 900 days. However, the choice of the ejected mass was arbitrary and would have lead to the 800 day return trip if it were chosen as about 40 percent.

When the 800-day case is desired, the optimal planetary maneuvers are found (fig. 2) to be

$$T_{4, 5} = 120 \text{ days}$$

$$J_{4, 5} = 19.5 \text{ m}^2/\text{sec}^3$$

$$T_{6, 7} = 59 \text{ days}$$

$$J_{6, 7} = 9.8 \text{ m}^2/\text{sec}^3$$

Therefore,

$$J_{m} = 6.1 + 23.64 + 12.5 + 19.5 + 44.63 + 9.8 = 116.17 \text{ m}^{2}/\text{sec}^{3}$$

$$N = 5$$

$$T_{w} = 125 \text{ days}$$

$$T_{m} = 94 + 1000 + 193 + 125 + 120 + 800 + 59 = 2391 \text{ days}$$

Introduction of atmospheric braking. - Next, consider the case where atmospheric braking is used at the end of the mission. This will be simulated by using an Earth flyby trajectory on the return trip from Saturn to Earth. Also, it will again be assumed that 20 percent of the vehicle mass is left at Saturn.

From previous calculations, it will still follow that the acceleration at the start of the return trip (and also of the spiral preceding the return trip) must be 1.072×10^{-3} meter per second squared. However, equation (16) must now be used with equation (19) to give

$$2K^{2}\left\{\dot{a}_{x}(T)\left[\dot{x}_{E}-\dot{x}(T)\right]+\dot{a}_{y}\left[\dot{y}_{E}-\dot{y}(T)\right]\right\}=a_{E,1}^{2}$$

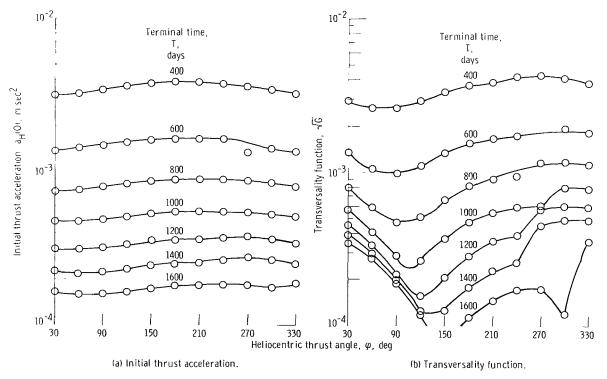


Figure 5. - Trajectory data for Saturn-Earth flyby.

$$G = \sqrt{\frac{\dot{\overline{a}}(T) \cdot [\overline{V}_E - \overline{V}(T)]}{K}} = \frac{a_{E, 1}}{K} = 1.361 \times 10^{-3} \text{ m/sec}^2$$

In order to satisfy both this condition and the prescribed initial acceleration, it is con-

venient to construct plots of $a_H(0) = a_H(t_5)$ and $\sqrt[4]{2a(T)} \cdot [(\overline{V}_E - \overline{V}(T)]$ as functions of ψ_H using T_H as a parameter. Since all the data needed to determine these quantities are available on cards, a very simple computer program can be written which will generate the data needed for any special plots. This has been done for the Saturn-Earth flyby and is displayed in figure 5.

From figure 5(a), it is clear that T_H should be between 700 and 750 days in order to satisfy the acceleration requirement at the start of the return trip. Unfortunately, the second requirement can only be satisfied for either $\psi_H \cong 300$ or $\psi_H \cong 0^O$. An examination of table I indicates that the 0^O case has a slightly lower value of J_H and will therefore be chosen as the optimal return trip.

Interpolating between entries in table I yields

$$T_{5, 6} = T_{H} = 700 \text{ days}$$

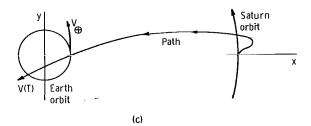
$$\psi_{5, 6} = \psi_{H} = 0^{O}$$

$$J_{H} = 22 \text{ m}^{2}/\text{sec}^{3} = J_{5, 6}$$

$$V_{x}(T) = -4.7 \times 10^{4} \text{ m/sec} = V_{x}(t_{6})$$

$$V_{y}(T) = -8.6 \times 10^{3} \text{ m/sec} = V_{y}(t_{6})$$

It is important to note that the terminal velocity components indicate a path of the type shown in sketch (c). In essence, the thrust is used to nullify the initial velocity where-upon the vehicle falls almost radially to meet Earth. While such a path may indeed be the optimal path for the conditions requested, it clearly gives very high atmospheric entry speeds. In the case shown in sketch (c),



$$\Delta V_{H, 6} = \sqrt{(V_x(T) - V_{xE})^2 + (V_y(T) - V_{yE})^2} = 6.06 \times 10^4 \text{ m/sec}$$

When the perigee of the approach hyperbola is near the surface of the Earth,

$$V_{c.6}(Surface) = 7920 \text{ m/sec}$$

and

$$V_a = \sqrt{(\Delta V_{H, 6})^2 + 2V_{c, 6}^2} = 6.16 \times 10^4 \text{ m/sec}$$

Considering that atmospheric entry speeds are often restricted to values below 20 kilometers per second, the case we have selected would very likely be rejected for practical reasons. However, the case has illustrated the general procedure for using the data for round-trip calculations. From this point on, the calculation of T_w , T_m , and J_m are the same as before.

Hybrid Case

As a final example, a case is considered where both high- and low-thrust rocket systems are combined. In particular, it will be assumed that a nuclear rocket is used at the start of the mission for the Earth escape maneuver. There is, of course, the trivial case of boosting exactly to escape energy. In this case, we would simply delete the first spiral and use the J_H from table Π . However, it is always better to go somewhat beyond escape energy, and this problem is considered in this section.

For small values of $\Delta V_{H,1}$, the procedure would be to use the first-order approach where $J_H(0)$ is modified using the initial slope $2a_H(0)$.

$$J_{1, 2}(\Delta V_{H, 1}) = J_{1, 2}(0) - 2a_{H}(t_{1})\Delta V_{H, 1}$$

Where $J_{1,2}(0)$ and $a_H(t_1)$ are values taken from table Π at the proper time and angle.

For higher values of $\Delta V_{H,\ 1}$, a plot of $J_{1,\ 2}(\Delta V_{H,\ 1})$ can be constructed from the data in tables I and II. For example, consider the 1000-day Earth-Saturn path used previously. From table II we compute

$$T_{H} = 1000 \text{ days}$$

$$\psi_{\mathrm{H}}$$
 = 3.665 rad

$$J_{H}(\Delta V_{H, 1} = 0) = 23.64 \text{ m}^{2}/\text{sec}^{3}$$

$$\frac{dJ_{H}}{d(\Delta V_{H, 1})} = -2a_{H}(t_{1}) = -17.15 \times 10^{-4} \text{ m/sec}^{2}$$

and, from table I,

$$J_{\rm H} = 7.3 \, {\rm m}^2/{\rm sec}^3$$

$$V_{x}(T) = -5.592 \times 10^{3} \text{ m/sec}$$

$$V_y(T) = -4.53 \times 10^4 \text{ m/sec}$$

$$\Delta V_{H, 1} = 2.835 \times 10^4 \text{ m/sec}$$

From this data, a figure such as figure 6 can be constructed in the following manner:

- (1) From table II, the point value of J and the slope $(-2a_H(t_1))$ at the value $\Delta V_{H,1} = 0$ are obtained.
- (2) From table I, the values of J and $\Delta V_{H, 1}$ are used as the minimal J coordinates (because the Earth flyby corresponds to minimal J with respect to $V_{x}(T)$ and $V_{y}(T)$, and therefore with respect to the total relative magnitude $\Delta V_{H, 1}$).

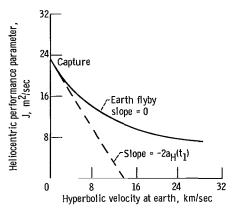


Figure 6. - Effect of initial high-thrust boost on Earth-Saturn propulsive requirements.

Assuming that the mass ratio for the nuclear and electric rockets can be approximated by

$$\frac{m_1}{m_0} = \left(1 + \frac{m_s}{m_p}\right) e^{-\Delta V/Ig} - \frac{m_s}{m_p} - \frac{F}{m_0} \left(\frac{M_{eng}}{F}\right)$$

$$\frac{\mathbf{m_2}}{\mathbf{m_1}} = \left(\frac{1}{\mathbf{m_1}} + \frac{\mathbf{J_H}}{2\mathbf{P}}\right)^{-1}$$

These equations are the same as equation (28) except for the addition of the initial thrust acceleration F/m_0 and specific engine mass $m_{\rm eng}/F$, which are used here to account for the nuclear rocket engine, reactor, and shield mass.

By differentiating these equations, a set of conditions equivalent to equation (29) are derived.

$$\frac{\left(\frac{m_{1}}{m_{0}} + \frac{m_{s}}{m_{p}} + \frac{m_{eng}}{m_{0}}\right) \Delta V_{H, 1}}{\left(\frac{m_{1}}{m_{0}}\right) Ig \sqrt{\Delta V_{H, 1}^{2} + 2V_{c, 0}^{2}}} = \frac{a_{H}(t_{1})}{\frac{P}{m_{1}}}$$

A plot of the left side of this relation can be made once the following choice of parameters is made:

Specific impulse, I, sec
Structure- to propellant-mass ratio, m_s/m_p 0.10
Specific engine mass, m _{eng} /F
Initial thrust acceleration, F/m ₀

Figure 7 illustrates the form of the relation along with a similar function for a typical chemical rocket. The reader may find this plot rather useful because it will change only if the initial parking orbit about Earth changes.

As indicated in sketch (b), we must superimpose a plot of $a_H(t_1)/2(P/m_1)$ as a function of $\Delta V_{H, 1}$ on figure 7. For a given value of P/m_1 , this can be estimated from figure 6 to vary between $2a_H(t_1)$ at $\Delta V_{H, 1} = 0$, and zero at the Earth flyby point. For sim-

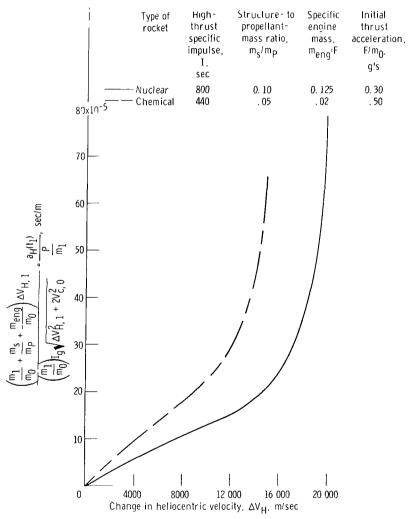


Figure 7. - Graphical method of locating best value of heliocentric velocity increment for hybrid system performance. Circular Earth orbit, 300 nautical miles (555.6 km).

plicity, it is assumed that $a_H(t_1)$ is a linear function of $\Delta V_{H,1}$.

In order to obtain a numerical answer, it is assumed that $\alpha P/m_1 = 1/3$, which is often the case in many problems of this type. Also, we will assume $\alpha = 15$ kilograms per kilowatt. The value of P/m then becomes

$$\frac{P}{m_1} = \frac{1000}{3 \times 15} = 22.2 \text{ W/kg}$$

By drawing a straight line on figure 7 having the intercept $a_H(t_1)/(P/m_1)$ at $\Delta V_{H, 1} = 0$ and the other at zero and $\Delta V_{H, 1} = 2.835 \times 10^4$ meters per second, the best value of $\Delta V_{H, 1}$ is found to be 2400 meters per second.

For the circular orbit altitude in figure 8, $V_{c,\,0}$ is equal to 7590 meters per second. Therefore,

$$\Delta V_0 = \sqrt{\Delta V_{H, 1}^2 + 2 V_c^2} - V_{c, 0} = 3420 \text{ m/sec}$$

and,

$$\frac{m_1}{m_0} = 0.5735$$

From figure 6 at a $\Delta V_{H, 1}$ value of 2400, J_H is equal to 19.6 square meters per second cubed; therefore,

$$\frac{\frac{m_2}{m_1} = \frac{1}{1 + \frac{J_{1,2}}{2\left(\frac{P}{m_1}\right)}} = 0.694$$

and

$$\frac{m_2}{m_0} = 0.5735 \times 0.694 = 0.3975$$

For comparison, the value of m_2/m_0 corresponding to $\Delta V_{H,~1}$ = 0 is 0.3930, indicating only a small loss relative to the optimum value. On the other hand, m_2/m_0 for $\Delta V_{H,~1}$ = 4000 meters per second is 0.382, still indicating a rather flat curve for m_1/m_0 as a function of $\Delta V_{H,~1}$.

Although the example here is for a fixed value of P/m_1 , it can be repeated for other values until an optimum value is found. Also, the inclusion of other high-thrust maneuvers is similar in principle, but otherwise more complicated than the rather simple case used herein. Clearly, for very complex missions using hybrid systems and possibly some planetary spirals, a computerized procedure would be advisable. This is the reason for placing the data of tables I to III on cards.

CONCLUDING REMARKS

In presenting this data, an effort has been made to include enough data to allow the reader to make significant mission analyses for constant power electric vehicles. However, the data has not as yet been used extensively for mission analysis purposes. Therefore, it will no doubt be true in many instances that some cases of interest will lie outside the range of the data presented. This is most likely going to be true for the case of Mercury, where polar travel angles in excess of 330° are likely to be of interest. An effort to extend the angle range for Mercury was made, but numerical difficulties were encountered beyond 330° .

Although initial and terminal conditions have been included, the accuracy data was based only on the error in the parameter J. It is therefore very possible that the errors in the initial and terminal conditions are much larger. Unfortunately, there is no apparent way to avoid or detect such errors without additional computation which calls for careful numerical integration of the nonlinear differential equations using the starting conditions given in the tables. Such additional calculations could be very time consuming and would not be justified unless the data as presented prove too inaccurate for the type of analysis for which it is used. In any event, the initial conditions presented would make excellent starting guesses for more accurate methods.

Finally, some effort has been made to construct a curve fit to the surface $J(\Delta V_{H,\,1}, \Delta V_{H,\,2})$. Although this work is incomplete at this time, it appears best to make an expansion in terms of the variables $(\Delta V_{H,\,1} - \Delta V_{H,\,1}^*)$ and $(\Delta V_{H,\,2} - \Delta V_{H,\,2}^*)$, where $\Delta V_{H,\,1}^*$ and $\Delta V_{H,\,2}^*$ are the values required for the two-impulse or single-conic transfer.

Use of these variables assures the existence of a bowl shaped zero minimum at the two impulse transfer point and also to prevent $\, J < 0 \,$ from occurring elsewhere on the surface.

Lewis Research Center,

National Aeronautics and Space Administration, Cleveland, Ohio, October 10, 1967, 120-20-07-01-22.

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TABLE I. - PLANET-EARTH FLYBY TRAJECTORIES

(a) Mercury-Earth flyby trajectories

TIME	PST	j	VX(T)	VY(T)	AX(O)	AY (G)	AXDOT(C)	AYDOT(0)	AXDOT(T)	AYDOT(T)
0.2500E 02 0.2500E 02 0.2500E 02 0.2500E 02 0.2500E 02 0.2500E 02 0.2500E 02 0.2500E 02 0.2500E 02 0.2500E 02	0.1C47E C1 C.1571E C1 C.2C94E C1 C.2C98E C1 C.3142E C1 C.3605E C1 C.4189E C1 C.4/12E C1 C.5236E C1	0.2273E 04 0.1819E 04 0.3210E 04 0.5478E 04 0.7442E 04 0.8457E 04 0.8459E 04 0.8459E 04	4. 0.4843L U5 4. 0.1257E U5 40.3701E U5 40.8551E 05 40.1187E 06 40.1256E 06 40.1015E 06 40.5120E U5 6. 6459E U4 5. 0.4561E U5	0.6060E 05 0.7329E 05 0.5837E 05 0.1943E 05 -0.3370E 05 -0.8662E 05 -0.1230E 06 -0.1309E 06 -0.1106E 06	0.5576E-01 0.5463E-02 -0.4483E-01 -0.8267E-01 -0.1006E 00 -0.1014E 00 -0.9418E-01 -0.8539E-01 0.7269E-01	0.354EE-C1 0.4964E-C1 0.3934E-C1 0.9693E-C2 -0.2628E-C1 -0.5441E-C1 -0.71C3E-C1 -0.7596E-C1 -0.1321E CC	-0.6610E-07 -0.1524E-07 C.26CCE-07 C.6661E-07 C.9766E-07 C.9533E-07 C.9533E-07 C.9151E-07 -C.7297E-07	-0.2083E-07 -0.1433E-07 0.3652E-08 0.3076E-07 0.5853E-07 0.7527E-07 0.7877E-07 0.7458E-07 0.3263E-08		-0.1221E-07 -0.2146E-07 -0.1951E-07 -0.8037E-08 0.9604E-08 0.2943E-07 0.4530E-07 0.5106E-07 0.7464E-07
0.5COUE U2 C.5OCOUE U2 G.5CCOUE C2 C.5CCOUE U2 O.5CCOUE U2 C.5CCOUE U2 C.5CCOUE U2 C.5CCOUE U2 C.5CCOUE U2 C.5CCOUE U2 O.5COUE U2	C.1047E C1 0.1571E C1 0.2094E C1 0.2018E C1 0.3142E C1 0.3665E C1 0.4189E C1 0.4712C C1 0.5236E C1	0.1331E 0.05659E C. 0.2152E U C.1823E C C.3178E C. 0.4842E C C.06111E C C.6883E C C.7363E U	4 0.2537E 05 4 0.1034E 05 3 -0.1118E 05 3 -0.3190E 05 3 -0.4480E 05 3 -0.4480E 05 3 -0.4480E 05 3 -0.494E 05 3 -0.5094E 05 3 0.4357E 05 0.55517E 05	0.1117E 05 0.1773E 05 0.1119E 05 -0.0243E 04 -0.2892E 05 -0.4914E 05 -0.5963E 05 -0.5623E 05 -0.3944E 05	0.3765E-01 0.2304E-01 0.8289E-02 -0.3793E-02 -0.1151E-01 -0.1483E-01 -0.1490E-01 -0.1306E-01 -0.1021E-01	0.1443E-01 0.1725E-C1 0.1472E-01 0.7847E-C2 -0.9046E-03 -0.9030E-C2 -0.1517E-01 -0.1516E-C1 -0.2133E-C1	-C.3413E-07 -C.242CE-07 -O.1291E-07 -C.2235E-08 0.6C46E-08 C.1115E-07 C.1351E-07 C.1361E-07	-0.1547E-07 -0.1011E-07 -0.4151E-08 0.1804E-08 0.6759E-08 0.9822E-08 0.1077E-07 C.9953E-08 0.7834E-08	-0.6544E-08 -0.3502E-08 -0.2832E-09 0.2341E-08 0.3756E-08 0.3636E-08 0.2087E-08 -0.3672E-09 -0.3008E-08	-0.1663E-08 -0.7722E-09 0.1073E-08 0.3214E-08 0.4884E-08 0.5458E-08 0.4651E-08
0.7500E C2 0.7500E C2 0.7500E U2 0.7500E U2 0.7500E 02 0.7500E C2 0.7500E C2 0.7500E C2	C.1047E C1 C.1571E C1 C.2654E C1 C.2018E C1 C.3142E C1 C.305E C1 C.4189E C1 C.4712E C1 C.5236E C1	C.1089E C U.6087E U U.2854E O C.1148E C U.5686E O C.6143E O C.8968E O G.1208E O O.1484E O	C.215bE U5 4 C.1381E U5 3 C.1684E 04 3 -U.1003E U5 3 -C.1675E 05 4 -U.1553E U5 12 -0.6140E 04 0 0.8645E 04 0 0.8645E 05 0 0.3465E 05 0 0.3721E U5	-0.5934E 04 -0.2858E 03 -0.2819E 04 -0.1186E 05 -0.2349E 05 -0.3275E 05 -0.3530E 05 -0.2911E 05 -0.1527E 05	0.2662E-01 0.1951E-01 0.1203E-01 0.5448E-02 0.5977E-03 -0.2303E-C2 -0.3534E-C2 -0.3570E-C2 -0.2849E-02	0.1611E-C1 0.1621E-C1 0.1425E-C1 0.1654E-C1 0.5942E-C2 0.1432E-C2 -0.232EE-C2 -0.5077E-C2	-C.156 EE-07 -C.143 ZE-07 -C.88 7 CE-08 -C.41 ZE-08 -C.535 EE-09 C.18 Z EE-08 C.38 7 7 E-08	-0.1318E-07 -0.9637E-08 -0.6107E-08 -0.2868E-08 -0.2391E-09 0.1542E-08 0.2422E-08 0.2508E-08	-0.3705E-08 -0.2566E-08 -0.1345E-08 -0.2889E-09 0.4016E-09 0.3760E-09 -0.1872E-09 -0.8670E-09	0.5301E-09 -0.3712E-09 -0.7329E-09 -0.6015E-09 -0.1159E-09 0.5145E-09 0.1054E-08 0.1307E-08
C.1COOE 03	0.1047E C1 0.1571E C1 0.2094E C1 0.2618E C1 0.3142E C1 0.3665E C1 0.4189E C1 0.4712E C1 0.5236E C1	C.3198E C C.1622E C U.7597E C U.3936E C U.3095E C U.3554E C L.4485E C	0.1842E 05 0.1059E 05	-0.1818E 05 -0.2210E 05 -0.2109E 05 -0.1407E 05 -0.2287E 04	0.1849E-01 0.1473E-01 0.1038E-01 0.6268E-02 0.2955E-02 0.6838E-03 -0.5944E-03 -0.1084E-02	0.1661E-C1 0.1589E-C1 0.1412E-C1 0.1412E-C1 0.8213E-C2 0.50C8E-C2 0.2197E-02 2-0.12C5E-C4 2-0.1565E-02	-C.1789E-07 -C.1577E-07 -C.1275E-07 -C.9412E-08 -C.6257E-08 -C.3627E-08 -C.3627E-08 -C.2523E-09 -C.5675E-09	-0.9967E-08 -0.7776E-08 -0.5496E-08 -0.3368E-08 -0.1594E-08 -0.3035E-09 0.4678E-09 0.6887E-09	0.1290E-09 -0.4997E-10 -0.3078E-09	0.7720E-10 -0.4027E-09 -0.6128E-09 -0.5775E-09 -0.5775E-09 -0.5770E-10 0.2254E-09 0.3966E-09 0.4021E-09

```
0.1250E 03 0.5236E 00 0.9019E 03 0.2573E 05 -0.2650E 05 0.1303E-01 0.1587E-01 -0.1336E-07 -0.7804E-08 -0.2029E-08 0.22492E-09
0.1250E 03
          0.1047E 01 0.6949E 03 0.2286E 05 -0.1652E 05 0.1263E-01 0.1575E-01 -0.1373E-07 -0.7129E-08 -0.1673E-08 -0.1731E-09
0.1250E 03 0.1571E C1 C.4873E 03 0.1725E 05 -0.1054E 05 0.1077E-01 0.1497E-01 -0.1281E-07 -0.5896E-08 -0.1240E-08 -0.4444E-09
0.1250E 03 0.2094E 01 0.3117E 03 0.1161E 05 -0.8936E 04 0.8177E-02 0.1346E-01 -0.1103E-07 -0.4432E-08 -0.7965E-09 -0.5575E-09
0.1250E 03 0.2618E 01 0.1828E 03 0.8418E 04 -0.1059E 05 0.5486E-02 0.1134E-01 -C.8831E-08 -0.2977E-08 -0.4041E-09 -0.5279E-09
0.1250E 03 0.3142E 01 0.1001E 03 0.9045E 04 -0.1321E 05 0.3153E-02 0.8865E-02 -0.6593E-08 -0.1708E-08 -0.1112E-09 -0.3913E-09
0.1250E 03 0.4189E C1 0.3238E 02 0.1916E 05 -0.1129E 05 0.3061E-03 0.4083E-02 -0.2974E-08 -0.9043E-10 0.8813E-10 -0.1247E-10
0.1250E 03 0.4712E C1 0.2470E 02 0.2395E 05 -0.4156E 04 -0.2555E-03 0.2214E-02 -0.176CE-08 0.2360E-09 0.2005E-10 0.1187E-09
0.1250E (3 0.5236E (1 0.2412E 02 (.2490E 05 0.5988E 04 -0.4039E-03 0.8121E-03 -c.9116E-09 0.2993E-09 -0.1040E-09 0.1608E-09
0.1500E 03 0.5236E 00 0.6869E 03 0.2889E 05 -0.2665E 05 0.7731E-02 0.1398E-01 -0.9775E-08 -0.4799E-08 -0.1467E-08 -0.3920E-10
0.1500E 03 0.1047E 01 0.5600E 03 0.2676E 05 -0.1728E 05 0.8449E-02 0.1423E-01 -c.1078E-07 -0.4903E-08 -0.1197E-08 -0.2922E-09
0.1500E 03 0.1571E C1 0.4183E C3 0.2235E 05 -0.1109E 05 0.7747E-02 0.1371E-C1 -0.1057E-07 -0.4332E-08 -0.8835E-09 -0.4483E-09
C.1500E 03 0.2094E 01 0.2885E 03 0.1779E 05 -0.8361E 04 0.6243E-02 0.1253E-01 -0.9547E-08 -0.3428E-08 -0.5696E-09 -0.5035E-09
0.1500E 03
          0.2618E C1 0.1855E C3
                               0.1500E 05 -0.8161E 04 0.4464E-02 0.1085E-C1 -C.8C54E-08 -0.2430E-08 -0.2926E-09 -0.4679E-09
0.1500E 03 0.3142E C1 0.1131E 03
                               0.1500E 05 -0.8647E 04 0.2799E-02 0.8857E-02 -0.6410E-08 -0.1507E-08 -0.8225E-10 -0.3641E-09
0.1500E G3 0.3665E 01 0.6747E G2
                               0.1747E 05 -0.7735E 04 0.1472E-02 0.68G8E-C2 -0.4851E-08 -0.7603E-09 0.4370E-10 -0.2244E-09
0.1500E 03
          0.4189E 01 0.4159E 02
                               0.2084E 05 -0.3929E 04 0.5593E-03 0.4906E-02 -0.3516E-08 -0.2375E-09 0.8394E-10 -0.8530E-10
0.1500E 03 0.4712E 01 0.2846E C2 0.2280E 05 0.2994E 04 0.3544E-04 0.3289E-C2 -0.2457E-08 0.6205E-10 0.5421E-10 0.2008E-10
0.1560E 03 0.5236E C1 C.2275E 02
                               0.1527E 05 0.1999E 05 -0.1751E-03 0.2024E-02 -0.1121E-08 0.1244E-09 -0.9533E-10 0.5852E-10
G.1500E 03 0.5759E C1 C.2100E 02 0.2126E 05 0.1176E 05 -0.1610E-03 0.1125E-02 -0.1670E-08 0.1680E-09 -0.1678E-10 0.7008E-10
0.1750E 03 0.5236E 00 0.5339E 03 0.3200E 05 -0.2554E 05 0.4083E-02 0.1166E-01 -0.7178E-08 -0.2605E-08 -0.1080E-08 -0.1872E-09
0.1750E 03 0.1047E 01 0.4570E 03 0.3008E 05 -0.1670E 05 0.5464E→02 0.1250E-01 -0.8602E-08 -0.3222E-08 -0.8737E-09 -0.3393E-09
0.1750E 03
          0.1571E C1 0.3592E 03 0.2631E 05 -0.1038E 05 0.5486E-02 0.1235E-C1 -0.8861E-08 -0.3103E-08 -0.6388E-09 -0.4283E-09
0.1750E G3
          C.2094E C1 0.2622E 03 0.2232E 05 -0.6878E 04 0.4689E-02 0.1151E-C1 -C.8324E-08 -0.2590E-C8 -0.4064E-09 -0.4492E-09
0.1750E 03 0.2618E 01 C.1800E C3 C.1961E 05 -0.5411E 04 0.3524E-02 0.1019E-01 -C.7305E-08 -0.1916E-08 -0.2023E-09 -0.4091E-09
0.1750E 03 0.3142E C1 0.1182E 03 0.1896E 05 -0.4476E 04 0.2330E-02 0.8566E-C2 -0.6073E-08 -0.1241E-08 -0.4630E-10 -0.3231E-09
0.1750E 03 0.3665E C1 0.7615E 02 0.2003E 05 -0.2414E 04 0.1317E-02 0.6860E-C2 -0.4835E-08 -0.6679E-09 0.4989E-10 -0.2130E-09
0.1750E 03 U.4189E C1 U.4981E 02 U.2145E 05 0.1889E 04 0.5794E-03 0.5239E-02 -C.3724E-08 -0.2459E-09 0.8526E-10 -0.1032E-09
0.1750E G3 C.4712E C1 0.3451E G2 0.2133E 05 0.8441E 04 0.1229E-03 0.3824E-02 -C.28C4E-08 0.1338E-10 0.7010E-10 -0.1629E-10
0.1750E 03 0.5236E 01 0.2620E 02 C.1803E 05 0.1600E 05 -0.9294E-04 0.2681E-02 -0.2088E-08 0.1255E-09 0.2358E-10 0.3260E-10
0.1750E 03 0.5759E C1 0.2197E 02 0.1094E 05 0.2244E 05 -0.1279E-03 0.1830E-02 -0.1564E-08 0.1205E-09 -0.3138E-10 0.3878E-10
```

TABLE I. - Continued. PLANET-EARTH FLYBY TRAJECTORIES

(b) Venus-Earth flyby trajectories

TIME	PSI	J	VX(T)	VY(T)	AX (0)	AY(C)	AXDUT(C)	AYDOT(0)	AXDOT(T)	AYDOT(T)
0.50CCE C2 0.50CCE C2	6.4189E 61 6.47126 61	C.9261E C2 G.9373E 02 G.4221E C3 G.8783E 03 G.1252E G4 G.1441E G4 G.1478E G4 G.1437E 04 G.3221E G4	-C.72C2E 05 -0.5392E 05 -0.2212E 05 -0.1519E 05 -C.2020E 05	0.2007E 05 0.2460E 05 0.1530E 05 -0.6283E 04 -0.3487E 05 -0.6221E 05 -0.7895E 05 -0.7880E 05 -0.5750E 05	0.8955E-02 -0.3607E-02 -0.1611E-01 -0.2549E-01 -0.3004E-01 -0.3038E-01 -0.2856E-01 -0.2610E-01 0.1372E-01	0.2433E-02 0.6303E-C2 0.4245E-C2 -0.2361E-02 -0.1042E-C1 -0.21C1E-C1 -0.21C1E-C1 -0.4034E-C1	0.1264E-07 0.1326E-07 0.1251E-07 0.1235E-07 -0.5724E-08	-C.1105E-08 -0.5185E-C9 0.1438E-08 0.4372E-08 C.7255E-C8 C.8988E-08 C.9406E-C8 0.8997E-08 C.2789E-08	-0.1587E-08 0.1217E-08 0.4120E-08 0.6386E-08 0.7365E-08 0.6570E-08	-0.1441E-09
C.1CCGE G3 G.1CGGE G3 C.1CGGE G3 G.1CGGE G3 G.1CGGE G3 C.1CGGE G3	C.5236E CO C.1C47E C1 C.1571E C1 C.2C94E C1 C.2C16E C1 C.3142E C1 C.3C05E C1 C.4149E C1 C.4712E C1 C.5236E C1 C.5759E C7	C.2230E 03 0.8187E C2 0.1499E U2 C.5099E 01 0.2087E 02 0.5474E 02 0.7059E 02 C.8969E 02 0.9084E 02	-0.7150E 04 -0.149CE 05 -0.2165E 05 -0.2375E 05 -0.1887E 05 -0.7049E 04 0.8920E 04 0.2429E 05 0.341JE 05	-0.8505E 04 -0.0911E 04 -0.1135E 05 -0.2043E 05 -0.3080E 05 -0.3888E 05 -0.3888E 05 -0.3106E 05 -0.1038E 05	0.1002E-01 0.6236E-02 0.2431E-02 -0.7190E-03 -0.2808E-02 -0.3809E-02 -0.3963E-02 -0.3977E-02 -0.2894E-02	0.1566E-02 0.2482E-C2 0.2C56E-C2 0.6713E-C3 -0.1238E-02 -0.3C73E-C2 -0.45C5E-C2 -0.55464E-C2 -0.599GE-C2		-0.1683E-08 -0.1125E-C8 -0.4947E-09 0.1389E-09 0.6705E-09 0.1013E-C8 0.1141E-08 C.1087E-C8 C.8964E-09	-0.1049E-08 -0.6522E-09 -0.2052E-09 0.1827E-09 0.4160E-09 0.4375E-09 0.2547E-09 -0.5958E-10 -0.4040E-09	
C.15CCE C3 O.15CCE C3 O.15CCE C3 O.15CCE C3 C.15CCE C3 C.15CCE C3 C.15CCE C3 C.15CCE C3 C.15CCE C3 C.15CCE C3	C.1571E C1 C.2094E C1 C.2618E C1 C.3142E C1 O.3605E C1 C.4149E C1 C.4712E C1 C.5236E C1	U.2150E U3 U.1210E 03 U.5595E U2 U.1935E 02 U.4127E C1 U.4127E 01 U.4330E 01 U.8577E C1 U.1257E C2	-0.1099E 04 -0.3278E 04 -0.4850E 04 -0.3627E 04 -0.100B 05 -0.100B 05 -0.1978E 05 -0.2730E 05 -0.2730E 05	-0.2212E U5 -0.1251E U5 0.4980E U3	0.5871E-02 0.3851E-02 0.2057E-02 0.6902E-03 -0.1873E-03 -0.6311E-03 -0.7505E-03 -0.6564E-03	0.3457E-C2 0.3567E-C2 0.3180E-U2 0.2367E-C2 0.1324E-C2 0.2686E-C3 -0.6379E-C3 -0.1322E-C2 -0.1776E-G2	-C.295(E-C8 -C.26(8E-G8 -C.21(6E-08 -C.1522E-08 -C.94(1E-09 -C.4367E-09 -C.5353E-10 G.2C55E-09 C.3618E-09 C.4451E-09 C.4841E-09	-0.1599E-08 -0.1208E-08 -0.8185E-09 -0.4590E-09 -0.1612E-09 0.5091E-10 0.1712E-09 0.2095E-09 0.1839E-09	-0.6674E-09 -0.5097E-09 -0.3255E-09 -0.1534E-09 -0.2670E-10 0.3431E-10 0.2836E-10 -0.2678E-10 -0.1029E-09	-0.8988E-10 -0.4754E-10 0.2753E-10 0.9984E-10 0.1394E-09 0.1303E-09
C.2COOE 03 0.2COOE 03	0.5236E CO 0.1047E C1 0.1571E C1 C.2054E C1 0.3142E C1 0.3655E C1 0.4169E C1 C.4712E C1 C.5236E C1 0.5759E C1	C.2521E 03 0.1618E 03 C.1185E C3 0.6913E 02 0.3543E 02 0.1553E C2 0.5583E 01 0.1693E 01 0.9240E C0 0.1511E 01 0.2632E 01	C.4762E U4 C.5138E 04 O.5750E 04 C.8047E 04 U.1262E 05 G.1878E 05 U.2468E 05 U.2783E 05	0.9901E U4	0.5687E-02 0.4592E-02 0.3370E-02 0.2213E-02 0.1258E-02 0.5674E-03 0.1349E-03 -0.8485E-04 -0.1497E-03	0.4223E-02 0.4653E-62 0.3634E-62 0.2952E-62 0.2220E-62 0.1434E-02 0.7258E-63 -0.2758E-03	-0.213CL-C8 -0.20C2L-08 -0.1745E-08 -0.1405E-08 -0.1048E-09 -0.7090E-09 -0.4245E-09 -0.2066E-09 -0.5172E-10 -0.5154E-10	-0.1257E-08 -0.1002E-08 -0.7410E-09 -0.2907E-09 -0.2907E-09 -0.2908E-10 0.2604E-10 0.4127E-10	-0.4583E-09 -0.3619E-09 -0.2516E-09 -0.1463E-09 -0.6243E-10 -0.1025E-10 -0.8167E-11 -0.7551E-12	0.7454E-10 -0.2990E-10 -0.8995E-10 -0.1072E-09 -0.8985E-10 -0.5201E-10 -0.1028E-10 0.2062E-10 0.3170E-10

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C.25Cue U3 C.523cE CC C.1936E C3 C.7197E O4 -U.319ze U5 C.4298E-02 U.4395E-C2 -C.1579E-08 -C.1036E-08 -0.3779E-09 0.9558E-10
C.25Cue u3 c.1047E c1 c.1491E c3 C.1012E u5 -0.2732E u5 0.4025E-02 0.43C6E-C2 -0.1567E-08 -0.9254E-C9 -0.3282E-09 0.5631E-11
v.25Ccc U3 C.1571E C1 C.1C57E C3 C.1172E U5 -U.2570E U5 U.3430E-02 0.4076E-C2 -U.144CE-U8 -C.77C3E-O9 -U.2589E-O9 -U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589E-U.2589
U.2500c 03 C.2044c C1 C.6004E 02 C.1320E 05 -U.2135E 05 U.2672E-02 0.3663E-C2 -C.1236E-U8 -C.5970E-09 -U.1822E-09 -0.9500E-10
U.25002 03 0.20188 C1 0.41196 C2 0.15756 05 -0.19378 05 0.18978-02 0.31458-02 -0.95528-09 -0.42706-09 -0.10938-09 -0.10438-09
U.2560E U3 U.3142E C1 U.2260E U2 U.1947E 05 -U.1656E U5 0.1215E-02 U.2519E-02 -U.752EE-09 -C.2767E-09 -0.4953E-10 -0.9181E-10
U.25CUE U3 U.36U5L C1 U.113dE 02 C.2374E U3 -U.1167E U5 0.6842E-Ú3 0.1878E-U2 -U.5353E-U9 -U.1568E-U9 -U.9119E-11 -0.6565E-10
C.25CUE US C.4189E C1 U.528UE C1 C.2698E U5 -0.4C52E U4 0.3181E-03 U.128EE+C2 -C.3563E-09 -C.7120E-10 U.1633E-10 -0.3543E-10
6.2500E to 0.4712E (1 0.2340E )1 6.2725E 05 0.5772E 04 0.9872E-04 0.7834E-63 -0.2186E-09 -0.1860E-10 0.1186E-10 -0.9920E-11
0.25666 03 0.52366 01 0.11436 01 0.23696 05 0.16046 05 -0.56386-05 0.3d626-03 -0.11626-09 0.60446-11 0.18266-11 0.50536-11
U.25CCE GS C.5759E C1 C.63C3E UG C.1424E U5 U.2419E U5 -0.2849E-04 U.1613E-C3 -0.482GE-10 U.9216E-11 -0.1231E-10 U.7406E-11
U-3U(UE U3 U-5236E CO (.1510E C3 U.1144E O5 -U-3293E O5 U-2771E~U2 0.41C6E-C2 -C-1196E-C8 -C-6866E-C9 -0-2819E-O9 0.3013E-10
G.3CCJE G3 C.1C47E C1 G.1222E G3 C.1484E G5 -U.2797E G5 U.2799E-G2 -C.1252E-G8 -0.6575E-G9 -U.2412E-G9 -0.2879E-10
C.3CCUE US C.1071E C1 C.9175E UZ C.1099E UD -U.2360E U5 U.2516L-UZ U.3873E-C2 -C.12CZE-C8 -C.5736E-C9 -U.1883E-09 -0.6984E-10
0.5060e (3 (.20)44e 01 0.641ze 02 0.1885E 05 -0.2005e 05 0.2053E-02 0.3541E-02 -0.1078E-08 -0.4618E-09 -0.1313E-09 -0.9148E-10
U.30CUE U3 U.2018E U1 U.4191E U2 U.2114E 05 -0.1057E 05 U.1529E-02 U.3091E-02 -0.9122E-09 -0.3429E-09 -0.7768E-10 -0.9489E-10
0.3000t to 1.3142t C1 t.2578t C2 t.2398t C5 
v.3Cbug U3 U.3cbbe C1 U.1566e G2 C.2668e U5 -C.6229e U4 U.63U9E-U3 U.2C31e-U2 -G.5625e-U9 -C.14U5E-U9 -0.2535E-11 -0.6275E-10
U.30CUE U3 C.4189E C1 U.8473E U1 U.2791E U5 U.1849E U4 0.3330E~03 U.1523E-C2 -C.414EE-09 -U.7156E-10 0.1385E-10 -0.3879E-10
G.3CCLE U3 C.4712L C1 C.4684E C1 C.2012E U5 U.1129E U5 U.1394E~03 0.1679E-C2 -C.255CE-G9 -U.2599E-10 0.1745E-10 +0.1742E-10
U.30CUL U3 C.5236E U1 U.2628E U1 U.2628E U1 U.2627E U5 0.2040E C5 0.3263E~U4 0.7168E-03 -C.2C28E-09 -0.1C88E-11 0.1221E-10 -0.2717E-11
C.3CCCE C3 C.5759L C1 C.1565E C1 C.1041E C5 C.2690E C5 C.4854E-C5 C.4357E-C3 -C.1345E-C9 C.7349E-11 0.2974E-11 0.3659E-11
0.3500g U3 0.5236E CC 0.1150E U3 C.1544E U5 -0.3291E U5 0.1698E-02 U.3627E-C2 -0.9214E-U9 -0.4288E-09 -0.2139E-09 -0.5538E-11
U.350UE U3 U.1047E U1 U.1011E U3 C.1895E 05 -U.2760E U5 0.19U6E-U2 0.3692E-02 -C.1018E-08 -0.4530E-09 -0.4806E-U9 -0.4511E-10
C.35CGL U3 C.1571E C1 C.7933E C2 C.2128E O5 -0.2200E O5 0.1823E-02 C.3576E-C2 -C.1C1EE-C8 -C.4183E-C9 -0.1390E-09 -0.7176E-10
C.35000 03 0.20946 01 0.58366 02 0.23146 05 -0.18156 05 0.15566-02 0.33176-02 -0.94596-09 -0.34996-09 -0.95206-10 -0.84436-10
C.35CUE C3 C.2618E C1 0.4053E C2 C.25C4E 05 -0.1361E 05 0.1203E-02 0.2545E-C2 -0.825EE-C9 -0.2677E-09 -0.5436E-10 -0.8409E-10
€.3500€ €3 €.3142€ €4 €.2602E 02 €.2761E 05 €.8295E 04 €.8459E~03 €.2512E-62 €.66542E-09 €0.1864E-09 €0.2670E-10 €0.7330E-10
0.35600E C3 0.3665E C1 0.1712E 02 0.2839E 05 -0.1576E 04 0.5354E-03 0.2054E-02 -0.55584E-09 -0.1156E-09 0.3075E-11 -0.5580E-10
U.35CGE L3 U.4189E (1 C.1070E UZ C.28L3E U5 U.6637E U4 U.2963E~03 0.1613E−02 −C.4354E−09 −0.6649E−10 U.1612E−10 −C.3598E−10
C.35tuE U3 C.4712E C1 C.6672E C1 C.2468L U5 C.1558E U5 C.1324E-U3 C.1219E-02 -C.3315E-09 -C.2233E-10 C.1959E-10 -U.1792E-10
0.35CUE C3 C.5236E C1 C.4230E U1 C.1762E U5 U.2304E U5 0.35CUE-U4 U.88863E-C3 -C.2463E-C9 C.1068E-12 0.1616E-10 -0.4569E-11
0.35000 03 0.57596 01 0.27806 01 0.71036 04 0.28776 05 -0.99186-05 0.62676-03 -0.16466-09 0.95636-11 0.92046-11 0.27546-11
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TABLE I. - Continued. PLANET-EARTH FLYBY TRAJECTORIES

(c) Mars-Earth flyby trajectories

TIME	PSI	J	VX(T)	VY(1)	AX (O)	AY(C)	AXDOT(G)	AYDOT(O)	AXDOT (T)	(T)TOGYA
0.5000E 02 0.5000E 02 0.5000E 02	0.1047E C1 0.1571E C1 C.2094E C1 0.2010E C1 C.3142E C1 C.3605E C1	0.6140E 03 0.1571E 04 0.2768E 04 0.3868E 04 0.4355E 04 0.5271E 04 0.4921E 04 0.3973E 04	3 -0.3850E U5 3 -0.5087E 05 4 -0.8171E 05 4 -0.1215E U6 4 -0.1215E 06 4 -0.1212E 06 -0.125E 06 -0.128E 06 -0.8367E U5 4 -0.8367E U5	0.2857E U5 U.3321E U5 U.2311E U5 -U.1201E U4 -U.38V0E U5 -U.1642E U5 -U.4512E U5 -U.57V3E U5	-0.2048E-01 -0.3246E-01 -0.4437E-01 -0.5294E-01 -0.5613E-01 -0.5006E-01 -0.4269E-01 -0.3150E-01	0.4918E-C2 0.84C7E-C2 0.566CE-C2 -0.2C45E-C2 -0.1C65E-C1 -0.32C7E-C1 -0.3851E-C1 -0.4094E-C1	C.3133E-08 C.5413E-08 G.8575E-08 G.1185E-07 G.1185E-07 G.1545E-07 G.113CE-07 G.113CE-07 G.8253E-08 C.5265E-08	-0.8376E-C9 -0.1310E-C8	0.2421E-08 0.4446E-08 0.7239E-08 0.1008E-07 0.1226E-07 0.1318E-07 0.1307E-07 0.7505E-08 0.4599E-08	-0.1465E-08 -0.2595E-08 -0.2367E-08 -0.9851E-09
0.506.JE 62 0.1060E 63 0.1000E 63	0.5759E 01 0.5236E 00 0.1047E 01	0.1390E 04	4 -0.3914E UD 2 -0.2531E U5 2 -0.3302E U5	-0.4200E 04	-0.1141E-C1 -0.9984E-05 -0.2319E-02	-0.2840E-C1 -0.4171E-C2 -0.1869E-C2	C.3C68E-08 C.73S6E-10 C.4393E-09	0.6019E-08 C.3450E-C9 0.2065E-09	0.2492E-08 -0.7741E-10 0.1705E-09	0.6980 E-08 0.5571 E-09 0.1714E-09
C.1000c 05 C.1000c 05 C.1000c 03 C.1000c 03	0.1671E C1 0.2094E C1 0.2618L C1 0.3142E C1 0.3605E C1 0.4169E C1	0.1746E C. 0.287CE O. 0.3662E C. 0.3990E C. 0.3975E C.	2 -0.4341E 05 3 -0.5257E 05 3 -0.5025E 05 3 -0.5080E 05 3 -0.3477E 05 3 -0.1035E 05	-0.5484E 04 -0.1957E 05 -0.3743E 05 -0.5385E 05 -0.6255E 05	-0.8408E-02 -0.1063E-01 -0.1165E-01 -0.1164E-01 -0.1111E-01	-0.1158E-C2 -0.2643E-C2 -0.4464E-C2 -0.5941E-C2 -C.6883E-C2	C.\$4C2E-C9 C.1461E-U8 C.1673E-C8 O.2C61E-O8 C.21C3E-O8 C.2C35E-C8	0.2223E-C9 0.4083E-C9 0.7114E-09 0.1009E-08 0.1189E-08 0.1237E-C8	0.9226E-09 0.1242E-08 0.1385E-08 0.1244E-08 0.7939E-09	-0.6455E-10 -0.1177E-09 0.2154E-10 0.3525E-09 0.8094E-09 0.1217E-08
0.1660E 03 0.1660E 03 0.1660E 03	0.4712E C1 0.5236E C1 0.5759E C1	U.3650E C	3 0.1670E 05 3 -0.3713E 05 3 -0.2735E 05 2 -0.2210E 05	-0.2811E 05 -0.2303E 05	0.4238E-03	-0.1277E-61 -0.1042E-01	C.1569E-08 C.2743E-C9 C.8172E-12		0.1358E-09 0.3329E-09 -0.1813E-11 -0.1751E-09	0.1387E-08 0.1821E-08 0.1479E-08
0.1500E 03 C.1500E 03 0.1500E 03 0.1500E 03 0.1500E 03	0.1047E C1 0.1571E C1 0.2094E C1 0.2618E 01 0.3142E C1	0.1733E U. C.4756E C C.1602E C C.3891E C C.6102E G	2 C. 2542E U5 1 C. 30C5E C5 2 C. 3326E U5 2 C. 3224E U5 2 C. 3224E U5 2 C. 1149E C5	-0.9163E 04 -0.1071E 05 -0.1668E 05 -0.2609E 05 -0.3636E 05	0.8216E-03 0-0.6415E-03 0-0.2091E-02 0-0.3213E-02 0-0.3840E-02	-0.1524E-02 -0.5765E-03 -0.1033E-02 -0.1551E-02 -0.2261E-02			-0.1067E-09 0.6138E-11 0.1345E-09 0.2448E-09 0.3015E-09 0.2777E-09	0.1593E-09 0.5496E-10 0.1235E-10 0.3641E-10 0.1188E-09 0.2293E-09
6.15CUE U3 C.15CUE U3 C.15CUE U3 U.15CUE U3	0.4189E U1 0.4712E C1 0.5230E U1	U.8U39E 0 U.7944E C U.7587E C	2 C.5906E U4 2 C.2279E 05 2 U.3441E U5 3 -U.2596E 05	-0.4455E 05 -0.3720E 05 -0.2297E 05	5 -0.3820E-02 5 -0.3470E-02 5 -0.3045E-02	-0.3385E-C2 -0.3676E-C2 -0.3827E-C2	C.6287E-09 C.6CCCE-09 O.5662E-09	0.4011E-09 0.3825E-09 0.3404E-09	0.17326-09	0.3200 E-09 0.3480 E-09 0.2930 E-09 0.6474 E-09
C.2CUOE US C.2CUOE US C.2CUCE US	0.5236E 00 0.1047E 01 0.1571E 01 0.2054E 01 0.2618E 01 0.3142E 01 0.3605E 01 0.4712E 01 0.5236E 01 0.5755E 01	C.2691E C C.7768E U C.1764E U C.4668E C O.1115E U C.1717E C C.2697E C C.2256E C C.2294E U	2 C.2678E US	-0.1600E 05 -0.1800E 05 -0.268E 05 -0.2907E 05 -0.3496E 05 -0.3444E 05 -0.3444E 05 -0.2503E 06 -0.1098E 05	0 0.1702E-02 0 0.7858E-03 5 -0.1278E-03 5 -0.8722E-03 5 -0.1350E-02 5 -0.1555E-02 5 -0.1597E-02 5 -0.1397E-02 5 -0.1172E-02	-0.8699E-C3 -0.5425E-C3 -0.5375E-C3 -0.788CE-C3 -0.1163E-C2 -0.1533E-C2 -0.1820E-C2 -0.20CCE-C2 -0.2083E-C2	-C.1725E-G9 -C.6657E-10 C.4481E-10 C.142CE-G9 G.21(&E-G9 C.2478E-09 C.253GE-G9 G.2535E-G9 O.2413E-09	-0.7069E-10 -C.3284E-10 0.1662E-10 0.1161E-09 0.1161E-09 0.1452E-09 0.1544E-09 0.1245E-09	-0.1271E-09 -C.7696E-10 -0.1611E-10 0.3932E-10 0.7329E-10 0.7497E-10	0.1779E-10 0.4271E-10 0.8004E-10 0.1104E-09 0.1176E-09 0.9437E-10

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0.2500E U3 0.5236E C0 0.5760E 02 -0.1916E U5 -0.2034E U5 0.2471E-U2 -0.6935E-03 -0.2495E-09 -0.1424E-09 +0.1265E-09 0.1383E-09
0.2500E 03 0.1047E 01 0.3188E 02 -0.1783E 05 -0.2081E 05 0.1926E-02 -0.3256E+03 -0.1950E+09 -0.1122E-09 -0.1152E-09 0.8235E-10
C.250UE 03 C.1571E C1 0.1388E C2 -C.1680E 05 -0.2276E 05 0.1268E-02 -0.1276E-C3 -C.1257E-09 -0.7739E-10 -0.8746E-10 0.3869E-10
C.2500E L3 L.2094E C1 0.4123E U1 -C.1452E 05 -U.2627E U5 0.6068E-03 -U.1255E-C3 -C.5184E-10 -0.3919E-10 -0.5151E-10 0.1210E-10
0.2560E 03 0.2618E 01 0.9376E 00 -0.9524E 04 -0.3042E 05 0.4630E-04 -0.2843E-03 0.1541E-10 -0.1525E-11 -0.1672E-10 0.3885E-11
C.25COE L3 C.3142E C1 0.1632E U1 -C.1299E 04 -U.3333E U5 -0.3489E-03 -0.5252E-C3 C.6746E-10 0.3011E-10 0.8041E+11 0.1104E-10
C.2500E U3 U.3co5E C1 C.3747E C1 C.9521E 04 -U.3285E 05 -0.5663E-03 -0.7816E-C3 0.1C11E-09 0.5131E-10 0.1695E-10 0.2614E-10
C.25CUE U3 U.4189E C1 U.5784E 01 0.2074E 05 -0.2737E 05 -0.6335E-03 -0.9877E-C3 C.1183E-09 0.6055E-10 0.9930E-11 0.3947E-10
0.250vE 03 0.471zf (1 0.7220E 01 0.2931E 05 -0.1679E 05 -0.5948E-03 -0.1125E-02 0.1237E-09 0.5903E-10 -0.7276E-11 0.4295E-10
0.25tuz (3 0.5236E t1 0.8198E 01 0.3237E 05 -0.2927E 04 -0.4935E-03 -0.1191E-C2 0.1226E-09 0.4922E-10 -0.2581E-10 0.3310E-10
0.25CUE U3 C.5759E C1 C.9287E U1 0.2838E 05 0.1080E 05 -0.3690E-03 -0.1196E-C2 C.12C6E-09 0.3371E-10 -0.3717E-10 0.1080E-10
C.3660E C3 0.5236E CU 0.5386E CZ -0.1764E U5 -0.2359E 05 0.2327E-02 -0.1463E-03 -0.2363E-09 -0.1554E-09 -0.1665E-09 0.1005E-09
0.3660-10 0.1047E C1 0.3341E 62 -0.1487E 05 -0.2442E 05 0.1903E-02 0.7958E-C4 -0.1917E-09 -0.1260E-09 -0.1003E-09 0.5936E-10
C.3LCUE U.3 U.1571E (1 C.1772E C2 -C.1223E 05 -U.2605E 05 0.1397E-02 0.1923E-C3 -C.1421E-09 -C.9488E-10 -0.8208E-10 0.2630E-10
C.3CCUE U3 U.2U94E C1 0.7592E 01 -0.8514E 04 -0.2848E 05 0.8839E-03 0.1764E-03 -0.8831E-10 -0.6302E-10 -0.5741E-10 0.4629E-11
C.3CODE U3 U.2618E C1 C.2395E 01 -0.2678E 04 -0.3084E 05 U.4347E-03 0.5144E-04 -C.376CE-10 -0.3295E-10 -0.3234E-10 -0.4787E-11
0.3100€ 03 0.3142E 01 0.6383E 00 0.5567E 04 -0.3156E 05 0.9693E-04 -0.1355E-03 0.4133E-11 -0.7771E-11 -0.1253E-10 -0.3777E-11
0.3000E 03 0.3005E 01 0.7315E 00 0.1535E 05 -0.2893E 05 -0.1158E-03 -0.3323E-03 0.3411E-10 0.1007E-10 -0.1696E-11 0.3264E-11
C.3000E C3 C.41d9E C1 0.1510E C1 0.2467E 05 -0.21d5E 05 -0.2177E-03 -0.5000E-03 C.5279E-10 0.1978E-10 -0.2475E-12 0.1068E-10
0.3CCCE 03 0.4712L C1 0.2372E C1 0.3087E 05 -0.1058E 05 -0.2373E-03 -0.6193E-03 0.6268E-10 0.2214E-10 -0.5230E-11 0.1374E-10
C.3CCUL V3 C.5236E CI V.3167E V1 C.3159E 05 V.3V16E 04 -0.2V56E-03 -0.6866E-C3 C.671CE-10 V.1890E-10 -0.1178E-10 V.1029E-10
C.3CCUE 03 0.5759E (1 0.4C56E (1 C.2575E 05 0.1577E 05 -0.1534E-03 -0.7C87E-C3 C.6584E-10 C.1226E-10 -0.1508E-10 0.9414E-12
C.3500E C3 C.5236E C0 C.4948E U2 -0.1594E 05 -0.2632E 05 0.2116E-02 0.2453E-C3 -C.2C76E-C9 -0.1527E-09 -0.9129E-10 0.7503E-10
0.350CE 03 (.1047E 01 0.3302E 02 -0.1206E 05 -0.2719E 05 0.1781E-02 0.3703E-03 -0.1798E-09 -0.1263E-09 -0.8690E-10 0.4285E-10
G.35CUL G. 0.1571E C1 C.1958E C2 -C.8258E 04 -G.2837E 05 0.1379E-02 0.4244E-C3 -C.1427E-09 -C.9881E-10 -O.7333E-10 0.1669E-10
C.3500E 03 C.2094E 01 C.1006E 02 -C.3564E 04 -0.2980E 05 0.9649E-03 0.3897E-03 -C.1014E-09 -C.7150E-10 -0.5458E-10 -0.1119E-11
C.3500c U3 U.2cide C1 C.4317E C1 C.2779E 04 -0.3069E 05 0.5932E-03 0.2774E-C3 -C.6128E-10 -0.4616E-10 -0.3493E-10 -0.9957E-11
0.3500E 03 0.3142E 01 0.1487E 01 0.1084E 05 -0.2971E 05 0.3005E-03 0.1191E-03 -0.2674E-10 -0.2481E-10 -0.1833E-10 -0.1103E-10
C.350LE C3 C.3665E C1 C.4984E CC 0.1969E C5 -U.2549E O5 0.1001E-03 -0.4640E-C4 -C.1842E-12 -C.8981E-11 -0.7436E-11 -0.7187E-11
0.3560E U3 0.4189E C1 0.4556E CU 0.2745E 05 -0.1729E U5 -0.1531E-04 -0.1960E-03 0.1821E-10 0.8502E-12 -0.2774E-11 -0.2093E-11
0.35600E 03 C.4712E C1 C.7992E 00 0.3177E 05 -0.5612E 04 -C.66475E-04 -0.3C77E-C3 C.2581E-10 C.5266E-11 -0.2743E-11 0.1125E-11
0.3500E C3 0.5236E C1 0.1282E 01 0.3071E 05 0.7644E 04 -0.7115E-04 -0.3797E-03 0.3680E-10 0.5569E-11 -0.4446E-11 0.9365E-12
0.3500E 03 0.5759E 01 0.1667E 01 0.2350E 05 0.1950E 05 -0.5822E-04 -0.4172E-03 0.4175E-10 0.3484E-11 -0.4904E-11 -0.2351E-11
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TABLE I. - Continued. PLANET-EARTH FLYBY TRAJECTORIES

(d) Jupiter-Earth flyby trajectories

TIML	PSI	J	Vx(1)	VY(T)	AX (O)	AY(C)	AXBUT(C)	AYDOT(O)	AXDOT(T)	AYDOT(T)
0.2000	0.4712E (1 0.523CE (1	U. 2453E U. 2991E U. 3590E U. 4074E U. 4299E U. 4299E U. 4354E U. 4354E U. 3520E Ü. 3150E C	3 - 0.0435 ± 05 3 - 0.0649 E 05 3 - 0.739 E 05 3 - 0.735 U 05 3 - 0.735 U 05 3 - 0.735 U 05 3 - 0.8107 E 05 3 - 0.8107 E 05 3 - 0.820 E 05 3 - 0.820 E 05 3 - 0.820 E 05	-0.1292E 04 -0.3128E 04 -0.9827E 04 -0.2231E 05 -0.4107E 05 -0.6299E 05 -0.1935E 04 -0.9837E 04 -0.1225E 05	-U.6633E-02 -U.7371E-02 -0.8094E-U2 -C.8660E-U2 -U.8776E-02 -0.8720E-02 -U.7981E-02 -U.752E-02 -U.6594E-02	-0.8749E-C3 -0.64CCE-C3 -0.7826E-G3 -0.121CE-C2 -0.1695E-C2 -0.2C17E-C2 -0.3665E-C2 -0.3795E-C2 -0.3559E-C2	0.3654E-09 0.4264E-09 0.4666E-09 0.5173E-09 0.5528E-09 0.5652E-09 0.5617E-09 0.5682E-09 0.4634E-09 0.4176E-09 0.3642E-09	0.8501E-10 0.5723E-10 0.4992E-10 C.6605E-10 C.1003E-C9 C.1355E-C9 0.1534E-09 0.1846E-C9 C.1994E-09 G.1918E-09 0.1641E-09	0.3034E-09 0.3363E-09 0.3838E-09 0.4367E-09 0.4860E-09 0.5125E-09 0.4635E-09 0.4621E-09 0.3993E-09 0.3452E-09 0.3076E-09	-0.1563E-10 -0.3014E-10
C.3CUCL C3 C.3CUCC C3 C.3CCCC C3 C.3CCCC C3 C.3CCCC C3 C.3CCCC C3 C.3CCCC C3 C.3CCCC C3 C.3CCCC C3 C.3CCCC C3	0.1047E 01 0.1571E 01 0.2054E 01 0.2618E 01 0.3142E 01 0.3605E 01 0.4189E 01 0.4712E 01 0.5236E 01	C. 6273E 0 C. 75356 0 C. 9691E C C. 1114E 0 C. 1114E 0 C. 1127E 0 C. 1105E 0 C. 1145E 0	2 - C. 4 8 8 4 E	-0./654E U4 -0.1106E 05 -0.17d5E U5 -0.2817E 05 -0.4696E 05 -0.5304E 05 -0.5965E 05 -0.2117E 04 -0.6558E U4	-0.2715E-02 -0.3040E-02 -0.3356E-02 -0.3578E-02 -0.3663E-02 -0.3637E-02 -0.3570E-02 -0.2950E-02 -0.2661E-02	-0.8191E-03 -0.6666E-03 -0.7325E-03 -0.8867E-03 -0.1076E-02 -0.1228E-02 -0.1326E-02 -0.2186E-02 -0.2057E-02	C.1145E-09 C.1257E-09 C.141CE-U9 C.1562E-09 C.1672E-09 C.1714E-09 C.17C4E-09 C.136CE-09 C.136CE-09 C.1228E-09 C.1132E-09	0.4117E-10 C.3405E-10 C.3274E-10 C.3780E-10 C.4718E-10 0.5656E-10 0.6221E-10 C.6387E-10 C.7072E-10 C.6928E-10 C.6218E-10	0.6898E-10 0.7918E-10 0.5520E-10 0.1142E-09 0.1323E-09 0.1413E-09 0.1285E-09 0.8689E-10 0.1101E-09 0.88820E-10 0.7322E-10	0.3790E-10 0.1710E-10 0.1936E-11 -0.4914E-11 0.9491E-12 0.2566E-10 0.6759E-10 0.1096E-09 0.1127E-09 0.8444E-10
C.4CCCE C3 0.4000E C3 0.4000E C3 0.4000E C3 C.4000E C3	C.5236E CU U.1U47E C1 U.1571E C1 C.2C54E C1 G.2618E C1 U.3665E C1 U.4189E C1 U.4712E C1 U.5236E O1 G.5759E C1	0.2263E C 0.2637E C 0.3182E C 0.4013E C 0.4116E C 0.5562E C 0.5015E C	02 - C. 42 L d E U5 02 - U. 42 7 d E U5 03 - U. 42 7 d E U5 03 - U. 42 5 2 E U5 03 - U. 42 5 2 E U5 04 - U. 2983 E U5 05 - U. 4893 E U5 05 - U. 4893 E U5 05 - U. 486	-0.1181E U5 -U.16U9E U5 -U.2274E U5 -U.4078E U5 -U.4078E U5 -U.48U9E U5 U.1116E U5 U.2337E U4 -0.3336E U4	-0.1350 E-02 -0.1534E-02 -0.1713E-02 -0.1841E-02 -0.1895E-02 -0.1565E-02 -0.1565E-02 -0.1286E-02	-0.6742E-03 -0.5930E-03 -0.5972E-03 -0.6658E-03 -0.7599E-13 -0.8450E-03 -0.1475E-02 -0.1481E-02 -0.1441E-02	C.4697E-10 G.5220E-10 C.5915E-10 C.66C2E-10 C.71C4E-10 C.7322E-10 C.73CCE-10 C.59C6E-10 C.5448E-10 C.4542E-10 C.4568E-10	0.2240E-10 0.1993E-10 C.1974E-10 0.2194E-10 0.2564E-10 0.2928E-10 0.3159E-10 0.3082E-10 C.3269E-10 C.3244E-10 C.3001E-10	0.1943E-10 0.2379E-10 0.3134E-10 0.4062E-10 0.4931E-10 0.5352E-10 0.4879E-10 0.5952E-10 0.4496E-10 0.3239E-10 0.2355E-10	0.2378 E-10 0.1271E-10 0.4442E-11 0.6328E-12 0.3182E-11 0.1327E-10 0.2871E-10 0.5598 E-10 0.6033E-10 0.5660E-10 0.4769E-10
0.5000E 03 0.5000E 0	0.523cE CO 0.1C47E C1 C.1571E C1 C.2C94E C1 C.2618E C1 U.3142E C1 U.3665E C1 U.4189E C1 U.4712E C1 C.5236E C1 G.5755E C1	0.101UE (0.1112E (0.1327E (0.1556E (0.1723E (0.1795E (0.1787E (0.1732E (0.1732E (0.2329E (02 -0.3d50E 05 02 -0.3d50E 05 02 -0.3d732E 05 02 -0.3d791E 05 02 -0.2957E 05 02 -0.2032E 05 02 -0.7197E 04 02 0.2337E 05 02 -0.4256E 05 02 -0.44573E 05	-0.1493E U5 -0.1971E U5 -0.2608E U5 -0.3352E U5 -0.4055E U5 -0.4449E U5 -0.4449E U5 -0.3804E U5 -0.1377E U4	-0.7252E-03 -0.8465E-03 -0.9642E-03 -0.1051E-02 -0.1092E-02 -0.1091E-02 -0.1015E-02 -0.6545E-03	-0.5473E-C3 -0.4871E-C3 -0.479E-C3 -0.5137E-C3 -0.5668E-C3 -0.6190E-C3 -0.6602E-C3 -0.6692E-C3 -0.6892E-C3	C.2237E-10 C.2537E-10 C.2527E-10 C.3312E-10 C.36C1E-10 C.3743E-10 C.3751E-10 C.3577E-10 C.3573E-10 C.2277E-10 C.22113E-10	0.1293E-10 0.1198E-10 0.1210E-10 0.1329E-10 0.1512E-10 0.1688E-10 0.1799E-10 0.1798E-10 0.1788E-10 0.1695E-10	0.4814E-11 0.6910E-11 0.1103E-10 0.1625E-10 0.2109E-10 0.2349E-10 0.2149E-10 0.4237E-11 0.1484E-10 0.8691E-11	0.1675E-10 0.9869E-11 0.4635E-11 0.2060E-11 0.3016E-11 0.7633E-11 0.1442E-10 0.2038E-10 0.2239E-10 0.3606E-10 0.3112E-10

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0.6LCUE C3 L.5236E C0 0.6528E 01 -0.3631E 05 -0.1333E 05 -0.3224E-03 -0.5247E-03 C.113CE-10 0.7568E-11 -0.2903E-12 0.1270E-10
0.60CUE 03 0.1047E 01 0.5392E 01 -0.3505E 05 -0.1743E 05 -0.3926E-03 -0.4451E-03 0.1329E-10 0.7248E-11 0.7228E-12 0.7973E-11
0.60CUE C3 C.1571E C1 C.54C9E 01 +C.3313E C5 -0.2248E 05 -0.4809E-03 -0.3978E-C3 C.158CE-10 C.7477E-11 0.3153E-11 0.4286E-11
0.6000E 03 0.2094E (1 0.6229E 04 -0.2953E 05 -0.2852E 05 -0.5669E-03 -0.3865E-03 0.1828E-10 0.8248E-11 0.6351E-11 0.2294E-11
0.6000E Co 0.3142E C1 0.8247E 01 -0.1358E 05 -0.4026E 05 -0.6665E-03 -0.4361E-03 0.2128E-10 0.1031E-10 0.1093E-10 0.4628E-11
C.66CCE C3 C.3665E C1 C.8751E 01 -0.9821E 03 -0.4267E 05 -0.6700E-03 -0.4701E-03 C.2149E-10 0.1091E-10 C.1008E-10 0.7887E-11
C.6600E U3 C.4189E (1 C.8842E 01 C.1303E U5 -U.4047E U5 -U.6502E-03 -0.4982E-C3 C.211CE-10 C.1102E-10 0.6638E-11 0.1057E-10
C.66000 (3 0.4712E C1 0.1783E 02 -0.4140E 05 0.6974E 04 -0.3669E-03 -0.8395E-C3 C.12C3E-10 0.8863E-11 0.1395E-10 0.2576E-10
0.6CLUE U3 C.5236E C1 0.1516E 02 -0.4072E 05 -0.2038E 03 -0.3186E-03 -0.7966E-C3 C.1C9CE-10 0.9116E-11 0.7933E-11 0.2525E-10
C.600LE U2 C.5759E C1 C.1192E U2 -0.3918E U5 -0.5544E U4 -0.2862E-03 -0.72C1E-03 C.1C16E-10 C.8841E-11 0.3285E-11 0.2224E-10
C.8CCUE L3 L.5236E CO 0.3027E 01 -0.3364E 05 -0.1641E 05 -0.3120E-04 -0.3450E-03 C.2469E-11 0.2205E-11 -0.2955E-11 0.8324E-11
0.8000E 03 0.1047E 01 0.2527E 01 -0.3097E 05 -0.2132E 05 -0.7813E-04 -0.2963E-03 0.3604E-11 0.2331E-11 -0.2833E-11 0.5594E-11
C.8CUUE L3 L.1571E (1 C.1976E C1 -0.2733E U5 -U.2652E U5 -U.1349E-03 -U.2647E-C3 C.496CE-11 0.2633E-11 -0.1874E-11 0.3337E-11
0.8000 € 63 0.2694E 01 0.1891E 01 -0.2201E 05 -0.3189E 05 -0.1906E-03 -0.2525E-03 0.6317E-11 0.3099E-11 -0.4317E-12 0.1879E-11
0.80000 U3 0.2018E 01 0.2088E 01 -0.1438E 05 -0.3659E 05 -0.2352E-03 -0.2566E-03 0.7437E-11 0.3630E-11 0.1013E-11 0.1381E-11
C.8CCUE U3 C.3142E (1 C.2371E C1 -C.43C7E 04 -U.3952E U5 -U.2626E-03 -U.27C4E-G3 G.8167E-11 0.4084E-11 G.1933E-11
                                                                                                         0.1733E-11
G.86CUE U3 0.3665E C1 0.2665E C1 0.7552E 04 -0.3925E 05 -0.2714E-03 -0.2867E-03 0.8476E-11 0.4339E-11 0.1954E-11
                                                                                                         0.2492E-11
C.8(COE C3 U.4189E C1 C.2741E C1 C.1965E U5 -U.34/8E U5 -U.2643E-03 -C.3CCEE-C3 C.8435E-11 C.4333E-11 0.1058E-11
                                                                                                         0.3012E-11
0.8153E-11 0.4060E-11 -0.3590E-12 0.2697E-11
C.8LCUE to 0.5236E tl 0.2887E 01 t.3646E to -0.1456E 05 -0.2182E-03 -0.3148E-03 c.7729E-11 0.3516E-11 -0.1633E-11 0.1190E-11
C.dudue 03 0.5759E 01 0.7018E 01 -0.3778E 05 -0.5953E 04 0.6321E-05 -0.4599E-03 0.1526E-11 0.2152E-11 0.1929E-13 0.1346E-10
0.1000E U4 0.1047E 01 0.1914E 01 -0.2800E U5 -0.2433E U5 0.5059E-C4 -0.1956E-C3 0.2542E-12 0.1190E-12 -0.3374E-11 0.4143E-11
C.1CCCE C4 C.1571E C1 C.1291E C1 -C.2311E C5 -C.2937E C5 C.8175E-C5 -C.1735E-C3 C.1152E-11 0.4374E-12 -C.2951E-11 0.2514E-11
G.10COE 04 C.2C94E C1 0.9713E 00 -0.1662E 05 -0.3396E 05 -0.3379E-04 -0.1634E-C3 0.2C61E-11 0.8067E-12 -0.2163E-11 0.1326E-11
G.1000E L4 0.2618E C1 0.8803E L0 -0.0180E 04 -0.3738E 05 -0.0892E-04 -0.1638E-C3 C.2849E-11 C.1176E-11 -0.1287E-11 0.6678E-12
C.1CCGE C4 C.3142E C1 U.9210E 00 U.2094E 04 -0.3859E 05 -0.9296E-04 -0.17C6E-C3 C.3424E-11 0.1476E-11 -0.6046E-12 0.4749E-12
U.1000E 04 0.3005E C1 0.1009E C1 (.1338E 05 -0.3651E 05 -0.1045E-03 -0.1797E-03 C.3752E-11 0.1645E-11 -0.3670E-12 0.5220E-12
0.1000E 04 0.4189E 01 0.1104E 01 0.2419E 05 -0.3052E 05 -0.1046E-03 -0.1875E-03 0.3857E-11 0.1649E-11 -0.4009E-12 0.4940E-12
G.1600E 04 0.4712E C1 0.1202E 01 0.3271E 05 -0.2093E 05 -0.9538E-04 -0.1926E-63 0.3769E-11 0.1476E-11 -0.6907E-12 0.1076E-12
0.1000E 04 0.52366 01 0.1338E 01 0.37486 05 -0.9125E 04 -0.7926E-04 -0.1924E-03 0.3608E-11 0.1120E-11 -0.8452E-12 -0.8112E-12
C.1CCCE G4 C.5755E C1 C.16C5E G1 C.3809E 05 C.2515E 04 -C.6054E-04 -C.187CE-C3 C.3466E-11 C.5091E-12 -C.4729E-12 -C.2817E-11
```

TABLE I. - Continued. PLANET-EARTH FLYBY TRAJECTORIES

(e) Earth-Saturn flyby trajectories

TIME	051	J	VX(T)	VY(T)	AX(O)	AY (O)	AXDOT(0)	AYDOT(O)	AXDOT(T)	AYDOT(T)
0.4000E 03 0.4000E 03 0.4000E 03 0.4000E 03 0.4000E 03 0.4000E 03 0.4000E 03 0.4000E 03	0.52365 00 0.10475 01 0.105717 01 0.20947 01 0.26185 01 0.31425 01 0.46557 01 0.52365 01 0.57597 01	0.1195F 0 0.1319F 0 0.1454F 0 0.1557F 0 0.1603F 0 0.1602F 0 0.1475F 0	3 -0.47835 3 -0.70135 3 -0.71575 3 -0.70215 3 -0.63075 3 -0.46585 3 -0.71655 3 -0.68775	05 -0.4971F 0.05 -0.5898F 0.05 -0.9121F 0.05 -0.1563F 0.05 -0.2640F 0.05 -0.4193F 0.05 -0.4560F 0.05 -0.4260F 0.05 -0.5415F 0.05 -0.5415F 0.05	4 -0.3252F-02 4 -0.3434E-02 5 -0.3611F-02 5 -0.3733E-02 5 -0.3775F-02 5 -0.3758E-02 3 -0.3416F-02 4 -0.3242F-02	-0.4840E-03 -0.4225E-03 -0.4538E-03 -0.5542E-03 -0.6697E-03 -0.7510E-03 -0.1223E-02 -0.1162E-02	0.9668E-10 0.1010E-09 0.1070E-09 0.1129E-09 0.1171E-09 0.1185E-09 0.1181E-09 0.1007E-09 0.9651E-10	0.1846E-10 0.1502F-10 0.1413E-10 0.1610F-10 0.2019F-10 0.2432F-10 0.2650F-10 0.3260F-10 0.3169E-10 0.2826F-10	0.7554E-10 0.7999E-10 0.8686E-10 0.9528E-10 0.1043E-09 0.1096E-09 0.9970E-10 0.9047E-10 0.8210E-10 0.7651E-10	-0.6146E-11
0.4000E 03	0.52367 00 0.10477 01 0.15719 01 0.2046 01 0.26187 01 0.36650 01 0.41909 01 0.47127 01 0.52365 01	0.3202E 0 0.3409E 0 0.3845E 0 0.4127E 0 0.4276E 0 0.4230E 0	02 -0.51445 02 -0.51875 02 -0.51025 02 -0.47305 02 -0.24525 02 -0.48465 02 -0.48465 02 -0.15585	05 -0.7645E 0 05 -1.1047E 0 05 -1.1499E 0 05 -0.2191E 0 05 -0.3106E 0 05 -0.4185E 0 05 -1.5165E 0 04 -1.5664E 0 05 -0.5936E 0	5 -0.1368F-02 5 -0.1447E-02 5 -0.1523F-02 5 -0.1576F-02 5 -0.1586F-02 5 -0.1588F-02 5 -0.1589F-02 5 -0.1379E-02	-0.3787F-03 -0.3456E-03 -0.3514F-03 -0.3861E-03 -0.4309E-03 -0.4691F-03 -0.4956E-03	0.2900E-10 0.3038F-10 0.3222E-10 0.3403F-10 0.3529F-10 0.3574E-10 0.3559F-10 0.2478E-10 0.5639E-10	0.8586E-11 0.7696E-11 0.7516F-11 0.8101E-11 0.9190F-11 0.1028F-10 0.1097E-10 0.1119F-10 0.4035E-11	0.3038E-10 0.2779E-10 0.1933E-10 -0.5050E-10	0.7261E-11 0.3317E-11 0.2132E-12 -0.1371F-11 -0.2567E-12 0.4900E-11 0.1364F-10 0.2241E-10 0.4446E-09 0.1068E-08
0.8000F 03 0.8000F 03 0.8000F 03 0.8000F 03 0.8000F 03 0.8000F 03 0.8000F 03 0.8000F 03	0.5236F 00 0.1047F 01 0.1571F 01 0.2004F 01 0.2618F 01 0.3142F 01 0.3665F 01 0.5752F 01	0.1207F (0.1300F (0.1423F (0.1532F (0.1598F (0.1615F (0.1758F (0.1577F (0.1	02 -0.4305F 02 -0.4305F 02 -0.4062F 02 -0.3541F 02 -0.2631F 02 -0.11935F 02 -0.4673F	75 -0.9638E 0 75 -0.1363E 0 75 -0.1363E 0 75 -0.1887F 0 75 -0.2565E 0 75 -0.3366E 0 75 -0.4174E 0 75 -0.4274F 0 75 0.8290F 0 75 0.1939F 0 75 -0.2672E 0	5 -0.7099E-03 5 -0.7547E-03 5 -0.7977T-03 15 -0.8279E-03 5 -0.8403E-03 15 -0.8368E-03 14 -0.6936E-03	-0.2967F-03 -0.2741E-03 -0.2727F-03 -0.2874F-03 -0.3094F-03 -0.3307F-03 -0.5069E-03 -0.4852F-03	0.1220F-10 0.1283F-10 0.1365F-10 0.1444E-10 0.1501E-10 0.1523E-10 0.1307E-10 0.1247E-10 0.1203E-10	0.4704E-11 0.4384F-11 0.4339E-11 0.4579E-11 0.4997E-11 0.5417E-11 0.6015E-11 0.5976F-11	0.5322E-11 0.6011E-11 0.7331E-11 0.9061E-11 0.1075E-10 0.1158E-10 0.1061E-10 0.1031E-10 0.7919E-11	0.4529F-11 0.2383E-11 0.7217F-12 -0.7052E-13 0.4600F-12 0.2566E-11 0.5780E-11 0.1146E-10 0.1072E-10 0.9027E-11
0.1000F 04 0.1000F 04 0.1000F 04 0.1000F 04 0.1000F 04 1.1000F 04 0.1000F 04 0.1000F 04 0.1000F 04	0.5236F 00 0.1047F 01 0.1571F 01 0.2044F 01 0.2618F 01 0.3665F 01 0.4199F 01 0.4271F 01 0.5236F 01	0.5533F (0.5828F (0.6330F (0.6831F (0.7172F	01 -0.3970F 01 -0.3775F 01 -0.3415F 01 -0.2792F 01 -0.1837F 01 -0.5592F 01 0.9165F 01 0.2352E 03 0.5574F	05 -0.1129F 0 05 -0.1606F 0 05 -0.2169F 0 05 -0.2327F 0 05 -0.3531F 0 06 -0.4159F 0 04 -0.4530F 0 04 -0.4566F 0 05 -0.3880F 0 05 -0.5626F 0	15 -0.4079E-02 15 -0.4373E-03 15 -0.4656E-07 15 -0.4860E-03 15 -0.4952E-03 15 -0.4938E-03 15 -0.4716E-03 15 -0.4716E-03 15 -0.4849E-07	3 -0.2373E-03 3 -0.2204E-03 3 -0.2165E-03 3 -0.2231E-03 3 -0.2353F-03 3 -0.2483F-03 3 -0.2595E-03 3 -0.2685F-03 3 -0.8413E-03		0.2809E-11 0.2677E-11 0.2672E-11 0.2796F-11 0.2997F-11 0.3195E-11 0.3361E-11 0.3315E-11 -0.3502E-10 -0.3324E-10		0.3219E-11 0.1880E-11 0.8423E-12 0.3297E-12 0.5386F-12 0.1498E-11 0.2904E-11 0.4142F-11 0.4580E-11 0.2109E-08 0.1267E-08

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0.12000 04 0.52367 00 0.3093F 01 -0.3871E 05 -0.1272E 05 -0.2289F-03 -0.2148E-03 0.3350E-11 0.1756E-11 0.3712E-12 0.2472E-11
0.1200F 04 0.1047F 01 0.2915F 01 -0.3689F 05 -0.1802E 05 -0.2461F-03 -0.1933E-03 0.3582E-11 0.1701F-11 0.5171E-12 0.1554E-11
0.1200F 04 0.1571F 01 0.2972F 01 -0.3410F 05 -0.2386F 05 -0.2675F-03 -0.1797F-03 0.3870F-11 0.1712E-11 0.9459E-12 0.8295E-12
1.12005 04 0.20945 01 0.31905 01 -0.29595 05 -0.30195 05 -0.28815-03 -0.17515-03 0.41505-11 0.17885-11 0.15395-11 0.43815-12
0.12005 04 0.24135 01 0.34245 01 -0.2262E 05 -0.3643F 05 -0.3035F-03 -0.1780E-03 0.4360E-11 0.1901E-11 0.2104E-11 0.4764E-12
0.1200F 04 0.2142F 01 0.3616F 01 -0.1277E 05 -0.4139E 05 -0.3111E-03 -0.1851F-03 0.4468E-11 0.2009E-11 0.2396E-11 0.9257F-12
0.12005 04 0.36655 01 0.37125 01 -0.40395 03 -0.43565 05 -0.31095-03 -0.19355-03 0.44765-11 0.20765-11 0.2045-11 0.15905-11
0.1200F 04 0.4189F 01 0.3711F 01 0.1319F 05 -0.4156F 05 -0.3046E-03 -0.2011E-03 0.4413F-11 0.2085E-11 0.1487E-11 0.2136E-11
0.1200F 04 0.5759F 01 0.4138F 01 -0.4111F 05 -0.2202F 04 -0.2198F-03 -0.2667E-03 0.3208E-11 0.1939E-11 0.1143E-11 0.4289E-11
9.1400F 04 0.5236F 00 0.1938F 01 -0.3721F 05 -0.1402F 05 -0.1368E-03 -0.1763E-03 0.1939E-11 0.1116F-11 -0.1563E-12 0.1994E-11
0.1400F 04 0.1047F 01 0.1728F 01 -0.3482F 05 -0.1968F 05 -0.1505F-03 -0.1594E-03 0.2107E-11 0.1099F-11 -0.1108E-12 0.1318E-11
0.1400F 04 0.1571F 01 0.1683F 01 -0.3133F 05 -0.2560F 05 -0.1673E-03 -0.1483F-03 0.2310E-11 0.1118F-11 0.1448E-12 0.7698E-12
0.1400F 04 0.2094F 01 0.1754F 01 -0.2611F 05 -0.3166F 05 -0.1835E-03 -0.1436E-03 0.2508E-11 0.1172E-11 0.5229E-12 0.4422E-12
0.1400F 04 0.26185 01 0.1874F 01 -0.1877F 05 -0.3722E 05 -0.1959F-03 -0.1445F-03 0.2662F-11 0.1244E-11 0.8923E-12 0.3893E-12
0.14005 04 0.31425 01 0.19855 01 -0.85215 04 -0.41175 05 -0.20255-03 -0.14885-03 0.27495-11 0.13105-11 0.10985-11 0.58575-12
0.14005 04 0.36655 01 0.20535 01 0.35445 04 -0.42185 05 -0.20315-03 -0.15435-03 0.27675-11 0.13475-11 0.10205-11 0.90245-12
0.1400F 04 0.4180F 01 0.2074F 01 0.1631F 05 -0.3919F 05 -0.1987F-03 -0.1596F-03 0.2731F-11 0.1345F-11 0.6422E-12 0.1138F-11
0.1420F 04 0.5759F 01 0.2749F 01 -0.4012F 05 -0.2373F 04 -0.1274F-03 -0.2160E-03 0.1810E-11 0.1190E-11 0.5422E-12 0.3283E-11
0.1600F 04 0.5236F 00 0.1339F 01 -0.3605F 05 -0.1521F 05 -0.7861F-04 -0.1463E-03 0.1145E-11 0.7041E-12 -0.3809E-12 0.1661E-11
0.1600F 04 0.10477 01 0.1142F 01 -0.3317F 05 -0.2110F 05 -0.9016F-04 -0.1327F-03 0.1274F-11 0.7065F-12 -0.3922F-12 0.1136F-11
0.1600F 04 0.1571 01 0.1053F 01 -0.2908F 05 -0.2704F 05 -0.1040F-03 -0.1233F-03 0.1428E-11 0.7298E-12 -0.2393E-12 0.6965E-12
0.1600F 04 0.2094F 01 0.1055F 01 -0.2328F 05 -0.3291F 05 -0.1174E-03 -0.1188E-03 0.1579E-11 0.7729E-12 0.1222E-13 0.4088E-12
0.1600F 04 0.2618F 01 0.1107F 01 -0.1531E 05 -0.3778F 05 -0.1279F-03 -0.1186E-03 0.1700E-11 0.8247E-12 0.2688E-12 0.3068E-12
0.1600F 04 0.3142F 01 0.1168F 01 -0.5110F 04 -0.4090F 05 -0.1340E-03 -0.1212F-03 0.1773F-11 0.8690F-12 0.4264E-12 0.3687E-12
0.1600F 04 0.3665F 01 0.1218F 01 0.6708F 04 -0.4101F 05 -0.1352E-03 -0.1250F-03 0.1797F-11 0.8915E-12 0.4098F-12 0.5067E-12
0.1600F 04 0.4189F 01 0.1243E 01 0.1884F 05 -0.3725F 05 -0.1322E-03 -0.1287E-03 0.1778E-11 0.8840E-12 0.2127E-12 0.5910E-12
0.1600F 04 0.4712F 01 0.1259E 01 0.2952F 05 -0.2963E 05 -0.1260F-03 -0.1319E-03 0.1729E-11 0.8440E-12 -0.9083E-13 0.4981E-12
0.1690F 04 0.5236F 01 0.1284F 01 0.3681E 05 -0.1982E 05 -0.1172F-03 -0.1343E-03 0.1664E-11 0.7567E-12 -0.4383E-12 0.3558E-13
0.1600F 04 0.5759F 01 0.2009F 01 -0.3949F 05 -0.2720F 04 -0.6914E-04 -0.1778E-03 0.1027E-11 0.7212E-12 0.2519E-12 0.2626E-11
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01 UNITCS, EDF. REC= 00000 FIL=

TABLE I. - Continued. PLANET-EARTH FLYBY TRAJECTORIES

(f) Uranus-Earth flyby trajectories

Time	PSI	J	VX(1)	VY(T)	AX (0)	AY (C)	AXDOT(C)	A YDOT (O)	(T) TDDXA	AYCOT(T)
G.44CUE US G.4CUE US G.4CUE US G.4CCUE US	U.5236c Ul	L.50C4E L3 C.5898E C3 C.6198E C3 C.6495E C3 C.6495E C3 C.642CE C3 C.66C4ZE C3 C.66C4ZE C3 C.5694E L3	-0.1268E U6 -0.1299E U6 -0.1327E Ü6 -0.1333E U6 -0.1159E U6 -0.153E U6 -0.1362E U6 -0.1270E C6	-0.1284E 04 -0.2934E 04 -0.7883E 04 -0.1852E 05 -0.4242E 05 0.1361E 04 -0.3852E 04 -0.5015E 04		-0.2559E-C3 -0.2C67E-C3 -0.2518E-C3 -0.3758E-C3 -0.512CE-C3 -0.5449E-C3 -0.9259E-C3 -0.9767E-C3 -0.5175E-C3	C.2CC3E-09 C.2C44E-C9 C.21CCE-09 C.2157E-09 C.2157E-09 C.213E-09 C.23CE-09 C.215EE-09 C.215EE-09 C.21CCE-G9 C.2CC3E-G9	C.1171E-10 0.7895E-11 0.6642E-11 0.8380E-11 0.1269E-10 0.1738E-10 0.1509E-10 U.2563E-10 0.2735E-10 0.261CE-10 0.2228E-10	0.2050E-09	0.8905E-11 0.1675E-11 -0.3885E-11 -0.8097E-11 -0.1078E-10 0.8458E-11 0.6208E-11 0.6208E-10 0.4147E-10 0.3798E-10 0.2551E-10
0.8000E U3 0.8000E U3 0.8000E U3	0.5236E CO C.1047E C1 C.1071E C1 C.2C94E C1 C.2018E C1 C.3142E C1 C.3465E C1 C.4712E C1 C.5230E C1 C.5230E C1 C.5759E C1	0.6/10E 02 0.7032E 02 0.7309E 02 0.7616E 02 0.7718E 02 0.7703E 02 0.7624E 02 0.7506E 02 0.6542E 02	-U.769E U5 -U.7169E U5 -U.7189E U5 -U.6239E U5 -U.6239E U5 -U.6239E U5 -U.7340E U5 -U.7340E U5 -U.737E U5	-0.7179E 04 -0.1101E 05 -0.1744E 05 -0.2764E 05 -0.4241E 05 -0.5952E 05 0.4137E 05 0.4137E 05	4 -U.1682E-02 4 -U.1716E-02 5 -O.1701E-02 5 -O.1804E-02 5 -U.1834E-02 5 -U.183E-02 5 -U.183E-02 5 -U.1799E-02 4 -U.1757E-02 2 -U.1714E-02 4 -U.1681E-02	-0.2070E-C3 -0.1514E-C3 -0.1950E-C3 -0.2237E-C3 -0.2523E-C3 -0.2727E-C2 -0.3853E-C3 -0.3770E-C3	C.253&t-10 C.2591E-10 C.2644E-10 C.2737E-10 C.2737E-10 C.2787E-10 C.2766E-10 C.2766E-10 C.2658E-10 C.2536E-10 C.2536E-10	C.3569E-11 C.3135E-11 C.302CE-11 C.3260E-11 C.3759E-11 C.4260E-11 C.5119E-11 C.5350E-11 C.5234E-11 C.4802E-11	0.2361E-10 0.2544E-10	-0.8300 E-12 -0.1938 E-11 -0.1700 E-11 0.2079 E-11 0.1034 E-10 0.9855 E-11 0.9313 E-11 0.7976 E-11
0.1166E 64 0.1060E 04 C.1660E 04 G.1660E 04 C.1660E 04 C.1660E 04 C.1660E 64 C.1660E 64 G.1660E 64	C.5236E CO C.1047E C1 C.1571E C1 C.2694E C1 C.2618E C1 C.3142E C1 C.3605E C1 C.4189E C1 C.4712E C1 C.5236E C1 C.5236E C1	0.3340E	-U.6040E U5 -C.6075E 05 -L.5085E 05 -C.5085E 05 -C.4889E U5 -C.3399E U5 -C.6265E U5 -C.6229E U5 -U.6138E 05	-0.9061E U-0.1350E C-0.2033E U-0.3000E U-0.5513E U-0.5513E U-0.6574E U-0.6574E U-0.6574E U-0.1630E U-0.163	4 -0.1062E-02 4 -0.1084E-02 5 -0.1112E-02 5 -0.1139E-02 5 -0.1158E-02 5 -0.1161E-02 5 -0.1161E-02 5 -0.1138E-02 4 -0.1081E-02 4 -0.1081E-02 4 -0.1061E-02	-0.1765E-03 -0.1655E-03 -0.1688E-03 -0.1828E-03 -0.1999E-03 -0.2136E-03 -0.3927E-03 -0.2989E-03 -0.2880E-03	C.13C5E-10 C.1336E-10 C.1374E-10 C.141E-10 C.1436E-10 C.144E-10 C.1441E-10 C.146E-10 C.1333E-10 C.13C7E-10	C.2345E-11 C.2135E-11 C.2084E-11 U.2206E-11 C.2447E-11 C.2689E-11 C.2833E-11 C.4197E-11 C.3210E-11 O.3159E-11	0.1057E-10 0.1156E-10 0.1270E-10 0.1338E-10 0.1229E-10 0.1274E-10 0.1121E-10 0.1026E-10	0.5081E-12 -0.4815E-12 -0.1089E-11 -0.7796E-12 0.1311E-11 0.5261E-11 0.7120E-11 0.5913E-11
C.12COE C4 C.12COE C4 C.12COE C4 U.12COE C4 C.12COE C4 C.12COE C4 C.12COE C4 C.12COE C4 C.12COE C4 C.12COE C4 C.12COE C4	C.5236E CU C.1647E C1 C.1671E C1 C.2618E C1 C.2618E C1 C.3142E C1 C.3665E C1 C.4189E C1 C.4112E C1 C.5236E C1 C.5759E C1	0.1873E 02 0.1954E 02 0.2643E 02 0.2110E 02 0.2143E 02 0.2142E 02 0.2083E 02 0.2079E 02	-G.>388E 05 -G.5368E 05 -G.5225E 05 -G.4821E 05 -G.3981E 05 -G.2565E 05 -G.6509E 04 -G.144CE 05 -G.3771E 65	-U.1061E U -U.150UE 0 -U.2255E U -U.3168E 0 -U.4237E 0 -U.5230E 0 -U.5787E U -U.6115E 0	4 -0.7258E-03 5 -0.7405E-03 5 -0.7599E-03 5 -0.7784E-03 5 -0.7910E-03 5 -0.7953E-03 5 -0.7951E-03 5 -0.7867E-03 5 -0.7844E-03 5 -0.7844E-03 5 -0.7835E-03	-0.1523E-03 -0.143EE-C3 -0.1451E-C3 -0.1537E-C3 -0.1646E-C3 -0.1745E-C3 -0.1822E-C3 -0.1878E-C3	C.7626E-11 C.7765E-11 C.8CCFE-11 C.8216E-11 C.8262E-11 C.8469E-11 C.8367E-11 C.8215E-11 C.8474E-11 C.8476E-11	C.1968E-11 O.1886E-11 O.1867E-11	0.5687E-11 0.6375E-11 0.7133E-11 0.7548E-11 0.6950E-11 0.5444E-11 0.4594E-12 0.1608E-12	0.1199E-11 0.3982E-12 -0.2666E-12 -0.6263E-12 -0.3623E-12 0.8936E-12 0.3049E-11 0.5456E-11 -0.464E-12 0.1949E-13 -0.4756E-13

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0.1400E 04 0.5236E 00 (.1116E 02 -0.4967E 05 -0.7780E 04 -0.5230E-03 -0.1464E-03 C.4822E-11 0.1209E-11 0.2766E-11 0.9232E-12
0.140LE (4 0.1047E 01 0.1141E 02 54.4944E 05 -0.1192E 05 -0.5337E-03 -0.1331E-03 0.4528E-11 0.1140E-11 0.2953E-11 0.3405E-12
0.14CGE C4 0.1571E C1 0.1187E U2 -0.4874E C5 -0.1729E 05 -0.5479E-03 -0.1263E-C3 0.5C6EE-11 0.1126E-11 0.3312E-11 -0.1292E-12
0.14006 04 0.20946 01 0.12396 02 -0.40686 05 -0.24306 05 -0.56136-03 -0.12646-03 0.52026-11 0.11686-11 0.38106-11 -0.35966-12
G.1400E 04 C.2018E C1 C.1280E CZ -0.4199E 05 -0.3295E 05 -0.5704E-03 -0.1319E-C3 C.5293E-11 0.1246E-11 0.4334E-11 -0.1575E-12
C.1466E 64 6.314ZE 61 0.136E 62 -0.33ZE 05 -0.4234E 05 -0.5737E-03 -0.1396E-03 C.53Z4E-11 0.1326E-11 0.4606E-11 0.4606E-11 0.6426E-12
C.1400E C4 C.4189E C1 U.1290E U2 -U.1965E U4 -U.5394E U5 -U.5670E-03 -U.1526E-C3 C.5274E-11 0.1404E-11 0.3113E-11 0.3140E-11
0.14CUE 04 0.4712E 01 0.1288E 02 -0.512UE 05 0.9933E 04 -0.5433E-03 -0.2002E-03 0.5013E-11 0.1489E-11 0.3879E-11 0.2935E-11
C.1400E t4 t.5236E (1 t.1223E 02 -t.51t7E 05 t.3909E 04 -0.5308E-03 -0.1936E-C3 t.4894E-11 0.1476E-11 0.3309E-11 0.2639E-11
U.14CUE (4 0.5759L C1 0.1163E G2 -0.5047E 05 -0.5840E 03 -0.5216E-03 -0.18G4E-03 C.48C6E-11 G.1409E-11 0.2936E-11 0.2138E-11
C.16CGE 04 0.5236E 00 0.7245E 01 -0.4676E 05 -0.8488E 04 -0.3914E-03 -0.1283E-C3 C.3241E-11 0.9187E-12 0.1633E-11 0.7457E-12
0.1600E 04 0.1047E 01 0.7375E 01 -0.4623E 05 -0.1305E 05 -0.3997E-03 -0.1177E-03 0.3314E-11 0.8754E-12 0.1769E-11 0.3060E-12
C.16C0E t4 0.1571E t1 0.7652E 01 -0.4510E 05 -0.1869E 05 -0.4105E-03 -0.1119E-03 0.340EE-11 0.8665E-12 0.2038E-11 -0.4044E-13
C.16CLE 04 C.2C94E C1 C.79a0E 01 -0.4249E 05 -0.2571E 05 -0.42∪7E-03 -0.1114E-03 C.3499E-11 0.8935E-12 0.2407E-11 -0.1999E-12
C.16CUE L4 C.2610L C1 C.8240E C1 -0.3726E C5 -0.3392E C5 -0.4277E-C3 -0.115CE-C3 C.356CE-11 C.9434E-12 0.2782E-11 -0.5176E-13
0.16Cue u4 0.3142E 01 0.8391E 01 -0.2827E 05 -0.4231E 05 -0.4303E-03 -0.1206E-03 0.3582E-11 0.9947E-12 0.2971E-11 0.4801E-12
C.16LUL 04 0.3E03E 01 0.84C0E 01 -0.13C1E 05 -0.4887E 05 -0.4291E-03 -0.1261E-C3 C.3573E-11 0.1030E-11 0.2741E-11 0.1294E-11
v.lc(Cc t4 t.4189c t1 t.88636 v1 -t.4626c 05 v.1928c 05 -0.41416-03 -0.17136-03 C.34256-11 C.10686-11 0.31326-11 0.21046-11
C.16CUE 04 0.4712E 01 0.8464E 01 -0.48C2E 05 0.1110E 05 -0.4057E-03 -0.1711E-03 0.3356E-11 0.1095E-11 0.2569E-11 0.2215E-11
C.16CLE t4 C.5236E t1 t.8035E 01 -6.4819E 05 0.4696E 04 -0.3966E-03 -0.1655E-(3 C.3281E-11 C.1088E-11 0.2108E-11 0.2025E-11
C.1600E 04 0.5759E 01 0.7612E 01 -0.4774E 05 -0.2642E 03 -0.3899E-03 -0.1551E-€3 0.3226E-11 0.1046E-11 0.1797E-11 0.1662E-11
C.2(CCE t4 t.5236E to t.3476E t1 -0.4258E t5 -0.9723E t4 -0.2371E-03 -0.1C18E-C3 C.166CE-11 0.5698E-12 0.6238E-12 0.5359E-12
0.2000E 04 0.1047E 01 0.3502E 01 -0.4192E 35 -0.1491E 05 -0.2426E-03 -0.9447E-04 0.1699E-11 0.5503E-12 0.6963E-12 0.2637E-12
6.2000E 04 0.1571E 01 0.3512E 01 -0.4004E 05 -0.2091E 05 -0.2495E-03 -0.9007E-04 0.1750E-11 0.5468E-12 0.8540E-12 0.540E-12 0.5402E-13
0.2000E 04 0.2094E 01 0.3755E 01 -0.3555E 05 -0.2785E 05 -0.2561E-03 -0.8900E-04 0.1798E-11 0.5597E-12 0.1068E-11 -0.3985E-13
C.20tue t4 t.26tet t1 t.3edzé č1 -0.3t5te 05 -0.3532E 05 -0.2et7é-03 -0.9t62t-C4 C.1831t-11 C.5830E-12 0.1276E-11 0.3415E-13
C.20CUE 04 0.3142E 01 0.3959E 01 -0.2117E 00 -0.4220E 05 -0.2025E-03 -0.9373E-04 C.1844E-11 0.6071E-12 0.1378E-11 0.2898E-12
0.2000E t4 t.3cc5E t1 t.3476E t1 -t.3441E 04 -0.4685E 05 -0.2618E-03 -0.5719E-04 C.184CE-11 C.6239E-12 0.1272E-11 0.6590E-12
          C.4169E (1 U.3945E C1 U.6511E U4 -U.4734E U5 -U.2592E-03 -0.1004E-03 C.1825E-11 C.6307E-12 0.9350E-12 0.9952E-12
0.20CUE 04 0.47126 01 0.41846 01 -0.43890 05 0.12756 05 -0.24446-03 -0.13136-03 0.17046-11 0.64766-12 0.13176-11 0.13846-11
0.2000 04 0.5236 01 0.3956 01 -0.4454 05 0.5790 04 -0.2392E-03 -0.1272E-03 0.1670E-11 0.6461E-12 0.1601E-11 0.1303E-11
C.2060E 04 C.5759E C1 C.3725E 01 -0.4450E 05 0.5564E 02 -0.2355E-03 -0.1266E-C2 C.1646E-11 0.6278E-12 0.7735E-12 0.1097E-11
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TABLE I. - Continued. PLANET-EARTH FLYBY TRAJECTORIES

(g) Neptune-Earth flyby trajectories

TIME	PSI	J	VX(T)	VY(T)	AX (U)	AY(C)	AXDUT(L)	AYDOT(O)	AXDOT(T)	AYDOT(T)
0.4000E 03	0.1571b C1 0.2094b C1 0.26186 C1 0.3142b C1 0.3605b C1 0.4712b C1 0.4712b C1 0.523cb C1	0.1422E	4 -0.1934E U6 4 -0.1958E U6 4 -0.1991E U6 4 -0.2021E U6 4 -0.2017E U6 4 -0.2047E U6 4 -0.2024E U6 4 -0.1992E 06 4 -0.1992E 06 4 -0.1934E U6	0.6951E 03 -0.1368E 03 -0.3944E 04 -0.1317E 05 -0.4250E 05 0.8283E 04 -0.1372E 04 -0.5289E 04 -0.6161E 04	-0.1110E-01 -0.1128E-01 -0.1147E-C1 -0.1160E-01 -0.1165E-01 -0.1160E-01 -0.1147E-01 -0.1128E-01 -0.1110E-01	-0.1444E-C3 -C.5285E-C4 -0.1411E-C3 -0.2726E-O3 -0.4154E-C3 -0.67C3E-C3 -0.8C11E-C3 -0.8C1E-C3 -0.7578E-C3	C.3162E-C9 C.3223L-C9 C.3276E-G9 C.3333E-09 C.3375E-09 C.33876E-C9 C.33874E-C9 C.3323E-09 C.3223E-09 C.3223E-09 C.3162E-09	0.8252E-11 C.4346E-11 0.2983E-11 U.4585E-11 U.8824E-11 C.1364E-10 O.1846E-10 C.2266E-10 C.2266E-10 O.2290E-10 O.1899E-10		-0.4220 E-11 -0.7304E-11 -0.1131E-10 0.1262E-10 0.3710E-10 0.3434E-10 0.3149E-10 0.2718E-10
0.80C0E 03	0.1047E C1 0.1571E C1 C.2654E 01 0.2618E C1 C.3142E C1 0.3665E C1 0.4185E C1 C.4712E C1 0.5236E C1	C.1754E C C.1810E C U.1867E C U.1907E C C.1922E C C.1886E C G.1831E C O.1772E C	3 - 0.1 C19E 06 3 - 0.1 C19E 06 3 - 0.1 C31E 06 3 - 0.1 C47E 06 3 - 0.1 C59E 06 3 - 0.1 C53E 06 3 - 0.1 C63E 06	-0.4191E 04 -0.6874E 04 -0.1226E 05 -0.2257E 05 -0.4249E 05 -0.1825E 05 0.7142E 04 0.1439E 04 -0.1379E 04	-0.2761E-02 -0.2807E-02 -0.2853E-C2 -0.2884E-02 -0.2894E-02 -0.2851E-02 -0.2807E-02 -0.2761E-02	-0.1521E-03 -0.1382E-C3 -0.1487E-C3 -0.1776E-C3 -0.2698E-03 -0.2925E-C3 -0.3213E-C3 -0.3178E-C3	0.3998E-10 0.4050E-10 0.4121E-10 0.4152E-10 0.4244E-10 0.4240E-10 0.4240E-10 0.415E-10 0.4140E-10 0.3998E-10	0.2741E-11 0.2275E-11 0.2131E-11 0.2358E-11 0.2888E-11 0.3439E-11 0.3916E-11 0.4428E-11 0.4652E-11 0.4042E-11	0.3899E-10	0.4193E-12 -0.9486E-12 -0.2214E-11 -0.2808E-11 0.1614E-11 0.8571E-11 0.8789E-11 0.7751E-11
C.1CCUE U4 G.1CGUE U4 C.1CGUE U4 G.1CGUE U4	0.1047E C1 C.1571E C1 U.2U94E C1 O.2018E C1 C.3142E C1 G.3E65E C1 C.4189E C1 C.5236E C1	C.8894E C.9172E C.9453E C.9454E C.972CE C.9699E C.9608E C.9902E C.9002E C.9002	02 - C.8452E	-0.5706E U4 -0.9047E C4 -0.1500E U5 -0.2532E 05 -0.4253E 05 -0.6515E U5 -0.9325E 05 0.1865E 03	-0.1761E-02 -0.1790E-02 -0.1819E-02 -0.1838E-02 -0.1844E-02 -0.1847E-02 -0.1847E-02 -0.1760E-02	-0.1341E-03 -0.1248E-C3 -0.1306E-63 -0.1480E-03 -0.1673E-03 -0.1802E-03 -0.1823E-03 -0.2412E-03	C.2C54E-10 C.2C81E-10 C.2117E-10 C.2154E-10 C.2188E-10 C.2188E-10 C.2162E-10 C.223CE-10 C.2C6CE-10	0.1838E-11 0.1606E-11 0.1539E-11 0.1659E-11 0.1924E-11 0.2190E-11 0.2336E-11 0.2721E-11 0.2490E-11	0.1947E-10 0.2052E-10 0.2135E-10 0.2026E-10	0.2371E-12 -0.6870E-12 -0.1480E-11 -0.1603E-11 0.7667E-11 -0.1623E-11 0.4190E-11
C.12CUE C4 C.12CUE U4 C.12CUE U4 C.12CUE U4 C.12CUE U4 C.12CUE U4 C.12CUE U4 C.12CUE U4 C.12CUE U4 C.12CUE U4 C.12CUE U4	0.1647E C1 C.1571E C1 C.2094E C1 U.2618E C1	C.5091E C.5245E C.5462E C.5515E C.55548E C.5548E C.5548E C.5342E C.5342E	02 -0.7334E 05 02 -0.7402E 05 02 -0.7403E 05 02 -0.7403E 05 02 -0.7269E 05 02 -0.6553E 05 02 -0.4937E 05 02 -0.7602E 05 02 -0.7560E 05 02 -0.7453E 05 02 -0.7453E 05	-0.6968E 04 -0.1085E 05 -0.1721E 05 -0.2737E 05 -0.4249E 05 -0.6033E 05 0.1221E 05 0.5353E 04 0.1223E 04	-0.1218E-02 5-0.1238E-02 5-0.1257E-02 5-0.1270E-02 5-0.1274E-02 5-0.1275E-02 -0.1255E-02 4-0.1236E-02 -0.1217E-02	2 -0.1183E-03 2 -0.1115E-03 -0.1150E-03 2 -0.1261E-03 2 -0.1389E-03 2 -0.1479E-03 2 -0.1972E-03 2 -0.1972E-03 2 -0.1937E-03	C.1163E-10 C.1205E-10 C.123CE-10 C.1251E-10 C.1266E-10 C.127CE-10 C.127CE-10 C.1245E-10 C.1225E-10 C.1208E-10 C.1193E-10	0.1313E-11 C.1183E-11 0.1147E-11 0.1218E-11 0.1366E-11 0.1514E-11 0.1588E-11 C.1777E-11 C.1846E-11 0.1810E-11 0.1681E-11	0.1099E-10	0.1414E-12 -0.5141E-12 -0.1022E-11 -0.9675E-12 0.7233E-12 0.4521E-11 0.3851E-11 0.3532E-11 0.2951E-11

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C.16CUE C4 C.5230E LU C.2055E U2 -0.0013E C5 -0.5725E 04 -0.6690E-03 -0.1C4CE-C? C.5C7CE-11 0.7598E-12 0.3700E-11 0.4808E-12 C.16CUE C4 C.1C47E C1 C.2094E U2 -0.6643E U5 -0.9013E U4 -0.6773E-03 -0.9449E-C4 C.5137E-11 C.7086E-12 0.3823E-11 0.7194E-13
C.166UE 04 1.1571E 01 0.2153E 02:-0.6658E 05 -0.1371E 05 -0.6882E-03 -0.9011E-04 0.5228E-11 0.6959E-12 0.4055E-11 -0.2905E-12
C.16tue C4 0.2094E C1 0.2215E 02 -0.5972E C5 -0.2056E C5 -0.6987E-03 -0.9133E-04 0.5317E-11 0.7252E-12 0.4403E-11 -0.5178E-12
U.1600E 04 0.2018E 01 0.2260E 02 -0.5641E 05 -0.3020E 05 -0.7057E-03 -0.9669E-04 0.5376E-11 0.7829E-12 0.4825E-11 -0.3943E-12
U.16CUE L4 U.314ZE (1 U.2279E UZ -U.485JE C5 -U.4247E U5 -U.7080E-03 -0.1C33E-C3 U.5394E-11 0.8411E-12 U.5083E-11 0.4030E-12
C.16CLL L4 C.36o5E C1 C.2275E U2 -U.3394E U5 -U.55U1E U5 -U.7U65E-U3 -0.1C88E-C3 C.53E2E-11 0.8779E-12 0.4754E-11 0.1870E-11
C.1600e 04 0.4189e 01 0.2270E 02 -0.6147E 05 0.1558E 05 -0.6967E-03 -0.1414E-03 0.5296E-11 0.9422E-12 0.4719E-11 0.2072E-11
C.16.UE (4 0.4712e t] 0.2211E 02 -0.6185e 05 0.8081E 04 -0.6869E-03 -0.1426E-03 C.5215E-11 0.9707E-12 0.4264E-11 0.1992E-11
0.16(UE 04 0.5236E 01 0.2142E 02 -0.6125E 05 0.3027E 04 -0.6764E-03 -0.1383E-03 0.513CE-11 0.9582E-12 0.3948E-11 0.1697E-11
U.1660E C4 0.5759E (1 0.2083E 02 -0.6052E 05 -0.4378E 03 -0.6686E-03 -0.1289E-03 0.5667E-11 0.9073E-12 0.3758E-11 0.1316E-11
U.ZUULE U4 U.DZDCE U0 U.1UZ4E UZ -C.5Z8ZE U5 -U.0654E 04 -U.42Z0E-03 -0.84Z9E-C4 G.2614E-11 C.4905E-12 0.1669E-11 0.3215E-12
C.2COUE 04 C.1571E C1 0.1068E 02 -0.5240E 05 -0.1587E 05 -0.4341E-03 -0.7472E-C4 C.2695E-11 0.4606E-12 0.1907E-11 -0.1610E-12
U.2000E 04 0.2094E 01 0.1097E 02 -0.5080E 05 -0.2294E 05 -0.4406E-03 -0.7500E-04 0.2740E-11 0.4749E-12 0.2137E-11 -0.2760E-12
6.2CCCE C4 0.2618E C1 0.1120E C2 -C.4063E C5 -0.3204E C5 -0.4450E-03 -0.7752E-04 0.2776E-11 0.5023E-12 0.2393E-11 -0.1749E-12
C.2CLUE 04 C.3142E C1 0.1130E 02 -C.3825E 05 -0.4245E 05 -0.4464E-03 -0.8187E-C4 C.2775E-11 0.5304E-12 0.2535E-11 0.2540E-12
U.2LCUE L4 U.3665E L1 U.1129E U2 -L.2448E U5 -U.3193E U5 -0.4455E-03 -0.8548E-C4 C.2773E-11 C.5492E-12 0.2357E-11 0.9592E-12
U.2CULL U4 U.4105E C1 U.1114E J2 -U.1119E U5 -U.019UE D5 -U.4467E-03 -0.8563E-C4 G.284CE-11 0.504IE-12 -0.1435E-11 -0.3766E-12
0.2000L 04 0.52366 C1 0.10736 02 -0.53936 05 0.43416 04 -0.42636-03 -0.10716-C3 0.26416-11 0.58656-12 0.18696-11 0.10986-11
C.2CCUE 04 0.5759E C1 C.1C4ZE 0Z -0.5337E 05 0.1296E 03 -0.4216E-03 -0.10C7E-C3 C.261CE-11 0.5623E-12 0.1725E-11 0.8621E-12
(.24tCe (4 t.5256E t0 t.5751E ul -0.4830E 05 -0.7446E 04 -0.2879E-03 -0.7056E-04 0.1521E-11 (.3404E-12 0.8425E-12 0.2388E-12
C.2460E C4 U.1C47E C1 C.5528E U1 -G.4797E 05 -U.1193E 05 -0.2915E-03 -U.6589E-04 C.1542E-11 0.3270E-12 0.8983E-12 0.5946E-13
C.24ULL 04 0.1571E 01 0.5571E 01 -0.4712E 05 -0.1755E 05 -0.2962E-03 -0.633EE-04 0.1569E-11 0.3240E-12 0.1009E-11 -0.8472E-13
U.2400E L4 U.2694E C1 C.0129E U1 -U.449UE U5 -U.2470E 05 -U.3006E-03 -U.6323E-C4 C.1594E-11 C.3318E-12 0.1167E-11 -0.1508E-12
U.24(UE U4 U.2610E U1 U.0250E U1 -U.4U(9E 05 -U.3330E U5 -0.3036E-03 -0.6492E-C4 C.1611E-11 C.3466E-12 0.1332E-11 -0.7879E-13
U.24C∪E U4 (.3142L U1 U.6312E U1 -C.314UE U5 -U.4241E U5 -U.3047E-03 -0.6748E-C4 0.1617E-11 0.3620E-12 U.1419E-11 0.1728E-12
C.2400E 04 0.3665E C1 C.63C9E C1 -0.1d16E 05 -0.4996E 05 -0.3040E-C3 -0.70C2E-C4 C.1614E-11 0.3728E-12 0.1323E-11 0.5587E-12
U.24CUE C4 C.4189E C1 0.6416E 01 -U.4779E C5 0.1952E 05 -0.2984E-03 -0.8951E-C4 C.1578E-11 0.3870E-12 0.1413E-11 0.8834E-12
U.24CUE U4 C.4712E C1 0.6258E C1 -0.4932E 05 U.1149E 05 -0.2946E-03 -0.8945E-C4 U.155EE-11 0.3950E-12 U.1187E-11 0.8593E-12
C.2400E L4 U.5236E C1 U.6066E 01 -C.4943E 05 0.0304E 04 -0.2905E-03 -0.8702E-04 C.1535E-11 G.3924E-12 0.1011E-11 0.7664E-12
G.24LUE U4 G.5759E C1 G.5883E 01 -C.49C2E 05 U.5148E U3 -0.2874E-03 -0.8241E-04 C.1518E-11 U.3794E-12 U.8961E-12 U.6111E-12
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TABLE I. - Concluded. PLANET-EARTH FLYBY TRAJECTORIES

and the control of the

(h) Pluto-Earth flyby trajectories

TIME	PSI	J	VX(T)	VY(T)	AX (0)	AY(C)	AXDOT(C)	AYDOT(O)	AXDOT(T) AYDO	OT (T)
0.46C0E 03 0.46C0E 03 C.44C0E 03 0.46C0E 03 C.40C0E 03 C.40C0E 03 C.46C0E 03 C.46C0E 03 C.46C0E 03 C.46C0E 03	0.1571E (1 C.2094E C1 C.2618E C1 C.3142E C1 U.3665E C1 C.4712E C1 U.5236E C1	C.2480E C.2544E C.26C8E C.26C8E C.26C9E C.2654E C.2658E C.2658E C.2658E C.2658E C.2658E C.2487E C.2487E C.2551E C.2487E C.2658E C.2487E C.2658E C.2487E C.2658E C.2487E C.2658E C.2487E C.2658E C.2487E C.2658E C.2668E C.2668	04 -0.2537E 06 04 -0.2561E 06 04 -0.2595E 06 04 -0.2628E 06 04 -0.2658E 06 04 -0.2651E 06 04 -0.2651E 06 04 -0.2659E 06 04 -0.2651E 06 04 -0.2537E 06	0.1609E 04 0.1165E 04 -0.2044E 04 -0.1021E 05 -0.4189E 05 0.5788E 04 -0.2633E 04 -0.5902E 04 -0.6366E 04	-0.1483E-01 -0.1502E-01 -0.1516E-01 -0.1517E-01 -0.1515E-01 -0.1502E-01 -0.1483E-01 -0.1465E-01	-0.8515E-04 -0.3415E-C4 -0.8322E-C4 -0.2172E-03 -0.3998E-C3 -0.6055E-C3 -0.7392E-C3 -0.7393E-C3	G.42C5E-09 G.4245E-09 G.4355E-09 G.4356E-09 G.4356E-09 G.4356E-09 G.4355E-09 G.4355E-09 G.4255E-09 G.425E-09 G.425E-09	0.6500E-11 0.2565E-11 0.1166E-11 0.2713E-11 0.6884E-11 0.1433E-10 C.1692E-10 C.2108E-10 0.2263E-10 0.2123E-10 0.1729E-10	0.4242E-09 0.26 0.4187E-09 0.26	706E-12 443E-11 732E-11 044E-10 547E-10
0.10CUE 04 0.1000E 04 0.1000E 04 C.1CGOE 04 C.1CGOE 04 C.1CGOE C4 0.10CUE C4 C.1CGOE C4 C.1CGOE C4 C.1CGOE C4	0.5236E CU 0.1047E C1 0.1571E C1 0.2094E C1 0.3142E C1 0.3665E C1 0.4189E C1 0.4712E C1 0.5236E C1 0.5759E C1	0.1569E (0.1647E (0.1646E (0.1673E (0.1683E (0.1680E (0.1650E (0.1650E (0.16579E (0.1579E (C3 -0.1071E 06 03 -0.1082E 06 03 -C.1095E 06 03 -C.1106E 06 03 -C.1101E 06 03 -C.1104E 06 03 -C.1109E 06 03 -C.1109E 06 03 -C.1109E 06 03 -C.1094E 06 03 -C.1084E 06 03 -C.1084E 06	0 -0.4088E 04 0 -0.6730E 04 0 -0.1194E 05 6 -0.2209E 05 6 -0.4242E 05 0 -1828E 05 0 -7459E 04 0 -1985E 04 0 -7643E 03	-0.2335E-02 -0.2364E-02 -0.2393E-02 5 -0.2413E-02 6 -0.2420E-02 5 -0.2412E-02 -0.2392E-02 4 -0.2364E-02 3 -0.2334E-02	-0.1112E-03 -0.1025E-C3 -0.1092E-03 -0.1281E-C3 -0.1488E-03 -0.2066E-C3 -0.2192E-03 -0.2259E-03 -0.2171E-03	0.27C3E-10 C.2729E-10 C.2766E-10 C.2802E-10 C.2827E-10 C.2827E-10 C.2827E-10 C.28C1E-10 C.2765E-10 C.2729E-10	0.1563E-11 0.1323E-11 0.1248E-11 0.1248E-11 0.1635E-11 0.1918E-11 0.2168E-11 0.2432E-11 0.2546E-11 0.2471E-11 0.2231E-11	0.2517E-10 0.18 0.2562E-10 -0.66 0.2624E-10 -0.14 0.2714E-10 -0.10 0.2749E-10 0.8 0.2749E-10 0.5 0.2643E-10 0.5 0.2523E-10 0.30	481E-11
0.1600E 04 0.1600E 04 0.1600E 04 0.1600E 04 0.1600E 04 0.1600E 04 0.1600E 04 0.1600E 04 0.1600E 04	0.2094E G1 0.2618E C1 0.3142E 01 0.3665E C1 0.4189E C1 0.4712E C1 0.5236E C1	0.3760E 0.3846E 0.3933E 0.3993E 0.4017E 0.4027E 0.3977E 0.3894E 0.3802E	02 -0.7293E 00 02 -0.7353E 00 02 -0.7419E 00 02 -0.7198E 00 02 -0.6486E 00 02 -0.7338E 00 02 -0.7522E 00 02 -0.7522E 00 02 -0.7339E 00 02 -0.7315E 00	5 -0.6948E 04 5 -0.1092E 05 5 -0.1732E 05 5 -0.2747E 05 6 -0.4245E 05 6 0.2392E 05 0.1295E 05 0.6106E 05 0.1917E 05	4 -0.9055E-03 5 -0.9167E-03 5 -0.9275E-03 5 -0.9348E-03 5 -0.9370E-03 5 -0.935E-03 5 -0.9266E-03 4 -0.9161E-03 4 -0.9051E-03	0 -0.8098E-04 0 -0.771CE-C4 0 -0.7901E-04 0 -0.8523E-C4 0 -0.9241E-C4 0 -0.125E-03 0 -0.1255E-03 0 -0.1255E-03 0 -0.1255E-03	0.6644E-11 0.6710E-11 C.6800E-11 0.6889E-11 C.66950E-11 C.66937E-11 C.6880E-11 C.6797E-11 C.6707E-11 C.66707E-11	0.6588E-12 0.6042E-12 0.5893E-12 0.6189E-12 C.6807E-12 0.7428E-12 0.7954E-12 0.8542E-12 0.8683E-12 0.8683E-12	0.5761E-11 -0.3 0.6059E-11 -0.6 0.6471E-11 -0.5 0.6778E-11 0.3 0.6740E-11 0.1 0.6239E-11 0.2 0.5873E-11 0.1	755E-13 427E-12 274E-12
C.20C0E G4 0.2C0UE U4 0.2CCUE 04 0.2CCUE 04 0.2CCUE 04 C.2CCUE 04 C.2COUE 04 C.2COUE 04 0.2CCUE 04 0.2CCUE 04 0.2CCUE 04 0.2CCUE 04 0.2CCUE 04	U.1047E C1 0.1571E C1 C.2094E C1 0.2618E C1 U.3142E C1 C.3665E C1 C.4189E C1 C.4712E C1 0.5236E C1	0.1896E 0.1937E 0.1978E 0.2009E 0.2021E 0.2017E 0.1994E 0.1968E 0.1922E	02 -C.6237E 0 02 -O.6274E 0 02 -C.63(1E 0 02 -C.5938E 0 02 -C.5938E 0 02 -C.5170E 0 02 -C.5170E 0 02 -O.2502E 0 02 -O.6465E 0 02 -C.6339E 0 02 -C.6269E 0	5 -0.8376E 0 5 -0.1295E 0 5 -0.1976E 0 5 -0.2959E 0 5 -0.4244E U 5 -0.5590E 0 6 -0.8094E 0 5 0.8053E 0	4 -0.5757E-03 5 -0.5827E-05 5 -0.5894E-03 5 -0.5939E-03 5 -0.5939E-03 5 -0.5937E-03 4 -0.5820E-03 4 -0.5753E-03	3 -0.6758E-04 3 -0.6484E-04 3 -0.6570E-04 3 -0.6570E-04 3 -0.7355E-C4 3 -0.7745E-C4 3 -0.7815E-04 3 -0.9546E-C4	0.3453E-11 C.3455E-11 0.3544E-11 C.3574E-11 0.3563E-11 C.3570E-11 0.3612E-11 C.3494E-11 0.3450E-11	0.4303E-12 0.4037E-12 0.3970E-12 0.4119E-12 0.4418E-12 0.4719E-12 0.4959E-12 0.4731E-12 0.5397E-12 0.5331E-12 0.5067E-12	0.2646E-11 0.1 0.2779E-11 -0.2 0.2990E-11 -0.3 0.3257E-11 -0.3 0.3429E-11 0.2 0.3389E-11 0.1 -0.3361E-12 -0.3 0.2887E-11 0.1 0.2709E-11 0.9	2270E-12 1785E-12 1072E-12 1173E-12 1056E-11 1443E-12

```
0.24CUE C4 0.5236E C0 0.1063E 02 -0.5573E 05 -0.5869E 04 -0.3930E-03 -0.62C3E-C4 0.1988E-11 0.3018E-12 0.1736E-IT 0.1770E-12
0.24CUE 04 0.1C47E 01 0.1077E 02 ₹0.5589E 05 ~0.9562E 04 ~0.3966E-03 ~0.577CE-C4 0.2C6E-11 0.287IE-12 0.1413E-11 0.2486E-14
U.24CUE U4 U.1571E C1 C.1100E U2 -0.5581E 05 -0.1459E 05 -0.4013E-03 -0.556CE-C4 C.2C34E-11 0.2835E-12 0.1514E-11 -0.1502E-12
0.2400E 04 0.2094E 01 0.1123E 02 -0.5466E 05 -0.2162E 05 -0.4059E-03 -0.5593E-04 0.2060E-11 0.2919E-12 0.1667E-11 -0.2368E-12
0.24tt 6 4 0.26tt C1 C.1140E 02 -0.510t 65 -0.3108E 05 -0.4089E-03 -0.58tte-04 C.2077E-11 0.3082E-12 0.1848E-11 -0.1698E-12
0.2460E 04 0.3142E C1 0.1147E C2 -0.4296E 05 -0.4242E 05 -0.4099E-03 -0.6095E-04 0.2082E-11 0.3249E-12 0.1955E-11 0.1504E-12
G.24CUE 04 U.3005E 01 0.1145E 02 -0.2908E U5 -0.5320E 05 -0.4092E-U3 -0.6354E-C4 G.2C79E-11 0.3366E-12 0.1786E-11 0.6456E-12
0.24CUE U4 U.4189E C1 U.1134E G2 -C.1527E U5 -U.6812E U5 -U.4U91E-03 -0.6448E-C4 C.21C1E-11 0.3261E-12 -0.3C17E-12 -0.3662E-12
0.24cue t4 0.4712E t1 0.1122E 02 -0.5715E 05 0.9564E 04 -0.4006E-03 -0.7969E-C4 0.2029E-11 0.3621E-12 0.1616E-11 0.8150E-12
C.24tub t4 t.5236E 01 6.1096b 02 -0.5675b 05 0.4177b 04 -0.3961E-03 -0.7762E-04 C.2005E-11 0.3587E-12 0.1474E-11 0.6933E-12
C.2460tb 04 0.5759tb (1 C.1674tb 02 -0.5615tb 05 0.3047tb 03 -0.3927tb-03 -0.7332tb-04 0.1587tb-11 0.3442tb-12 0.1391tb-11 0.5317tb-12
C.2860E 04 0.5236E CC C.0581E 01 -0.5125E 05 -0.0453E C4 -0.2860E-03 -C.5349E-C4 C.125EE-11 0.2224E-12 0.7802E-12 0.1357E-12
C.2660E 04 C.1047E C1 C.6055E G1 -0.512CE 05 -0.1056E 05 -0.2886E-03 -0.5018E-04 C.1270E-11 C.2136E-12 0.8187E-12 0.8125E-14
C.2EUUC 04 C.107xE C1 C.6785E C1 -C.5C61E 05 -0.1592E 05 -0.2920E-03 -0.4647E-C4 C.1267E-11 C.2115E-12 0.8959E-12 -0.9892E-13
C.2860t 04 C.26946 01 0.09236 01 -C.49216 05 -0.23076 05 -0.2953t-03 -0.48536-C4 C.13C3E-11 C.2166E-12 0.1011E-11 -0.1522E-12
C.28CUL 04 C.2018E LI U.7020E DI -C.4502E D2 -0.3217E D5 -0.2975E-03 -0.4993E-04 C.1313E-11 C.2263E-12 U.1138E-11 -0.9796E-13
C.28UUE U4 C.314ZE U1 U.7U73E 01 -U.3674E 05 -U.4239E U5 -U.4239E 03 -U.519ZE-C4 G.1317E-11 0.2363E-12 0.1209E-11 0.1095E-12
C.2860e 04 0.3665e 01 0.7064e 01 -6.2333e 05 -0.514de C5 -0.2977e-03 -0.5382e-C4 C.1314e-11 C.2434e-12 0.1133e-11 0.4395e-12
v.2860E 04 (.41d9E 01 0.70lbE 01 -0.7343E 04 -0.58d5E 05 -0.2982E-03 -0.5471E-04 0.1333E-11 0.2381E-12 -0.4149E-12 -0.6421E-12
C.28CUL C4 C.471ZE C1 C.6966E C1 -0.5240E C5 O.1074E C5 -0.2913E-03 -0.6695E-C4 C.126ZE-11 C.2586E-12 0.9916E-12 0.5924E-12
0.2860E 04 0.5236E 01 0.6808E 01 -0.5229E 05 0.4960E 04 -0.2881E-03 -0.6528E-04 0.1267E-11 0.2567E-12 0.8776E-12 0.5131E-12
C.28CUE L4 U.5759E L1 G.6000E C1 -U.5178E 05 U.6310E U3 -0.2857E-G3 -U.62CCE-C4 C.125EE-11 G.2481E-12 U.8079E-12 0.3977E-12
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REC = 00000 FIL=

C1 UNITUS, EUF.

TABLE II. - EARTH-PLANET ORBITER TRAJECTORIES

(a) Earth-Mercury orbiter trajectories

TIME	PST	J	AX (O)	AY (0)	AX (T)	AY(T)	AXDOT(O)	AYDOT(O)	AXDOT(T)	AYDOT(T)
0.2500F 02 0.2500F 02 0.2500F 02	0.5236F 00 0.1C47F 01 0.1571F 01 0.2094F 01 0.2618E 01 0.3142F 01 0.3665F 01 0.4189F 01 0.4712F 01 0.5236F 01	0.9128E 04 0.1235E 05 0.2044F 05 0.3011F 05 0.3750E 05 0.4072F 05 0.6160F 05 0.5769E 05	-0.1046F 00 -0.1140F 00 -0.1425E 00 -0.1815E 00 -0.2189E 00 -0.2422F 00 -0.2479F 00 -0.22496F 00 -0.2260E 00 -0.1882E 00	-0.1915E-01 0.1048E-01 0.2085E-01 0.9473E-02 -0.1648E-01 -0.3948E-01 -0.1028E 00 -0.1265E 00 -0.1375E 00	0.1088E 00 0.1144E 00 0.1426E 00 0.1852E 00 0.2273E 00 0.2441E 00 0.2694E 00 0.2729E 00 0.2498E 00	0.3873E-01 -0.5387E-02 -0.3972E-01 -0.5178E-01 -0.2821E-01 0.4105E-01 -0.3621E-01 0.3164E-01 0.8008E-01	0.2414E-06 0.2673E-06 0.2494E-06 0.2112E-06	0.2249E-07 -0.1050E-C7 -0.2496E-C7 -0.1508E-C7 0.1389E-C7 0.4002E-07 0.5504E-07 0.8966E-07 0.1144E-C6	0.1193E-06 0.1985E-06 0.3012E-06 0.3582E-06 0.1536E-06 0.1423E-06 0.1595E-06	0.6496E-07 0.9698E-08 -0.6541E-07 -0.1175E-06 -0.9956E-07 0.1272E-07 0.6617E-07 0.5164E-07 0.3040E-07
0.5000F 02 0.5000F 02 0.5000F 02 0.5000F 02 0.5000F 02 0.5000F 02 0.5000F 02 0.5000F 02 0.5000F 02	0.5759E 01 0.5236F 00 0.1047F 01 0.1571F 01 0.2094E 01 0.2618F 01 0.3142F 01 0.3665F 01 0.4189F 01 0.4712F 01 0.5236E 01	0.4654E C4 0.2433F 04 0.1199E 04 0.1012E 04 0.1587F 04 0.3158E 04 0.3583E 04 0.1331E 05	-0.1478E 00 -0.1832E-01 -0.1586F-01 -0.1973E-01 -0.2838E-01 -0.3867E-01 -0.4714E-01 -0.5187E-01 -0.5326E-01 -0.5709E-01	-0.4063E-01 -0.2803E-01 -0.1625E-01 -0.8435E-02 -0.6176E-02 -0.8677E-02 -0.1322E-01 -0.1744E-01 -0.5005E-01	0.4619E-01 0.4802E-01 0.6667E-01		0.9118E-08 0.97C6E-C8 0.1386E-C7 0.1977E-07 0.2504E-C7 0.2810E-C7 0.2903E-07 0.3866E-C7	0.1178E-C6 0.2C39E-C7 0.1461E-07 0.8455E-C8 0.4C14E-C8 0.2598E-C8 0.4004E-08 0.6596E-C8 0.8778E-08 0.1440E-C7 0.1987E-C7	0.6262E-07 0.4096E-07 0.1459E-07 0.1544E-08 0.9979E-08 0.3197E-07 0.4964E-07 0.4997E-07	0.3798E-07 0.3463E-07 0.1324E-07 -0.9326E-08 -0.1573E-07 -0.1196E-08 0.2415E-07
0.5000F 02 0.7500F 02 0.7500F 02 0.7500F 02 0.7500F 02 0.7500F 02 0.7500F 02 0.7500F 02 0.7500F 02 0.7500F 02	0.5226E 00 0.1047F 01 0.1571E 01 0.2094F 01 0.2618F 01 0.3142F 01 0.3665F 01 0.4189E 01 0.4712E 01 0.5236F 01	0.3360E 04 0.2085E 04 0.1083E 04 0.4775E 03 0.2546E 03 0.4518E 03 0.6131E 03 0.7316E 03	5 -0.3805E-01 4 -0.3224E-02 4 -0.1933F-04 4 -0.1002E-03 3 -0.3174E-02 3 -0.7966E-02 3 -0.1281E-01 3 -0.1646E-01 3 -0.1934F-01 3 -0.1934F-01 3 -0.1934F-01	-0.2994E-01 -0.2333E-01 -0.1621E-01 -0.1032E-01 -0.6863E-02 -0.5975E-02 -0.6847E-02 -0.8402E-02 -0.9913E-02 -0.1108E-01	0.4424E-01 0.2988E-01 0.1508E-01 0.4763E-02 0.1419E-02 0.4270E-02 0.9784E-02 0.1374E-01 0.1349E-01	0.1397E-01 0.6143E-02 0.3918E-02 0.7189E-02 0.1327E-01 0.1883E-01	0.3383E-C8 0.1104E-08 0.3592E-C9 0.1163E-C8 0.3007E-C8 0.5103E-C8 0.6780E-C8 0.7781E-C8 0.8215E-08 0.8320E-C8	0.9256E-C8 0.7552E-C8 0.5298E-C8 0.3268E-08 0.2049E-C8 0.1786E-08 0.2178E-C8 0.32767E-08 0.3245E-C8 0.3506E-C8	0.1300E-07 -0.2797E-08 -0.6649E-08 0.1051E-12 0.9129E-08 0.1311E-07 0.9515E-08 0.7990E-09	0.3879E-08 0.2466E-07 0.3073E-07 0.2233E-07 0.8080E-08 -0.1507E-08 -0.1423E-08 0.5713E-08 0.1355E-07 0.1681E-07
0.7500F 02 0.1000F 03	0.5759F 01 0.5236E 00 0.1047F 01 0.1571E 01 0.2094E 01 0.2618F 01 0.3142F 01 0.3665F 01 0.4189F 01 0.4712F 01 0.5236F 01 0.5236F 01 0.5759F 01	0.2693E 0 0.1890E 0 0.1161E 0 0.6101E 0 0.2732E 0 0.1230E 0 0.9597F 0 0.1281E 0 0.1760E 0 0.2194E 0	4 0.4630E-02 4 0.5547F-02 3 0.4335E-02	-0.2351E-01 -0.1927E-01 -0.1425E-01 -0.9593E-02 -0.6224E-02 -0.4502E-02 -0.4167E-02 -0.4646E-02 -0.5412E-02	0.3744E-01 0.2827E-01 0.1525E-01 0.3560E-02 -0.3343E-02 -0.4676E-02 0.2140E-02 0.3449E-02 0.3052E-02	0.2333E-01 0.2817E-01 0.2533E-01 0.1790E-01 0.9935E-02 0.4679E-02 0.3277E-02 0.4824E-02 0.7409E-02	0.9689E-C9 -0.5505E-C9 -0.1324E-C8 -0.1235E-C8 -0.4583E-C9 0.6435E-C9 0.1704E-C8 0.2508E-08 0.3013E-C8 0.3289E-C8	0.1230E-08 0.8552E-C9 0.8536E-09 0.1050E-08 0.1280E-08 0.1454E-C8	0.3524E-07 0.2815E-07 0.1257E-07 -0.2328E-08 -0.9550E-08 -0.8117E-08 -0.2324E-08 0.2419E-08 0.3235E-08	0.2621E-07 0.2276E-07 0.1238E-07 0.2629E-08 -0.1553E-08 -0.1513E-09 0.3548E-08 0.6010E-08

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0.1250E 03 0.5236E 00 0.2230E 04 0.3712E-02 -0.1903E-01 0.3107E-01 0.1707E-02 0.4035E-10 0.2429E-08 0.2722E-07 -0.1605E-08
0.1250E 03 0.1047E 01 0.1698E 04 0.6313E-02 -0.1607E-01 0.2654E-01 0.1593E-01 -0.1032E-08 0.2271E-08 0.2350E-07 0.1369E-07
           0.1571F 01 0.1163E 04 0.7516E-02 -0.1229E-01 0.1596E-01 0.2380E-01 -0.1690E-08 0.1780E-08 0.1145E-07 0.2233E-07
           0.2094F 01 0.7073E 03 0.7105E-02 -0.8489E-02 0.4453E-02 0.2422E-01 -0.1804E-08 0.1169E-08 -0.1809E-08 0.2125E-07
           0.2618E 01 0.3775E 03 0.5371E-02 -0.5426E-02 -0.3980E-02 0.1910E-01 -0.1429E-08 0.6503E-09 -0.9883E-08 0.1322E-07
           0.3142F 01 0.1780E 03 0.2957E-02 -0.3506E-02 -0.7598E-02 0.1180E-01 -0.7585E-09 0.3511E-09 -0.1068E-07 0.4013E-08
                      0.8176F 02 0.5364F-03 -0.2694E-02 -0.7004E-02 0.5527E-02 -0.2065E-10 0.2787E-09 -0.6607E-08 -0.1684E-08
           0.3665E 01
                       0.5123E C2 -0.1441E-02 -0.2664E-02 -0.4247E-02 0.2010E-02 0.6168E-09 0.3572E-09 -0.1793E-08 -0.2709E-08
           0.4189E 01
           0.4712F 01
                      0.5403E 02 -0.2829E-02 -0.3034E-02 -0.1488E-02 0.1271E-02 0.1086E-C8 0.4936E-09 0.8485E-09 -0.8307E-09
0.1259E 03 0.5236F 01 0.6947E 02 -0.3688E-02 -0.3524E-02 -0.5772E-04 0.2211E-02 0.1396E-08 0.6237E-09 0.7634E-09 0.1338E-08
0.1250F 03 0.5759E 01 0.8732E 02 -0.4163E-02 -0.3981E-02 -0.2281E-03 0.3460E-02 0.1592E-08 0.7183E-09 -0.8560E-09 0.2040E-08
0.1500F 03 0.5236E 00 0.1878E 04 0.4729E-02 -0.1554E-01 0.2496E-01 -0.3552E-02 -0.4162E-09 0.1052E-C8 0.2070E-07 -0.1370E-08
0.1500E 03 0.1047E 01 0.1518E 04 0.6969E-02 -0.1344E-01 0.2432E-01 0.1026E-01 -0.1198E-08 0.1116E-08 0.1929E-07 0.1096E-07
0.1500F 03 0.1571F 01 0.1120E 04 0.8206E-02 -0.1052E-01 0.1626E-01 0.1975E-01 -0.1736E-08 0.9136E-09 0.1003E-07 0.1912E-07
0.1500E 03 0.2094E 01 0.7485E 03 0.8180E-02 -0.7378E-02 0.5562E-02 0.2243E-01 -0.1909E-08 0.5756E-09 -0.1529E-08 0.1931E-07
0.1500F 03 0.2618F 01 0.4518F 03 0.7012F-02 -0.4651F-02 -0.3458F-02 0.1916F-01 -0.1717F-08 0.2499F-09 -0.9566F-08 0.1290F-07
0.1500E 03 0.3142E 01 0.2464E 03 0.5136E-02 -0.2747E-02 -0.8418E-02 0.1273E-01 -0.1272E-08 0.3961E-10 -0.1144E-07 0.4419E-08
0.1500F 03 0.3665E 01 0.1237E 03 0.3081E~02 -0.1744E-02 -0.9163F-02 0.6189E-02 -0.7251E-09 -0.2732E-10 -0.8392E-08 -0.1792E-08
0.1500E 03 0.4189E 01 0.6197E 02 0.1255E-02 -0.1455E-02 -0.7130E-02 0.1602E-02 -0.2081E-09 0.1621E-10 -0.3719E-08 -0.3998E-08
0.1500F 03 0.4712F 01 0.3779E 02 -0.1540E-03 -0.1598E-02 -0.4227E-02 -0.4559E-03 0.2097E-09 0.1145E-09 -0.2270E-09 -0.3089E-08
0.1500F 03 0.5236F 01 0.3339F 02 -0.1135E-02 -0.1932E-02 -0.1906E-02 -0.5526E-03 0.5146E-09 0.2216E-09 0.1033E-08 -0.1093E-08
0.1500F 03 0.5759F 01 0.3779E 02 -0.1766E-02 -0.2306E-02 -0.7864E-03 0.2617E-03 0.7244E-09 0.3120E-09 0.5868E-09 0.3103E-09
0.1750F ∩3 0.5236F 00 0.1602F 04 0.2204E~02 -0.1266E-01 0.1932E-01 -0.6484E-02 -0.6736E-C9 0.1673E-09 0.1539E-07 -0.6999E-09
0.1750F 03 0.1047E 01 0.1358E 04 0.7213E-02 -0.1120E-01 0.2180E-01 0.6019E-02 -0.1256E-08 0.3562E-09 0.1563E-07 0.9045E-08
0.1750F 03 0.1571E 01 0.1057E 04 0.8378E-02 -0.8936E-02 0.1610E-01 0.1622E-01 -0.1692E-08 0.3251E-09 0.8577E-08 0.1647E-07
0.1750F 03 0.2094E 01 0.7550E 03 0.8542E-02 -0.6334E-02 0.6482E-02 0.2047E-01 -0.1874E-08 0.1595E-09 -0.1415E-08 0.1739E-07
0.1750F 03 0.2618E 01 0.4946E 03 0.7720E-02 -0.3932E-02 -0.2631E-02 0.1870E-01 -0.1777E-08 -0.3298E-10 -0.9078E-08 0.1218E-07
0.1750F 03 0.3142F 01 0.2983E 03 0.6210E-02 -0.2130E-02 -0.8402E-02 0.1314E-01 -0.1463E-08 -0.1679E-C9 +0.1148E-07 0.4427E-08
0.1750F 03 0.3665F 01 0.1675E 03 0.4432E-02 -0.1065E-02 -0.1010E-01 0.6668E-02 -0.1040E-08 -0.2109E-09 -0.9122E-08 -0.1873E-08
0.1750F 03 0.4189F 01 0.9023F 02 0.2751E-02 -0.6424E-03 -0.8699E-02 0.1520E-02 -0.6111E-09 -0.1739E-09 +0.4663E-08 -0.4694E-08
0.1750F 03 0.4712F 01 0.5004E 02 0.1371E-02 -0.6507E-03 -0.5864E-02 -0.1360E-02 -0.2411E-09 -0.9140E-10 -0.7603E-09 -0.4364E-08
0.175NF 03 0.5236E 01 0.3228E 02 0.3421E-03 -0.8848E-03 -0.3083E-02 -0.2164E-02 0.4678E-10 0.3519E-11 0.1261E-08 -0.2499E-08
0.1750F 03 0.5759E 01 0.2667E 02 -0.3732E-03 -0.1200E-02 -0.1189E-02 -0.1690E-02 0.2570E-09 0.8973E-10 0.1505E-08 -0.6918E-09
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TABLE II. - Continued. EARTH-PLANET ORBITER TRAJECTORIES

(b) Earth-Venus orbiter trajectories

TIME	PSI	J	AX(0)	AY (O)	AX(T)	AY(T)	AXDOT(O)	AYDOT(O)	AXDOT(T)	AYDOT(T)
0.5000E 02 0.5000F 02 0.5000F 02 0.5000F 02 0.5000F 02 0.5000F 02 0.5000F 02 0.5000F 02 0.5000F 02	0.5236F 00 0.1047F 01 0.1571F 01 0.2094F 01 0.2618F 01 0.3142F 01 0.3665E 01 0.4189E 01 0.5759F 01	0.2456F 03 0.7498F 03 0.2381E 04 0.4436E 04 0.6105F 04 0.6962F 04 0.7165F 04 0.1150F 05 0.9396E 04	-0.4278E-02 -0.1067E-01 -0.2495E-01 -0.4302E-01 -0.5954F-01 -0.6971F-01 -0.7262F-01 -0.7163F-01 -0.5218E-01 -0.3594E-01	-0.6627E-02 0.5488E-02 0.8785E-02 0.2944E-02 -0.8341E-02 -0.1862E-01 -0.2495E-01 -0.6193E-01 -0.6389E-01	0.1755E-01 0.3259E-01 0.5135E-01	0.9694E-02 -0.8167E-02 -0.1974E-01 -0.2098E-01 -0.9311E-02 0.1462E-01 0.4314E-01 0.2619E-01 0.4292E-01	0.2166E-C7 0.3134E-07	-0.9026E-C9	0.1522E-07 0.2828E-07	-0.3825E-08 -0.1279E-07 -0.1653E-07 -0.1047E-07 0.6082E-08 0.2666E-07 0.2072E-07 0.1981E-07
0.1000F 03 0.1000F 03 0.1000F 03 0.1000F 03 0.1000F 03 0.1000F 03 0.1000F 03 0.1000F 03 0.1000F 03	0.5236F 00 0.1047F 01 0.1571F 01 0.2094F 01 0.2618F 01 0.3142F 01 0.4189F 01 0.4712F 01 0.5236F 01 0.5759F 01	0.6823E 02 0.2097F 03 0.3604E 03 0.4692E 03 0.5269F 03 0.2919E 04	0.5966E-02	-0.1660E-02 -0.2873E-02 -0.4946E-02 -0.6967E-02 -0.8533E-02 -0.2407E-01	0.8350E-02 0.1208E-01 0.1285E-01 0.1008E-01 0.2587E-01	0.1554E-01 0.1019E-01 0.4176E-02 -0.2000E-03 -0.1202E-02 0.1531E-02 0.6663E-02 0.1192E-01 0.1466E-02	0.2020E-C8 0.3466E-C8 0.4406E-C8 0.4818E-08	0.2975E-C8 0.2034E-08 0.1094E-08 0.5218E-C9 0.5120E-C9 0.9815E-09 0.1623E-C8 0.2148E-08 0.2442E-08 0.2833E-08 0.3480E-C8	0.3534E-08 0.5586E-08 0.5654E-08 0.3570E-08	-0.2975E-08
0.1500F 03 0.1500F 03 0.1500E 03 0.1500E 03 0.1500E 03 0.1500F 03 0.1500F 03 0.1500F 03 0.1500F 03	C.5236E 00 0.1047E 01 0.1571E C1 0.2094F 01 0.2618F 01 0.3142F 01 0.4189F 01 0.4712F 01 0.5236F 01 0.5236F 01	0.3650F 02 0.6155E 02 0.8051E 02	3 0.8114E-02 3 0.7151E-02 3 0.5132F-02 2 0.2554E-02	-0.2283F-02 -0.3114E-02 -0.3783F-02	0.5633E-02 0.8017E-03 -0.2121E-02 -0.2637E-02 -0.1216E-02 0.9624E-03 0.2603E-02 0.2907E-02 0.1800E-02	0.1290E-01 0.1154E-01 0.8182E-02 0.4375E-02 0.1593E-02 0.6647E-03 0.1479E-02 0.3201E-02 0.4803E-02	0.1011E-C8 0.1235E-08 0.1334E-C8	0.4771E-10 -0.1489E-10 0.7743E-10 0.2651E-C9 0.4631E-09 0.6118E-C9 0.6910E-C9	-0.6556E-09 0.3979E-09 0.1032E-08	0.4111E-08 0.3276E-08 0.1607E-08 0.2798E-09 -0.1762E-10 0.5752E-09 0.1406E-08 0.1841E-08
0.2000F 03 0.2000F 03 0.2000F 03 0.2000F 03 0.2000F 03 0.2000F 03 0.2000F 03 0.2000F 03 0.2000F 03	0.5236F 00 0.1047E 01 0.1571E 01 0.2094F 01 0.2618F 01 0.3142F 01 0.3665E 01 0.4189F 01 0.4712E 01 0.5236E 01	0.8934E 0: 0.6700E 0: 0.4517F C: 0.2678E 0: 0.1351F 0: 0.5462E 0: 0.1557E C: 0.29571E 0: 0.9167E 0:	3 0.8064E-02 3 0.8314E-02 3 0.7835E-02 3 0.6623E-02 0.4910E-02 2 0.3063E-02 0.1422E-02	-0.6686E-02 -0.5008E-02 -0.3126E-02 -0.1451E-02 -0.3145E-03 0.1605E-03 0.7686E-04 -0.338E-03 -0.8666E-03 -0.1364E-02	0.1083E-01 0.6809E-02 0.2104E-02 -0.1717E-02 -0.3729E-02 -0.3832E-02 -0.2638E-02 -0.1085E-02 0.3372E-04 0.3485E-03	0.6602E-02 0.1010E-01 0.1077E-01 0.9027E-02 0.5982E-02 0.2934E-02 0.8632E-03 0.1180E-03 0.4269E-03 0.1195E-02	-0.1523E-C8 -0.1690E-C8 -0.1689E-C8 -0.1497E-C8 -0.1151E-C8 -0.7315E-C9 -0.3271E-C9 0.1952E-11 0.2361E-O9	-C.2280E-C9 -0.1989E-09 -0.2381E-C9 -0.2875E-09 -0.2948E-09 -0.2380E-09 -0.1309E-09 -0.7377E-11 0.1013E-09 0.1785E-09	0.4459E-08 0.3635E-08 0.1677E-08 -0.3575E-09 -0.1554E-08 -0.1634E-08 -0.9870E-09 -0.2587E-09 0.1022E-09 0.2077E-10	0.1207E-10 0.2417E-08 0.3665E-08 0.3420E-08 0.2149E-08 0.7378E-09 -0.1113E-09 -0.2334E-09 0.6109E-10 0.4145E-09

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0.7500F 03 0.5236F 00 0.7813E 03 0.7749E-02 -0.4266E-02 0.1001E-01 0.3403E-02 -0.1419E-08 -0.6346E-C9 0.3765E-08 -0.2815E-09
0.2500F 03 0.1047E 01 0.6269E 03 0.7973E-02 -0.3225E-02 0.7318E-02 0.7704E-02 -0.1545E-08 -0.5389E-09 0.3301E-08 0.1881E-08
0.2500F 03 0.1571F 01 0.4627E 03 0.7693E-02 -0.1926E-02 0.3131E-02 0.9577E-02 -0.1569E-08 -0.4941E-09 0.1688E-08 0.3212E-08
0.2500F 03 0.2094F 01 0.3112F 03 0.6863E-02 -0.6569F-03 -0.9119E-03 0.8949F-02 -0.1464E-08 -0.4707E-09 -0.2148E-09 0.3250E-08
0.2500F 03 0.2618F 01 0.1887E 03 0.5596E-02 0.3098E-03 -0.3634E-02 0.6595E-02 -0.1244E-08 -0.4368E-09 -0.1545E-08 0.2241E-08
0.2500E 03 0.3142F 01
                      0.1018E 03 0.4132E-02 0.8248E-03 -0.4596E-02 0.3659E-02 -0.9514E-C9 -0.3745E-09 -0.1902E-08 0.8835E-09
0.2500F 03 0.3665E 01
                      0.4781E 02 0.2728E-02 0.9018E-03 -0.4067E-02 0.1173E-02 -0.6449E-09 -0.2852E-09 -0.1467E-08 -0.1478E-09
0.2500F 03 0.4189F 01
                      0.1884E 02 0.1564E-02 0.6699E-03 -0.2750E-02 -0.2948E-03 -0.3714E-C9 -0.1847E-09 -0.7408E-09 -0.5613E-09
0.2500F 03 0.4712E 01
                      0.5842E 01 0.7063E-03 0.2873E-03 -0.1386E-02 -0.7169E-03 -0.1548E-C9 -0.9118E-10 -0.1690E-09 -0.4717E-09
0.2500F 03 0.5236F 01 0.1661F 01 0.1334E-03 -0.1232E-03 -0.4645E-03 -0.4390E-03 0.2524E-11 -0.1628E-10 0.6394E-10 -0.1836E-09
0.2500F 03 0.5759F 01 0.1674F 01 -0.2131E-03 -0.4912E-03 -0.1346E-03 0.7837E-04 0.1099E-C9 0.3597E-10 0.1871E-10 0.3618E-10
0.3000F 03 0.5236F 00 0.6839F 03 0.7176E-02 -0.2396F-02 0.8847E-02 0.1160E-02 -0.1271E-08 -0.8228E-09 0.3090E-08 -0.3609E-09
0.3000F 03 0.1047E 01 0.5747E 03 0.7418E-02 -0.1810F-02 0.7359E-02 0.5721E-02 -0.1387E-08 -0.7062E-09 0.2898E-08 0.1508E-08
0.3000E 03 0.1571E 01 0.4491E 03 0.7266E-02 -0.9321E-03 0.3820E-02 0.8342E-02 -0.1427E-C8 +0.6258E-C9 0.1591E-08
0.3000F 03 0.2094F 01 0.3247F 03 0.6668E-02 0.1684E-04 -0.1507E-03 0.8533E-02 -0.1371E-08 -0.5664E-09 -0.1290E-09 0.3000E-08
0.3000F 03 0.2618F 01 0.2163F 03 0.5685E-02 0.8061F-03 -0.3220E-02 0.6775E-02 -0.1221E-08 -0.5082E-C9 -0.1461E-08 0.2182E-08
0.3000E 03 0.3142F 01 0.1325F 03 0.4484E-02 0.1281E-02 -0.4714E-02 0.4070E-02 -0.1005E-08 -0.4376E-09 -0.1946E-08 0.9156E-09
0.3000F 03 0.3665F 01 0.7446E 02 0.3266F-02 0.1409E-02 -0.4661E-02 0.1449E-02 -0.7630E-C9 -0.3527E-09 -0.1641E-08 -0.1665E-09
0.3000E 03 0.4189F 01 0.3824E 02 0.2195E-02 0.1262E-02 -0.3587E-02 +0.3931E-03 -0.5323E-09 -0.2616E-09 -0.9436E-09 -0.7142E-09
0.3000F 03 0.4712F 01 0.1780E 02 0.1352E-02 0.9578E-03 -0.2173E-02 -0.1246E-02 -0.3371E-09 -0.1757E-09 -0.2828E-09 -0.7417E-09
0.3000F 03 0.5236E 01 0.7403E C1 0.7414E-03 0.5983E-03 -0.9610E-03 -0.1290E-02 -0.1850E-09 -0.1033E-09 0.1042E-09 -0.4819E-09
0.3000F 03 0.5759F 01 0.2798E 01 0.3308E-03 0.2520F-03 -0.2179E-03 -0.8895E-03 -0.7324E-10 -0.4830E-10 0.2011E-09 -0.1880E-09
0.3500F 03 0.5236E 00 0.5985E 03 0.6415E-02 -0.8846E-03 0.7490E-02 -0.4083E-03 -0.1096E-08 -0.8881E-09 0.2456E-08 -0.3426E-09
0.3500F 03 0.1047F 01 0.5220E 03 0.6748E-02 -0.6598E-03 0.7092E-02 0.4085E-02 -0.1226E-08 -0.7763E-09 0.2485E-08 0.1229E-08
0.3500F 03 0.1571F 01 0.4252E 03 0.6717E-02 -0.1121E-03 0.4239E-02 0.7170E-02 -0.1285E-C8 -0.6857E-C9 0.1448E-08 0.2451E-08
0.3500F 03 0.2094F 01 0.3230E 03 0.6297E-02 0.5754E-03 0.4863E-03 0.7983E-02 -0.1264E-08 -0.6109E-09 -0.8158E-10 0.2736E-08
0.3500F 03 0.2618E 01 0.2285E 03 0.5525E-02 0.1200E-02 -0.2735E-02 0.6739E-02 -0.1162E-08 -0.5405E-09 -0.1362E-08 0.2066E-08
0.3500F 03 0.3142E 01 0.1507E 03 0.4524E-02 0.1609E-02 -0.4575E-02 0.4298E-02 -0.9980E-09 -0.4649E-09 -0.1907E-08 0.9000E-09
0.3500E 03 0.3665F 01 0.9301E 02 0.3461E-02 0.1743E-02 -0.4877E-02 0.1672E-02 -0.8018E-09 -0.3819E-09 -0.1688E-08 -0.1777E-09
0.3500F 03 0.4189F 01 0.5395E 02 0.2484F-02 0.1638E-02 -0.4026E-02 -0.3717E-03 -0.6051E-09 -0.2961E-05 -0.1029E-08 -0.7887E-09
0.3500F 03 0.4712E 01 0.2955E 02 0.1677E-02 0.1378E-02 -0.2641E-02 -0.1498E-02 -0.4301E-09 -0.2152E-C9 -0.3324E-09 -0.8839E-09
0.3500F 03 0.5236E 01 0.1532F 02 0.1064E-02 0.1052F-02 -0.1284E-02 -0.1768E-02 -0.2870E-09 -0.1457E-09 0.1363E-09 -0.6453E-09
0.350NE 03 0.5759F 01 0.7558E 01 0.6281E-03 0.7220E-03 -0.2962E-03 -0.1471E-02 -0.1767E-09 -0.9045E-10 0.3140E-09 -0.3120E-09
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TABLE II. - Continued. EARTH-PLANET ORBITER TRAJECTORIES

(c) Earth-Mars orbiter trajectories

TIME	PSI	J	AX(O)	AY(0)	AX(T)	AY(T)	AXDOT(O)	AYDOT(0)	AXDOT(T)	AYDOT(T)
0.5000F 02 0.5000F 02 0.5000F 02 0.5000F 02 0.5000F 02 0.5000F 02 0.5000E 02 0.5000F 02 0.5000F 02	0.1047E 01 0.1571E 01 0.2094F 01 0.2618E C1 0.3142E C1 0.3665E 01 0.4189F 01 0.4712F 01 0.5236E 01	0.1653E 04 0.4909F C4 0.9679E 04 0.1440E 05 0.1743E 05 0.2189E 05 0.2122E 00 0.1807E 05 0.1303E 05	0.2732E-01 0.4727E-02 0.4727E-02 0.3007E-01 0.6769E-01 0.9785E-01 0.9957E-01 0.9957E-01 0.9957E-01 0.9957E-01 0.1676E-01	0.3061E-01 0.4589E-01 0.4182E-01 0.1995E-01 -0.1011E-01 -0.6687E-01 -0.9974E-01 -0.99506E-01	-0.7406E-02 0.2435E-01 0.6193E-01 0.9502E-01 0.1140E 00 0.1186E 00 0.1014E 00 0.6945E-01 0.3153E-01	-0.3573E-01 -0.5632E-01 -0.5824E-01 -0.5824E-01 -0.4097E-01 -0.7393E-02 0.1950E-01 0.6018E-01 0.8505E-01	-0.3308E-C8 0.1389E-C7 0.3370E-C7 0.5102E-C7 0.6058E-C7 0.5406E-C7 0.4585E-C7 0.2943E-C7 0.1042E-C7	-0.1441E-07 -0.2127E-07 -0.1885E-07 -0.6950E-08 0.1065E-07 0.1733E-07 0.2850E-07 0.3748E-07	-0.3277E-08 0.1195E-07 0.2989E-07 0.4609E-07 0.5611E-07 0.5486E-07 0.2696E-07 0.2696E-07	-0.1603E-07 -0.2544E-07 -0.2655E-07 -0.1916E-07 -0.4430E-08 0.1974E-07 0.3733E-07 0.4469E-07 0.4276E-07
0.1000E 03 0.1000E 03 0.1000E 03 0.1000E 03 0.1000E 03 0.1000E 03 0.1000E 03 0.1000E 03 0.1000E 03	0.5236E 00 0.1047E 01 0.1571F 01 0.2094F 01 0.2618F 01 0.3142F 01 0.3665F 01 0.4189F 01 0.4712F 01 0.5236F 01 0.5759F 01	0.1452E 0: 0.1497E 0: 0.4911E 0: 0.9936F 0: 0.1442E 0: 0.1704E 0: 0.1792E 0: 0.3481E 0: 0.2955E 0:	3 0.1325E-01 3 0.8443E-02 3 0.1054E-03 3 -0.9557E-02 3 -0.1793E-01 4 -0.2297E-01 4 -0.2447E-01 4 -0.2394E-01 4 -0.5578E-02 0.1861E-02 0.9027E-02	0.7655E-03 0.5928E-02 0.6486E-02 0.2681E-02 -0.3444E-02 -0.8988E-02 -0.1265E-01 -0.3092E-01 -0.3019E-01	-0.6031E-02 -0.7800E-04 0.8738E-02 0.1785E-01 0.2437E-01 0.2571E-01 0.2078E-01 0.2330E-01 0.1395E-01	-0.8226E-03 -0.8360E-02 -0.1178E-01 -0.1006E-01 -0.3304E-02 0.6956E-02 0.1751E-01 0.1957E-01 0.2444E-01	-0.2573E-08 -0.2183E-C9 0.2811E-C8 0.5727E-C8 0.7701E-C8 0.8410E-C8 0.8345E-08 0.2824E-08 0.5862E-09	-0.4312E-09 -0.1280E-08 -0.1047E-08 0.3012E-09 0.2239E-08 0.3824E-08 0.4608E-08 0.3352E-08	-0.1571E-08 -0.6337E-10 0.2194E-08 0.4716E-C8 0.6700E-08 0.7218E-08 0.5815E-08	-0.2793E-09 -0.2061E-08 -0.3024E-08 -0.2758E-08 -0.1058E-08 0.1799E-08 0.4839E-08 0.6564E-08
0.1500F 03 0.1500F 03 0.1500F 03 0.1500F 03 0.1500F 03 0.1500F 03 0.1500F 03 0.1500F 03 0.1500F 03 0.1500F 03	0.3665E 01 0.4189E 01 0.4712E 01 0.5236E 01	0.2142E 0 0.5522E 0 0.3122E 0 0.1063E 0 0.2193E 0 0.3167E 0 0.3759E 0 0.4000E 0 0.1479E 0	3 0.1024E-01 3 0.8290E-02 2 0.4636E-02 2 0.1412E-03 3 -0.4072E-02 3 -0.8540E-02 3 -0.8825E-02 4 0.5872E-02 4 0.8411E-02	-0.1616E-02 0.1204E-02 0.2135E-02 0.1145E-02 -0.1085E-02 -0.3535E-02 -0.5526E-02 -0.6913E-02 -0.1477E-01	-0.4041E-02 -0.2642E-02 0.6386E-03 0.4728E-02 0.8226E-02 0.8763E-02 0.5353E-02 0.9729E-02	0.3809E-02 -0.4195E-03 -0.3228E-02 -0.3784E-02 -0.1876E-02 0.1909E-02 0.6241E-02 0.9599E-02 0.1100E-01	-0.2003E-08 -0.1226E-C8 -0.1359E-09 -0.1003E-08 -0.1907E-C8 -0.2420E-C8 -0.2571E-08 -0.9134E-09	-0.1933E-09 -0.3580E-C9 -0.2559E-C9 0.1351E-C9 0.6898E-09 0.1194E-08 0.1506E-08 0.157E-08	-0.6535E-09 -0.4181E-09 0.1425E-09 0.9459E-09 0.1713E-08 0.2073E-08 0.1807E-08 0.9803E-09	0.5157E-09 -0.1056E-09 -0.6133E-09 -0.7698E-09 -0.4038E-09 0.4212E-09 0.1380E-08 0.2077E-08
0.2000F 03 0.2000F 03 0.2000F 03 0.2000F 03 0.2000F 03 0.2000F 03 0.2000F 03 0.2000F 03 0.2000F 03 0.2000F 03	0.5236E 00 0.1047E 01 0.1571E 01 0.2094E 01 0.2618E 01 0.3142E 01 0.3665E C1 0.4189E 01 0.4712E 01 0.5236E 01 0.5759E 01	0.1108E 0 0.2906E 0 0.9739E 0 0.3043E 0 0.6502E 0 0.9563E 0 0.1156E 0	3 0.7784E-02	-0.1218E-02 0.5689E-03 0.1402E-02 0.1164E-02 0.1230E-03 -0.1232E-02 -0.2489E-02 -0.3462E-02 -0.4132E-02	-0.2684E-02 -0.2803E-02 -0.1532E-02 0.6099E-03 0.2809E-02 0.4217E-02 0.4285E-02 0.2983E-02 0.7510E-03	0.4782E-02 0.2020E-02 -0.2758E-03 -0.1429E-02 -0.1128E-02 0.4359E-03 0.2599E-02 0.4511E-02	2 -0.1331E-08 3 -0.7751E-09 2 -0.1513E-09 2 0.4030E-09 0 0.7928E-09 2 0.1085E-08 2 0.1085E-08 2 0.1086E-08	-0.3990E-09 -0.3883E-C9 -0.2931E-09 -0.9501E-10 0.1666E-09 0.4157E-C9 0.5905E-09 0.6722E-09	-0.2276E-09 -0.2765E-09 -0.1619E-09 0.1366E-09 0.5057E-09 0.7499E-09 0.4206E-09 -0.4407E-10	0.5262E-09 0.2837E-09 -0.9276E-11 -0.2051E-09 -0.1655E-09 0.1252E-09 0.5321E-09 0.8597E-09 0.9626E-09

```
0.2500F 03 0.5236E 00 0.4237E 03 0.7894E-02 -0.1821E-02 0.5466E-04 0.6230E-02 -0.1547E-08 -0.6072E-09 0.1186E-09 0.4132E-09
0.2500F 03 0.1047E 01 0.2765E 03 0.7196E-02 -0.4423E-03 -0.1736E-02 0.4896E-02 -0.1491E-08 -0.5355E-09 -0.3287E-11 0.4598E-09
0.2500E 03 0.1571E 01 0.1509E 03 0.5815E-02 0.7507E-03 -0.2512E-02 0.2960E-02 -0.1282E-08 -0.4666E-09 -0.1415E-09
0.2500F 03 0.2094E 01 0.6345E 02 0.3965E-02 0.1416E-02 -0.2196E-02 0.1047E-02 -0.9434E-09 -0.3684E-09 -0.1948E-09
           0.2618E 01 0.1737E 02 0.2011E-02 0.1413E-02 -0.1039E-02 -0.2742E-03 -0.5387E-09 -0.2277E-09 -0.1055E-09
0.2500E 03 0.3142F 01
                      0.4305E 01 0.3215E-03 0.8428E-03 0.4460E-03 -0.6580E-03 -0.1486E-09 -0.5897E-10 0.8504E-10 -0.5190E-10
0.2500F 03 0.3665E 01 0.1028E 02 -0.8758E-03 -0.2382E-04 0.1655E-02 -0.1049E-03 0.1619E-09 0.1035E-09 0.2590E-09 0.3307E-10
0.2500F 03 0.4189E 01 0.2283E 02 -0.1554E-02 -0.9136E-03 0.2127E-02 0.1037E-02 0.3683E-09 0.2275E-09 0.3063E-09 0.2212E-09
0.2500F 03 0.4712F 01 0.3463E 02 -0.1817E-02 -0.1663E-02 0.1719E-02 0.2231E-02 0.4827E-09 0.2984E-09 0.1951E-09 0.4004E-09
0.2500F 03 0.5236F 01 0.4302E 02 -0.1795E-02 -0.2217E-02 0.6199E-03 0.2995E-02 0.5321E-09 0.3183E-09 -0.2389E-10 0.4741E-09
0.2500F 03 0.5759E 01 0.4818E 02 -0.1596E-02 -0.2578E-02 -0.7853E-03 0.3054E-02 0.5425E-09 0.2958E-09 -0.2602E-09 0.4033E-09
0.3000F 03 0.5236E 00 0.3898E 03 0.7044E-02 -0.5536F-03 0.7595E-03 0.5433E-02 -0.1342E-08 -0.6914E-09 0.2372E-09 0.2641E-09
0.3000E 03 0.1047E 01 0.2772E 03 0.6585E-02 0.2844E-03 -0.1042E-02 0.4742E-02 -0.1325E-C8 -0.5992E-09 0.1253E-09 0.3946E-09
0.3000E 03 0.1571F 01 0.1730E 03 0.5613E-02 0.1091E-02 -0.2140E-02 0.3345E-02 -0.1199E-08 -0.5127E-09 -0.4420E-10
                      0.9119E 02 0.4249E-02 0.1599E-02 -0.2351E-02 0.1728E-02 -0.9723E-09 -0.4153E-09 -0.1732E-09 0.2972E-09
0.3000F 03 0.2094E 01
                      0.3796F 02 0.2739E-02 0.1663E-02 -0.1772E-02 0.3841E-03 -0.6845E-C9 -0.2985E-C9 -0.1880E-09 0.1308E-09
0.3000F 03 0.2618F 01
                      0.109E 02 0.1352E-02 0.1308E-02 -0.7390E-03 -0.3309E-03 -0.3887E-09 -0.1685E-09 -0.9276E-10 0.1079E-10
0.3000F 03 0.3142E 01
                      0.2563E 01 0.2797E-03 0.6922E-03 0.2928E-03 -0.3147E-03 -0.1330E-09 -0.4368E-10 0.3632E-10 -0.1145E-11
0.3000F 03 0.3665F 01
0.3000F 03 0.4189F 01
                      0.4061F 01 -0.4183E-03 0.7494F-05 0.9234E-03 0.2578E-03 0.5708E-10 0.5677E-10 0.1105E-09 0.7966E-10
0.3000E 03 0.4712E 01
                      0.9109E 01 -0.7864E-03 -0.6095E-03 0.9602E-03 0.1031E-02 0.1810E-09 0.1224E-09 0.8711E-10 0.1843E-09
0.3000F 03 0.5236F 01 0.1430E 02 -0.9098F-03 -0.1096E-02 0.4583E-03 0.1638E-02 0.2523E-09 0.1527E-09 -0.1599E-10 0.2423E-09
0.3000F 03 0.5759E 01 0.1842E 02 -0.8691E-03 -0.1438E-02 -0.3535E-03 0.1830E-02 0.2873E-09 0.1527E-09 -0.1449E-09 0.2174E-09
0.3500F 03 0.5236E 00 0.3589F C3 0.6250E-02 0.3874E-03 0.1231E-02 0.4749E-02 -0.1173E-08 -0.7035E-09 0.3011E-09 0.1648E-09
0.3500F 03 0.1047E 01 0.2704F 03 0.5981E-02 0.8809E-03 -0.5128E-03 0.4492E-02 -0.1185E-C8 -0.6159E-C9 0.2030E-09
                                                                                                                  0.3398E-09
0.3500F 03 0.1571E 01
                      0.1834E 03 0.5284E-02 0.1423E-02 -0.1774E-02 0.3482E-02 -0.1110E-08 -0.5294E-09 0.2393E-10 0.4052E-09
0.3500F 03 0.2094F 01
                      0.1096E 03 0.4242E-02 0.1800F-02 -0.2306E-02 0.2105E-02 -0.9517E-09 -0.4369E-09 -0.1423E-09 0.3378E-09
0.3500F 03 0.2618F 01 0.5599F 02 0.3032F-02 0.1871E-02 -0.2101E-C2 0.7971E-03 -0.7362E-C9 -0.3340E-C9 -0.2148E-09 0.1888E-09
0.3500F 03 0.3142E 01 0.2326F 02 0.1862E-02 0.1622E-02 -0.1381E-02 -0.8762E-04 -0.5020E-09 -0.2245E-09 -0.1764E-09 0.4861E-10
0.3500F 03 0.3665F 01 0.7208F 01 0.8996E-03 0.1149E-02 -0.5008E-03 -0.3857E-03 -0.2865E-09 -0.1197E-09 -0.7774E-10 -0.1477E-10
0.3500E 03 0.4189E 01 0.1847E 01 0.2160E-03 0.5899E-03 0.1870E-03 -0.1649E-03 -0.1139E-09 -0.3238E-10 0.6589E-11 0.6075E-11
0.3500F 03 0.4712F 01 0.1952F 01 -0.2003F-03 0.5794E-04 0.4668F-03 0.3335E-03 0.9609E-11 0.2963E-10 0.2912E-10 0.6803E-10
%a500F 03 0.5236F 01 0.4126F 01 -0.4050E-03 -0.3842F-03 0.3153E-03 0.8202E-03 0.9019E-10 0.6515E-10 -0.1106E-10 0.1163E-09
0.3500F 03 0.5759F 01 0.6647F 01 -0.4595F-03 -0.7150F-03 -0.1358E-03 0.1072E-02 0.1384E-09 0.7726E-10 -0.8170E-10 0.1162E-09
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TABLE II. - Continued. EARTH-PLANET ORBITER TRAJECTORIES

(d) Earth-Jupiter orbiter trajectories

TIME	PSI	J	AX(0)	AY (0)	AX(T)	AY(T)	A XDOT (O)	AYDOT(O)	AXDOT(T)	AYDOT(T)
0.2000F 03 0.2000F 03 0.2000F 03 0.2000F 03 0.2000F 03 0.2000F 03 0.2000F 03 0.2000F 03 0.2000F 03	0.5236F 00 0.1047F 01 0.1571F 01 0.2094F 01 0.2618F 01 0.3142F 01 0.3165F 01 0.4189F 01 0.4712F 01 0.5236F 01 0.5759F 01	0.1182F 04 0.1419E 04	0.1178E-01 0.3857F-02 -0.4478E-02 -0.1112E-01 -0.1460E-01 -0.1510F-01 0.1480E-02 0.6102E-02 0.1199F-01	0.8155E-02 0.1095E-01 0.9664E-02 0.4835E-02 -0.1567E-02 -0.6803E-02 -0.1903E-01 -0.1990E-01	-0.8278E-02 -0.1095E-02 0.6872E-02 0.1345E-01 0.1681E-01 0.1589E-01 0.1349E-01 0.5805E-02 -0.2598E-02	-0.8492E-02 -0.1223E-01 -0.1192E-01 -0.7732E-02 -0.8221E-03 0.7049E-02 0.1452E-01 0.1879E-01 0.1845E-01	0.1967E-C8 0.3110E-C8	-0.1174E-08 -0.1C79E-C8 -0.5102E-C9 0.4982E-C9 0.1679E-C8 0.2510E-C8 -0.7957E-C9 -0.3413E-C9 -0.4187E-10	-0.1012E-08 -0.1479E-09 0.7917E-09 0.1562E-08 0.1957E-08 0.1853E-08 0.1454E-08 0.4790E-09 -0.5255E-09	-0.9124E-09 -0.1339E-08 -0.1299E-08 -0.8225E-09 -0.4560E-10 0.8462E-09 0.2070E-08 0.2512E-08 0.2384E-08
0.3000F 03 0.3000F 03 0.3000F 03 0.3000F 03 0.3000F 03 0.3000F 03 0.3000F 03 0.3000F 03	0.5236F 00 0.1047E 01 0.1571F 01 0.2094F 01 0.2618F 01 0.3142E 01 0.3665F 01 0.4189F 01 0.4712F 01 0.5236F 01 0.5759F 01	0.3213F 03 0.3747F 03 0.4052F 03 0.4172E 03 0.4201F 03	0.8053F-02 0.4383F-02	0.3898E-02 0.5167E-02 0.4720F-02 0.2756E-02 0.3987E-04 -0.2464E-02 -0.4257E-02 -0.5384E-02 -0.6033E-02	-0.4697E-02 -0.1684E-02 0.1859E-02 0.4957E-02 0.6746E-02 0.6699E-02 0.4797E-02 0.1570E-02 -0.2102E-02	-0.2620E-02 -0.4683E-02 -0.4984E-02 -0.3501E-02 -0.6802E-03 0.2683E-02 0.5608E-02 0.7214E-02	0.1197E-C8 0.1189E-C8 0.1141E-C8	-0.6755E-C9 -C.4958E-C9 -0.2C31E-09 0.1809E-C9 0.5714E-09 0.8496E-09 0.9614E-C9 0.9360E-C9 0.8150E-C9	-0.4052E-09 -0.1528E-09 0.1341E-09 0.3830E-09 0.5287E-09 0.5275E-09 0.3752E-09 0.1141E-09 -0.1836E-09	-0.1874E-09 -0.3456E-09 -0.3671E-09 -0.2529E-09 -0.3590E-10 0.2255E-09 0.4543E-09 0.5775E-09 0.5541E-09
0.4000F 03 0.4000F 03 0.4000F 03 0.4000F 03 0.4000F 03 0.4000F 03 0.4000F 03 0.4000F 03	0.5236F 00 0.1047F 01 0.1571F 01 0.2094F 01 0.2618F 01 0.3142F 01 0.3665F 01 0.4189F 01 0.4712F 01 0.5736E 01	0.1030F 03 0.1250F 03 0.1426F 03 0.1534F 03 0.1595F 03	0.6241E-02 0.4103E-02	0.3010E-02 0.3649E-02 0.3399F-02 0.2327E-02 0.7969E-03 -0.7185E-03 -0.1917E-02 -0.2739E-02 -0.3235E-02	-0.3289E-02 -0.1699E-02 0.2931E-03 0.2136E-02 0.3320E-02 0.3511E-02 0.2657E-02 0.1013E-02 -0.9556E-03	-0.8234E-03 -0.2218E-02 -0.2644E-02 -0.2038E-02 -0.6131E-03 0.1199E-02 0.2851E-02 0.3838E-02	0.1386E-C9 0.3780E-C9 0.5005E-C9 0.5436E-C9	-0.5821E-09 -0.4171E-09 -0.2180E-C9 0.2133E-11 0.2079E-09 0.3559E-C9 0.4244E-09 0.42C5E-C9 0.3603E-C9	-0.2219E-09 -0.1157E-09 0.9341E-11 0.1236E-09 0.1979E-09 0.2111E-09	-0.4856E-10 -0.1281E-09 -0.1508E-09 -0.1140E-09 -0.2881E-10 0.8065E-10 0.1809E-09 0.2397E-09 0.2372E-09
0.5000F 03 0.5000F 03 0.5000F 03 0.5000F 03 0.5000F 03 0.5000F 03 0.5000F 03 0.5000F 03 0.5000F 03	0.5236E 00 0.1047F 01 0.1571E C1 0.2094F 01 0.2618F 01 0.3142E C1 0.3665F 01 0.4189E 01 0.4712E 01 0.5759E 01	0.5081F 02 0.5999F 02 0.6737F 02 0.7256E 02	0.5019E-02 0.3649F-02 0.2074E-02	0.2816E-02 0.3127E-02 0.2925E-02 0.2219E-02 0.1201F-02 0.1460E-03 -0.7441E-03 -0.1396E-02 -0.1815E-02	-0.2558E-02 -0.1606E-02 -0.3321E-03 0.9130E-03 0.1789E-02 0.2057E-02 0.1656E-02 0.7181E-03 -0.4774E-03	-0.1229E-03 -0.1167E-02 -0.1606E-02 -0.1372E-02 -0.5710E-03 0.5342E-03 0.1597E-02 0.2288E-02 0.2396E-02	-0.9139E-C9 -0.6527E-C9 -0.3678E-C9 -0.1108E-C9 0.8125E-10 0.2028E-C9 0.2626E-C9 0.2863E-O9	-0.5221E-09 -0.3856E-C9 -0.2357E-C9 -0.8217E-10 0.5577E-10 0.1570E-09 0.2105E-09 0.2185E-09 0.1896E-09	-0.1418E-09 -0.8689E-10 -0.2081E-10 0.4216E-10 0.8686E-10 0.1010E-09 0.8016E-10 0.3185E-10	-0.1242E-10 -0.5872E-10 -0.7653E-10 -0.6346E-10 -0.2350E-10 0.3191E-10 0.8548E-10 0.1195E-09

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0.4646F-02 -0.2282E-02 0.1239E-02 -0.9315E-09 -0.5481E-09 -0.1184E-09 0.3899E-10
0.6000F 03 0.1047F 01 0.1420F 03 0.4072F-02 0.2761E-02 -0.2112E-02 0.1793E-03 -0.9084E-09 -0.4601E-09 -0.9880E-10 -0.2310E-11
0.6000F 03 0.1571F 01 0.9040F 02 0.3175E-02 0.2892F-02 -0.1495E-02 -0.6481E-03 -0.7959E-09 -0.3536E-09 -0.6637E-10 -0.3132E-10
0.6000F 03 0.2094F 01 0.5288F 02 0.2067F-02 0.2704F-02 -0.6105E-03 -0.1069E-02 -0.6201E-09 -0.2370E-09 -0.2715E-10 -0.4457E-10
0.6000F 03 0.2618F 01 0.3174F 02 0.9877E-03 0.2179E-02 0.2995E-03 -0.1014E-02 -0.4160E-09 -0.1201E-C9 0.1152E-10 -0.4019E-10
0.4000F 03 0.2142F 01 0.2418F 02 0.1268E-03 0.1428F-02 0.9913E-03 -0.5395E-03 -0.2209E-C9 -0.1589E-10 0.4104E-10 -0.1940E-10
0.6000F 03 0.3665F 01 0.2487F 02 -0.4269E-03 0.6259E-03 0.1283E-02 0.1873E-03 -0.6308E-10 0.6268E-10 0.5357E-10 0.1203E-10
0.4000F 03 0.4189F 01 0.2889F 02 -0.6914E-03 -0.8265E-04 0.1110E-02 0.9292E-03 0.4676E-10 0.1087E-09 0.4541E-10 0.4422E-10
0.4712F 01 0.3332F 02 -0.7392E-03 -0.6288E-03 0.5424E-03 0.1451E-02 0.1137E-09 0.1229E-09 0.1929E-10 0.6632E-10
0.4600F 03 0.5236F 01 0.3705F 02 -0.6449F-03 -0.1001E-02 -0.2389E-03 0.1591E-02 0.1489E-09 0.1106E-09 -0.1644E-10 0.7063E-10
0.6000F 03 0.5759F 01 0.4013F 02 -0.4638E-03 -0.1207F-02 -0.1009E-02 0.1301E-02 0.1626E-C9 0.7756E-10 -0.5111E-10 0.5488E-10
0.8000F 03 0.5236F 00 0.1361F 03 0.2570F-02 0.2521F-02 -0.1589E-02 0.1030E-02 -0.5874E-09 -0.3521E-09 -0.6504E-10 0.1719E-10
0.8000F 03 0.1047F 01 0.1063E 03 0.2649E-02 0.2614F-02 -0.1578E-02 0.3643E-03 -0.6395E-09 -0.3342E-09 -0.5487E-10 -0.1959E-12
          0.1571F 01 0.7471E C2
                                0.2322F-02 0.2615F-02 -0.1282E-02 -0.2067E-03 -0.6143E-09 -0.2816E-09 -0.4055E-10 -0.1254E-10
                                0.1758F-02 0.2455F-02 -0.7894E-03 -0.5692E-03 -0.5326E-C9 -0.2120E-09 -0.2384E-10 -0.1944E-10
          0.2094F 01 0.4750F C2
          0.26185 01 0.2807E 02
                                C.8000F 03 0.3142F 01 0.1673E 02 0.5509E-03 0.1624F-02 0.2532F-03 -0.4896E-03 -0.2949E-C9 -0.6896E-10 0.8422E-11 -0.1352E-10
0.8000F 03 0.3665F 01 0.1171F 02 0.1256F-03 0.1085F-02 0.5388E-03 -0.1315E-03 -0.1832E-09 -0.1380E-10 0.1732E-10 -0.1382E-11
0.8000F 03 0.4189E 01 0.1056F 02 -0.1347F-03 0.5782E-03 0.5658E-03 0.2869E-03 -0.9434E-1C 0.2330E-10 0.1750E-10 0.1278E-10
0.8000F 03 0.4712E 01 0.1128E 02 -0.2528F-03 0.1573E-03 0.3493E-03 0.6274E-03 -0.3059E-10 0.4186E-10 0.9055E-11 0.2403E-10
0.8000F 03 0.5236F C1 0.1264F C2 -0.2659F-03 -0.1568F-03 -0.2662E-04 0.7826E-03 0.1128E-10 0.4425E-1C -0.4982E-11 0.2824E-10
0.8000F 03 0.5759F 01 0.1411F 02 -0.2090F-03 -0.3614E-03 -0.4398E-03 0.7039E-03 0.3607E-10 0.3389E-10 -0.1989E-10 0.2362E-10
0.1000F 04 0.5236F 00 0.9790F 02 0.1228F-02 0.2133F-02 -0.1193F-02 0.8277F-03 -0.3621F-C9 -0.1846F-09 -0.3915F-10 0.5468F-11
                               0.1640F-0? 0.2328E-02 -0.1247E-02 0.3756E-03 -0.4592E-C9 -0.2227E-09 -0.3291E-10 -0.1826E-11
          0.1047F 01 0.8305F 02
          0.1571F 01 0.6354F C2
                               0.1644E-02 0.2358E-02 -0.1100E-02 -0.4730E-04 -0.4821E-C9 -0.2119E-C9 -0.2562E-10 -0.6811E-11
          0.2094F 01 0.4421F 02 0.1389E-02 0.2252E-02 -0.7955F-03 -0.3550E-03 -0.4512E-09 -0.1753E-09 -0.1778E-10 -0.1009E-10
          0.2618F 01 0.2836F 02 0.1010F-02 0.2009F-02 -0.4129E-03 -0.4925E-03 -0.3854E-09 -0.1277E-09 -0.9341E-11 -0.1133E-10
0.1000F 04 0.3142F 01 0.1733F 02 0.6216E-03 0.1661F-02 -0.4730E-04 -0.4475E-03 -0.3036E-09 -0.7948E-10 -0.1073E-11 -0.9563E-11
0.1000F 04 0.3665F 01 0.1080F 02 0.2978F-03 0.1260E-02 0.2136E-03 -0.2557E-03 -0.2216E-C9 -0.3790E-10 0.5139E-11 -0.4508E-11
0.1000F 04 0.4189F 01 0.7606F 01 0.7130F-04 0.8651E-03 0.3144E-03 0.8562E-05 -0.1501E-C9 -0.7167E-11 0.7335E-11 0.2549E-11
0.1000F 04 0.4712E 01 0.6460F 01 -0.5886E-04 0.5192F-03 0.2480E-03 0.2546E-03 -0.9380E-10 0.1145E-10 0.4804E-11 0.9083E-11
0.1000F 04 0.5236F 01 0.6389F 01 -0.1105F-03 0.2442F-03 0.5566F-04 0.4037E-03 -0.5279E-10 0.1891E-10 -0.1371E-11 0.1255E-10
0.1000F 04 0.5759F 01 0.6797F 01 -0.1057E-03 0.4701E-04 -0.1894E-03 0.4111E-03 -0.2500E-10 0.1728E-10 -0.8813E-11 0.1149E-10
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TABLE II. - Continued. EARTH-PLANET ORBITER TRAJECTORIES

(e) Earth-Saturn orbiter trajectories

TIME	PST	J	AX(O)	AY (0)	AX(T)	AY(T)	AXDOT (O)	AYDOT(O)	(T) TODXA	AYDOT(T)
9.4000F 03 0.4000F 03 0.4000F 03 0.4000F 03 0.4000F 03 0.4000F 03 0.4000F 03 0.4000F 03	0.5236F 00 0.1047F 01 0.1571F 01 0.2094F 01 0.2618F 01 0.3142F 01 0.3665F 01 0.4189F 01 0.4712F 01 0.5759F 01	0.4814F 03 0.5317E 03 0.5592F 03 0.5699E 03 0.5739E 03	0.1075F-01 0.7966E-02 0.4112E-02 0.7722E-04 -0.3208E-02 -0.5101E-02 -0.5599F-02 -0.5251E-02 -0.4553E-02 -0.3722E-02 0.1137E-01	0.5321E-07 0.6355E-02 0.5578E-02 0.3234E-02 0.1620E-03 -0.2559E-02 -0.4409E-02 -0.5510E-02 -0.6102E-02	-0.4525E-02 -0.1157E-02 0.2502E-02 0.5467E-02 0.6940E-02 0.6515E-02 0.4296E-02 0.8918E-03 -0.2781E-02	-0.4032E-02 -0.5676E-02 -0.5449E-02 -0.3474E-02 -0.3296E-03 0.3120E-02 0.5914E-02 0.7241E-02 0.6703E-02	0.9563E-09 0.1043E-08 0.1032E-08 0.9845E-09	-0.6443E-C9 -0.4220E-09 -0.1123E-C9 0.2638E-09 0.6308E-09 0.8748E-C9 0.9461E-09 0.8839E-C9 0.7289E-09	-0.2838E-09 -0.8151E-10 0.1341E-09 0.3072E-09 0.3933E-09 0.3698E-09 0.421E-09 0.4535E-10 -0.1673E-09	-0.2138E-09 -0.3087E-09 -0.2954E-09 -0.1834E-09 -0.6676E-11 0.1870E-09 0.3438E-09 0.4167E-09
0.6000F 03 0.6000F 03 0.6000F 03 0.6000F 03 0.6000F 03 0.6000F 03 0.6000F 03 0.6000F 03	0.5236F 00 0.1047F 01 0.1571E 01 0.2694F 01 0.2618F 01 0.3142F 01 0.3665F 01 0.4189F 01 0.4712F 01 0.5236F 01 0.5759F 01	0.1148F 03 0.1291F 03 0.1418F 03 0.1506E 03 0.1565F 03	0.5213E-02 0.3442F-02	0.3608E-02 0.3915E-02 0.3499F-02 0.2430E-02 0.1018E-02 -0.3403E-03 -0.1394E-02 -0.2098E-02 -0.2497E-02	-0.2589E-02 -0.1124E-02 0.5354E-03 0.1949E-02 0.2747E-02 0.2722E-02 0.1891E-02 0.4944E-03 -0.1082E-02	-0.1383E-02 -0.2285E-02 -0.2363E-02 -0.1638E-02 -0.3401E-03 0.1154E-02 0.2415E-02 0.3077E-02 0.2943E-02	0.3454E-09 0.3535E-09	-0.5030E-09 -0.3402E-C9 -0.1628E-09 0.1583E-10 0.1702E-09 0.2723E-C9 0.3100E-09 0.2913E-09 0.2292E-09	-0.1147E-09 -C.5304E-10 0.1417E-10 0.7067E-10 0.1028E-09 0.1026E-09 0.7070E-10 0.1618E-10 -0.4573E-10	-0.5012E-10 -0.8479E-10 -0.8727E-10 -0.5925E-10 -0.9651E-11 0.4740E-10 0.9558E-10 0.1204E-09 0.1140E-09
0.8000F 03 0.8000F 03 0.8000F 03 0.8000F 03 0.8000F 03 0.8000F 03 0.8000F 03 0.8000F 03 0.8000F 03	0.5236F 00 0.1C47F 01 0.1571F 01 0.2094F 01 0.2618F 01 0.3142F 01 0.3665F 01 0.4189F 01 0.4712F 01 0.5736F 01 0.5759F 01	0.4710F 02 0.5195F 02 0.5664F 02 0.6053F 02	0.3660F-02 0.2733E-02 0.1623E-02	0.3128E-02 0.3180F-02 0.2869E-02 0.2210E-02 0.1346E-02 0.4772E-03 -0.2482E-03 -0.7737E-03 -0.1101F-02	-0.1831E-02 -0.1011E-02 -0.5013E-04 0.8068E-03 0.1343E-02 0.1428E-02 0.1053E-02 0.3348E-03 -0.5198E-03	-0.6060E-03 -0.1204E-02 -0.1343E-02 -0.1018E-02 -0.3426E-03 0.4796E-03 0.1208E-02 0.1630E-02 0.1619E-02	-0.8860E-09 -0.8662E-C9 -0.7533E-09 -0.5786E-C9 -0.3787E-C9 -0.1907E-09 -0.4264E-10 0.5652E-10 0.1139E-09 0.1415E-C9	-0.4057E-C9 -0.2968E-09 -0.1793E-09 -0.65538E-10 0.3100E-10 0.9745E-10 0.1289E-09 0.1283E-09 0.1023E-09	-0.6322E-10 -0.3559E-10 -0.5336E-11 0.2100E-10 0.3754E-10 0.4055E-10	-0.1929E-10 -0.3595E-10 -0.3907E-10 -0.2898E-10 -0.8963E-11 0.1528E-10 0.3676E-10 0.4906E-10 0.4824E-10
0.1000F 04 0.1000F 04 0.1000F 04 0.1000F 04 0.1000F 04 0.1000F 04 0.1000F 04 0.1000F 04 0.1000F 04 0.1000F 04	0.5236F 00 0.1047F 01 0.1571F 01 0.2094F 01 0.2618F 01 0.3142F 01 0.3665F 01 0.4189F 01 0.4712F 01 0.5236F 01 0.5759F 01	0.2666E 02 0.2884F 02	0.2576E-02 0.2121F-02 0.1450F-02 0.7607E-03 0.1959F-03	0.2813E-02 0.2792F-02 0.2547E-02 0.2079E-02 0.1470F-02 0.8394E-03 0.2860F-03 -0.1396F-03 -0.4266E-03	-0.1428E-02 -0.8994E-03 -0.2630E-03 0.3274E-03 0.7291E-03 0.8490E-03 0.6699E-03 0.2553E-03 -0.2695E-03	-0.3244E-03 -0.7547E-03 -0.8981E-03 -0.7390E-03 -0.3390E-03 0.1781E-03 0.6595E-03 0.9641E-03	3 -0.6113E-09 3 -0.6541E-09 3 -0.6104E-09 3 -0.5092E-09 3 -0.3790E-09 3 -0.2467E-09 3 -0.1332E-09 3 -0.4848E-10 0.7949E-11 0.4158E-10 0.5831E-10	-0.3139E-09 -0.2489E-09 -0.1696E-09 -0.8972E-10 -0.2046E-10 0.5795E-10 0.6484E-10 0.5457E-10	-0.4029E-10 -0.2495E-10 -0.8363E-11 0.6400E-11 0.1639E-10 0.1950E-10	-0.1123E-10 -0.2014E-10 -0.2230E-10 -0.1771E-10 -0.7758E-11 0.4847E-11 0.1655E-10 0.2388E-10 0.2453E-10

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0.1200F 04 0.5236E 00 0.1024E 03 0.1450E-02 0.2305E-02 -0.1375E-02 0.2376E-03 -0.4140E-09 -0.2097E-09 -0.3538E-10 -0.5713E-12
                                  0.1765F-02 0.2497E-02 -0.1170E-02 -0.2144E-03 -0.5009E-09 -0.2310E-09 -0.2769E-10 -0.8665E-11
           0.1047F 01
                      0.8412F 02
                       0.6221F 02
           0.1571F 01
                                  0.1615E-02
                                             0.2495E-02 -0.7987E-03 -0.5378E-03 +0.5013E-C9 -0.2015E-09 -0.1802E-10 -0.1357E-10
                       0.4251E 02
                                  0.1220E-02 0.2312E-02 -0.3416E-03 -0.6692E-03 -0.4454E-C9 -0.1500E-09 -0.7814E-11 -0.1481E-10
           0.2094E 01
                                              0.1962E-02 0.9741F-04 -0.5891E-03 -0.3580E-C9 -0.9268E-10 0.1388E-11 -0.1228E-10
                      0.2812F C2 0.7514F-03
           0.2618F 01
                      0.1958E 02 0.3318E-03 0.1501F-02
                                                         0.4171E-03 -0.3317E-03 -0.2612E-C5 -0.4030E-10 0.7971E-11 -0.6605E-11
           0.3142F 01
           0.3665F 01 0.1569E 02 0.2812E-04 0.1011F-02
                                                         0.5464E-03 0.2249E-04 -0.1720E-C9 0.2442E-13 0.1064E-10 0.8368E-12
                                                         0.4652E-03 0.3686E-03 +0.1001E-C9 0.2501E-10 0.8933E-11 0.8040E-11
           0.4189F 01 0.1470E 02 -0.1460F-03 0.5639E-03
           0.4712F 01 0.1516F 02 -0.2105F-03 0.2038E-03 0.2096E-03 0.6056E-03 -0.4803E-10 0.3490E-10 0.3514E-11 C.1291E-10
           0.5236F 01 0.1617E 02 -0.1960E-03 -0.5424E-04 -0.1382E-03 0.6648E-03 -0.1349E-10 0.3214E-1C -0.3891E-11 0.1395E-10
           0.5759F 01 0.1733E 02 -0.1317E-03 -0.209F-03 -0.4743E-03 0.5272E-03 0.6952E-11 0.2000E-10 -0.1103E-10 0.1071E-10
0.1400F 04 0.5236F 00 0.7654F 02 0.5732F-03 0.1748E-02 -0.1132E-02 0.1579E-03 -0.2557E-09 -0.9207E-10 -0.2523E-10 -0.3161E-11
           0.1047F 01 0.6708F 02 0.1142F-02 0.2155E-02 -0.9831E-03 -0.1708E-03 -0.3835E-09 -0.1587E-09 -0.1981E-10 -0.7615E-11
           0.1571E C1 0.5238F 02
                                 0.1202F-02 0.2226E-02 -0.7094E-03 -0.4211E-03 -0.4150E-C9 -0.1579E-C9 -0.1326E-10 -0.1028E-10
           0.2094F 01 0.3745E 02 0.9955E-03 0.2110E-02 -0.3639E-03 -0.5368E-03 -0.3899E-09 -0.1279E-09 -0.6524E-11 -0.1082E-10
0-1400F 04
                                  0.6795E-03 0.1847E-02 -0.2116E-04 -0.4976E-03 -0.3316E-C9 -0.8718E-10 -0.4118E-12 -0.9179E-11
           0.2618F 01 0.2538E 02
0.1400F 04
           0.3142F 01 0.1728E 02 0.3658F-03 0.1486E-02 0.2429E-03 -0.3222E-03 -0.2594E-C9 -0.4693E-10 0.4156E-11 -0.5608E-11
0.1400F 04
           0.3665F 01 0.1275E 02 0.1190F-03 0.1090E-02 0.3716F-03 -0.6483E-04 -0.1882E-09 -0.1404E-10 0.6341E-11 -0.8276E-12
0.1400F 04
           0.4189F 01 0.1077E C7 -0.3822E-04 0.7165E-03 0.3439E-03 0.1987E-03 -0.1272E-C9 0.8077E-11 0.5734E-11 0.3970E-11
0.1400F 04
           0.4712F 01 0.1028F 02 -0.1122F-03 0.4042F-03 0.1806E-03 0.3923E-03 -0.8009E-10 0.1894E-10 0.2639E-11 0.7438E-11
0.1400F 04
           0.5236F 01 0.1052F 02 -0.1223E-03 0.1695E-03 -0.6177E-04 0.4609E-03 -0.4662E-10 0.2001E-10 -0.1922E-11 0.8527E-11
           0.5759F 01 0.1107F 02 -0.8949F-04 0.1580E-04 -0.3076E-03 0.3850E-03 -0.2485E-10 0.1362E-10 -C.6508E-11 0.6854E-11
           0.1047E 01 0.5439F 02 0.6571E-03 0.1788F-02 -0.8375E-03 -0.1538E-03 -0.2890E-C9 -0.9677E-10 -0.1445E-10 -0.6981E-11
                                 0.8662E-03 0.1969E-02 -0.6305E-03 -0.3515E-03 -0.3448E-09 -0.1191E-09 -0.9861E-11 -0.8319E-11
           0.1571F 01 0.4483E 02
                                  0.7939E-03 0.1924F-02 -0.3606F-03 -0.4525E-03 -0.3421E-C9 -0.1062E-09 -0.5218E-11 -0.8390E-11
                      0.3360E 02
           0.2094F 01
0.1600F 04
                                  0.5893E-03 0.1732E-02 -0.8426E-04 -0.4261E-03 -0.3049E-C9 -0.7847E-10 -0.1000E-11 -0.7182E-11
           0.2618F 01
                       0.2362E 02
                                              0.1446E-02 0.1392E-03 -0.3114E-03 -0.2509E-C9 -0.4758E-10 0.2267E-11 -0.4768E-11
                       0.1626F 02
           0.3142E 01
                                  0.3557E-03
                                              0.1119F-02 0.2631E-03 -0.1163E-03 -0.1935E-09 -0.2059E-10 0.4024E-11 -0.1515E-11
0.1600F 04
           0.3665F 01
                      0.1164F 02
                                  0.1561E-03
                                              0.8015E-03 0.2665E-03 0.9272E-04 -0.1415E-C9 -0.1161E-11 0.3925E-11 0.1855E-11
           0.4189F 01
                      0.9171E C1 0.1809E-04
0.1600F 04
           0.4712E 01 0.8110E 01 -0.5649F-04 0.5265E-03 0.1607E-03 0.2561E-03 -0.9931E-10 0.9711E-11 0.2C79E-11 0.4436E-11
           0.5236F 01 0.7842E 01 -0.7890E-04 0.3116F-03 -0.1414E-04 0.3285E-03 -0.6769E-10 0.1278E-10 -0.8858E-12 0.5467E-11
0.1600F 04
0.1600F 04 0.5759F 01 0.7968F 01 -0.6448F-04 0.1621E-03 -0.2010E-03 0.2907E-03 -0.4576E-10 0.9716E-11 -0.4004E-11 0.4611E-11
```

TABLE II. - Continued. EARTH-PLANET ORBITER TRAJECTORIES

(f) Earth-Uranus orbiter trajectories

TIME	PSI	J	AX(O)	AY (O)	AX(T)	AY(T)	AXDOT(O)	AYDOT(O)	A XDOT (T)	AYDOT(T)
0.4000F 03 0.4000F 03 0.4000F 03 0.4000F 03 0.4000F 03 0.4000F 03 0.4000F 03 0.4000F 03	0.5236F 00 0.1047F 01 0.1571F 01 0.2094F 01 0.2618F 01 0.3142F 01 0.3665F 01 0.4189F 01 0.4712F 01 0.5236F 01 0.5759F 01	0.2051E 04 0.2222F 04	0.1174E-01 0.4202F-02 -0.3498E-02 -0.9465E-02 -0.1237E-01 -0.1242E-01 0.4951F-02 0.8744E-02 0.1374E-01	0.1107E-01 0.1303E-01 0.1115E-01 0.5961E-02 -0.7449E-03 -0.6131F-02 -0.1359E-01 -0.1414E-01 -0.1250E-01	-0.7711E-02 -0.6450E-03 0.6618E-02 0.1213E-01 0.1441E-01 0.1286E-01 0.8694E-02 0.1290E-02 -0.6210E-02	-0.1050E-01 -0.1294E-01 -0.1155E-01 -0.6805E-02 -0.4418E-04 0.6943E-02 0.1376E-01 0.1633E-01 0.1479E-01	0.1722E-C8	-0.8292E-09 -0.5363E-09 -0.1998E-10 C.7144E-09 0.1549E-C8 0.2120E-C8 -0.1904E-08 -0.1572E-08 -0.1219E-C8	-0.4596E-09 -0.4784E-10 0.3724E-09 0.6891E-09 0.8197E-09 0.7310E-09 0.4879E-09 0.4584E-10	-0.5751E-09 -0.7154E-09 -0.6362E-09 -0.3664E-09 0.1347E-10 0.4040E-09 0.8669E-09 0.1012E-08 0.9120E-09
0.8000F 03 0.8000F 03 0.8000F 03 0.8000F 03 0.8000F 03 0.8000F 03 0.8000F 03 0.8000F 03	0.5236F 00 0.1047F 01 0.1571F 01 0.2094F 01 0.2618F 01 0.3142F 01 0.4665F 01 0.4189F 01 0.4712F 01 0.5236F 01 0.5759F 01	0.2278F 03 0.2454F 03 0.2596E 03 0.2689E 03 0.2756F 03	0.6640E-02 0.5232E-02 0.3226E-02	0.3409F-02 0.4342F-02 0.4612F-02 0.4619F-02 0.2671F-02 0.9576F-03 -0.6278F-03 -0.1790F-02 -0.2513F-02 -0.2874F-02	-0.3672E-02 -0.2479E-02 -0.7236E-03 0.1131E-02 0.2596E-02 0.3048E-02 0.1936E-02 0.2643E-03 -0.1515E-02	-0.7C66E-03 -0.2244E-02 -0.3002E-02 -0.2812E-02 -0.1757E-02 -0.1501E-03 0.1562E-02 0.2907E-02 0.3189E-02	-0.1364E-C8 -0.1234E-C8 -0.98C2E-C9 -0.6467E-09 -0.2923E-C9 0.1449E-10 0.22C9E-C9 0.3252E-C9 0.3615E-C9	-0.6297E-09 -0.4671E-09 -0.2880E-09 -0.9708E-10 0.9129E-10 0.2496E-09 0.3453E-09 0.3659E-09 0.3235E-09 0.2339E-09	-0.1163E-09 -0.7922E-10 -0.2667E-10 0.2792E-10 0.7074E-10 0.9125E-10 0.8474E-10 0.5338E-10 0.5866E-11 -0.4493E-10	-0.1493E-10 -0.6020E-10 -0.8229E-10 -0.7697E-10 -0.4717E-10 -0.2013E-11 0.4592E-10 0.8349E-10 0.9998E-10 0.9020E-10
0.1000F 04 0.1000F 04 0.1000F 04 0.1000F 04 0.1000F 04 0.1000F 04 0.1000F 04 0.1000F 04	0.5236F 00 0.1047F 01 0.1571F 01 0.2094F 01 0.2618F 01 0.3665F 01 0.4189F 01 0.4712F 01 0.5236F 01 0.5236F 01	0.2855E C3 0.2177E 03 0.1613F 03 0.1254F 03 0.1105F 03 0.1107E 03 0.1177E 03 0.1256E 03 0.1320F 03	3 0.4717E-02 3 0.3959F-02 3 0.2712F-02 0.1313F-02	0.3232F-02 0.3668E-02 0.3734E-02 0.3283E-02 0.2367F-02 0.1212F-02 0.1081E-03 -0.7502F-03 -0.1318E-02 -0.1622E-02	-0.2569E-02 -0.1802E-02 -0.6698E-03 0.5380E-03 0.1512E-02 0.2005E-02 0.1898E©02 0.1233F-03 -0.9302E-03	-0.3428E-03 -0.1362E-02 -0.1890E-02 -0.1813E-02 -0.1176E-02 -0.1714E-03 0.9188E-03 0.1792E-02 0.2203E-02 0.2031E-02	-0.1CC9E-C8 -0.9620E-C9 -0.9620E-C9 -0.5958E-C9 -0.3554E-C9 -0.1365E-C9 -0.1255E-C9 -0.1748E-C9 -0.1922E-C9	-0.5168E-09 -0.4015E-09 -0.2682E-09 -0.1289E-09 0.3110E-11 0.1105E-09 0.1769E-09 0.1760E-09 0.1760E-09	-0.6740E-10 -0.4744E-10 -0.1974E-10 0.9098E-11 0.3213E-10 0.4392E-10 0.4189E-10	-0.5853E-11 -0.2985E-10 -0.4205E-10 -0.4205E-10 -0.4023E-10 -0.2572E-10 -0.2592E-11 0.2158E-10 0.4121E-10 0.5034E-10 0.4612E-10
0.1200F 04 0.1200F 04 0.1200F 04 0.1200F 04 0.1200F 04 0.1200F 04 0.1200F 04 0.1200F 04 0.1200F 04	0.5236F 00 0.1047F 01 0.1571F 01 0.2094F 01 0.2618F 01 0.3142F 01 0.3665F 01 0.4189E 01 0.5236F 01	0.2011E 03 0.1558E 03 0.1142F 03 0.8442E 02 0.6857F 02 0.6570F 02 0.6570F 02 0.7380F 02 0.7737F 02	3 0.3353E-02 0.3040E-02 0.2257E-02 0.1295F-02	0.3025E-02 0.3254E-02 0.3254E-02 0.2871E-02 0.2190E-02 0.1337F-02 0.5021E-03 -0.1758E-03 -0.6479E-03	-0.1955E-02 -0.1410E-02 -0.6136F-03 0.2429E-03 0.9461E-03 0.1323F-02 0.1285E-02 0.8551E-03 -0.6152E-03	-0.2001E-03 -0.9227E-03 -0.1313E-03 -0.1287E-03 -0.8679E-03 -0.1838E-03 -0.1189E-03 -0.1495E-03 -0.1495E-03	3 -0.7625E-C9 -0.7725E-09 2 -0.6865E-C9 2 -0.5399E-C9 3 -0.3669E-09 3 -0.2013E-C9 3 -0.6917E-10 0.2023E-10 0.7242E-10 0.9789E-10	-C.4077E-C9 -O.3393E-O9 -O.2431E-C9 -C.1383E-O9 -O.3882E-10 0.4230E-10 0.9457E-10 0.1145E-C9 0.1061E-00	-0.4411E-10 -0.3167E-10 -0.1501E-10 0.2291E-11 0.1632E-10 0.2392E-10	-0.3681E-11 -0.1769E-10 -0.2502E-10 -0.2433E-10 -0.1623E-10 -0.3198E-11 0.1113E-10 0.2281E-10 0.2856E-10 0.2661E-10

```
0.1400F 04 0.5236F 00 0.1496E 03 0.2303E-02 0.2744E-02 -0.1570E-02 -0.1528E-03 -0.5756E-09 -0.3048E-09 -0.3119E-10 -0.3515E-11
           0.1047F 01 0.1193F 03 0.2331F-02 0.2925F-02 -0.1156F-02 -0.6840F-03 -0.6298F-C9 -0.2805F-C9 +0.2263F-10 -0.1208F-10
                      0.8823F 02
                                 0.1865E-02 0.2890E-02 -0.5599E-03 -0.9818E-03 -0.5878E-09 -0.2152E-C9 -0.1166E-10 -0.1667E-10
           0.1571F 01
           0.2094F 01 0.6386F 02 0.1191E-02 0.2593E-02 0.8376E-04 -0.9783E-03 -0.4874E-09 -0.1360E-09 -0.3406E-12 -0.1631E-10
           0.2618F 01 0.4890F 02 0.5221E-03 0.2059E-02 0.6211E-03 -0.6851E-03 -0.3587E-C9 -0.5836E-10 0.8950E-11 -0.1131E-10
           0.3142F C1 0.4238E 02 0.1764E-05 0.1392E-02 0.9234E-03 -0.1905E-03 -0.2292E-C9 0.6309E-11 0.1423E-10 -0.3117E-11
           0.3665E 01  0.4140E 02 -0.3105E-03  0.7262E-03  0.9229E-03  0.3655E-03 -0.1199E-09  0.4990E-10  0.1445E-10  0.6024E-11
           0.4189F 01 0.4306E 02 -0.4307F-03 0.1669E-03 0.6307E-03 0.8287E-03 -0.4035E-10 0.6967E-10 0.9810E-11 0.1363E-10
C. 1400F 04
           0.4712F 01
                      0.4548F 02 -0.4117E-03 -0.2396E-03 0.1342F-03 0.1070E-02 0.1077E-10 0.6806E-10 0.1712E-11 0.1758E-10
          0.52365 01
                      0.4789F 02 -0.3070E-03 -0.4892E-03 -0.4265E-03 0.1019E-02 0.3962E-10 0.5001E-10 -0.7536E-11
0.1400F 04 0.5759F 01 0.5022E 02 -0.1584E-03 -0.5892E-03 -0.8967E-03 0.6839E-03 0.5228E-10 0.2099E-10 -0.1536E-10 0.1101E-10
                                 0.1448E-02 0.2376F-02 -0.1306E-02 -0.1506E-03 -0.4234E-C9 -0.2C79E-C9 -0.2317E-10 -0.3931E-11
           0.5236F 00 0.1148E 03
           0.1047F 01
                      0.9508F 02
                                 0.1760F-02 0.2626F-02 -0.9749E-03 -0.5469E-03 -0.5167E-09 -0.2259E-09 -0.1688E-10 -0.9208E-11
           0.1571F 01 0.7185F 02
                                 0.1600F 04
                                 0.1059E-02 0.2378E-02 -0.5769E-05 -0.7835E-03 -0.4401E-09 -0.1279E-09 -0.1324E-11 -0.1181E-10
0.1600F 04
           0.2094E 01 0.5196E 02
           0.2618F C1 0.3845F 02
                                 0.5507E-03 0.1948E-02 0.4217E-03 -0.5678E-03 -0.3428E-C9 -0.6637E-10 0.5199E-11 -0.8453E-11
0-1600F 04
           0.31425 01
                      0.3135E 02
                                 0.1311E-03 0.14C7E-02 0.6728E-03 -0.1937E-03 -0.2394E-09 -0.1340E-10 0.9057E-11 -0.2927E-11
0.1600F 04
                      0.2893F 02 -0.1410E-03 0.8570E-03 0.6930E-03 0.2339E-03 -0.1477E-C9 0.2395E-10 0.9519E-11 0.3309E-11
0.1600F 04
           0.3665F 01
0.1600F 04
           0.4189F 01
                     0.2911F 02 -0.2660F-03 0.3817F-03 0.4873E-03 0.5970E-03 -0.7711E-10 0.4308E-10 0.6659E-11 0.8593E-11
0.1600F 04
           0.4712F 01 0.3037F 02 -0.2777E-03 0.2365F-04 0.1196E-03 0.7949E-03 -0.2863E-10 0.4543E-10 0.1383E-11 0.1147E-10
           0.5236F 01 0.3191E 02 -0.2155E-03 -0.2083E-03 -0.3047E-03 0.7715E-03 0.1267E-11 0.3467E-10 -0.4780E-11 0.1111E-10
0.1600F 04
           0.5759F 01 0.3350F 02 -0.1134E-03 -0.3184F-03 -0.6667E-03 0.5289E-03 0.1685E-10 0.1513E-10 -0.1008E-10 0.7503E-11
          0.1C47E 01 0.6452E C2
                                 0.8915E-03 0.2033E-02 -0.7280E-03 -0.4156E-03 -0.3437E-09 -0.1288E-C9 -0.1012E-10 -0.6609E-11
           0.1571F 01
                      0.5188F 02
                                 0.9872E-03 0.2157E-02 -0.4207E-03 -0.5537E-03 -0.3838E-09 -0.1337E-09 -0.5872E-11 -0.7600E-11
           0.2094F 01
                      0.3871F C2
                                 0.7913E-03 0.2035E-02 -0.8489E-04 -0.5614E-03 -0.3607E-09 -0.1052E-09 -0.1585E-11 -0.7237E-11
           0.2618F 01
                      0.2826F 02
                                 0.4981F-03
                                            0.1752E-02 0.2081E-03 -0.4301E-03 -0.3050E-C9 -0.6670E-10 0.2026E-11 -0.5409E-11
                      0.2151F C2
                                 0.2206F-03
                                             0.1374F-02 0.3932E-03 -0.1935E-03 -0.2367E-09 -0.2999E-10 0.4297E-11 -0.2476E-11
           0.3142F 01
                                             0.9743F-03 0.4319E-03 0.8477E-04 -0.1704E-C9 -0.1681E-11
                                                                                                     0.4822E-11 0.8735E-12
           0.3665F 01
                      0.1799F 02
                                 0.1685E-04
                                             0.6118E-03 0.3227E-03 0.3297E-03 -0.1148E-C9 0.1537E-10 0.3591E-11 0.3801E-11
           0.4189F 01
                      0.1667E 02 -0.9790E-04
           0.4712F 01 0.1656E 02 -0.1355E-03 0.3223E-03 0.1027E-03 0.4749E-03 -0.7274E-10 0.2133E-10 0.1024E-11 0.5541E-11
0.2000F 04 0.5236F 01 0.1701F 02 -0.1179E-03 0.1187E-03 -0.1628E-03 0.4807E-03 -0.4380E-10 0.1819E-10 -0.2113E-11 0.5612E-11
0.2000F 04 0.5759F 01 0.1767F 02 -0.6730E-04 0.1185E-05 -0.3973E-03 0.3444E-03 -0.2588E-10 0.8757E-11 -0.4904E-11 0.3967E-11
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TABLE II. - Continued. EARTH-PLANET ORBITER TRAJECTORIES

(g) Earth-Neptune orbiter trajectories

TIME	PSI	j	AX(O)	AY (O)	AX(T)	AY(T)	AXDOT(0)	AYDOT(O)	(T) TOOKA	(T)TDDYA
										0 (0705 00
0.4000F 03 0.4000F 03	0.5236F 00 0.1047F 01	0.5607F 04 0.5132F 04	0.2444E-01 0.1592E-01				-0.4423E-C8			
0.4000F 03	0.1571F 01	0.4946E 04	0.4282E-02				-0.2028E-C8			
0.4000F 03	0.2094F 01		-0.7526F-02				-0.2977E-C9			
0.4000F 03	0.2618E 01						0.1464E-C8			-0.5889E-09
0.4000F 03	0.3142F 01	0.5655E C4	-0.2057F-01	-0.1469F-02	0.2270E-01	0.9730E-04	0.2842E-C8	0.2583E-C8	0.1299E-08	0.2287E-10
0.4000F 03	0.3665F 01	0.7203F 04	-0.3625E-02	-0.2028F-01	0.2073F-01	0.1202E-01	-0.1372E-C8	-0.1762E-C8	0.1196E-08	0.7540E-09
0.4000F 03	0.4189F 01	0.7553E C4					-0.1664E-C8		C.7076E-09	0.1280E-08
0.4000F 03	0.4712F 01	0.7684E 04					-0.2429E-C8		0.3794E-10	0.1480E-08
0.4000F 03	0.5236F 01	0.7476E 04					-0.3522E-C8			0.1313E-08
0.4000F 03	0.5759F 01	0.6956E 04	0.2513E-01	-0.1247E-01	-0.1894E-01	0.1365E-01	-0.44C4E-C8	-0.8975E-09	-0.1120E-08	0.8354E-09
0.8000F 03	0.52365 00	0.8835E 03	0.8901E-02	0 41105-03	-0 53145-03	_0 17765-02	-0.1770E-C8	-0 4000E-CO	-0 16165-00	-0 63635-10
0.8000F 03	0.1047F 01	0.7273E 03					-0.1770E-C8			
0.8000F 03	0.1571F 01	0.6208F 03					-0.1172E-C8			
0.8000F 03	0.2094F 01	0.5766F 03					-0.6904E-C9			
0.8000F 03	0.2618F 01		-0.2296E-02				-0.1834E-C9			-0.7228E-10
0.8000F 03	0.3142F 01	0.6200F 03	-0.3764E-02	0.6265E-03	0.5394E-02	-0.4888E-04	0.2439E-C9	0.5024E-09	0.1514E-09	0.1590E-11
0.8000F 03	0.3665F 01	0.6542E 03	-0.4091E-02	-0.1775E-02	0.4832E-02	0.2659E-02	0.4999E-C9	0.6461E-09	0.1357E-09	0.7740E-10
0.8000F 03	0.4189E 01	0.6754F 03	-0.3715E-02	-0.3388E-02	0.2940E-02	0.4717E-02	0.5952E-C9	0.6619E-09	0.8206E-10	0.1349E-09
0.8000F 03	0.5236F C1	0.1286E 04					-0.1330E-C8			
0.8000F 03	0.5759F C1	0.1203F 04	0.9394F-02	0.5433F-04	-0.5019E-02	0.4059E-02	-0.1639E-C8	-0.1085E-08	-0.1566E-09	0.1294E-09
	2 500/5 00			0 0/005 00	0 05075 00	0 10105 00		0 / 0505 00	0 00115 10	0 10005 10
0.1000F 04	0.5236F 00	0.5248E 03					-0.1334E-(8			
0.1000F 04 0.1000F 04	0.1047F 01 0.1571F 01	0.4201E 03 0.3411F 03					-0.1216E-C8			
0.1000F 04	0.2094F 01	0.2985F 03					-0.9759E-09			
0.1000F 04	0.2618F 01		-0.8335F-03				-0.3094E-09			-0.3768E-10
0.1000F C4	0.31425 01						-0.6322E-11			-0.3704E-12
0.1000F 04	0.3665F 01						0.1988E-C9			
0.1000F 04	0.4189F 01						0.3015E-C9			
0.1000F 04	0.57595 01	0.7121F 03	0.6233F-02	0.1920E-02	-0.3408E-02	0.2796E-02	-0.1084E-C8	-0.8622E-C9	-0.8851E-10	0.7212E-10
0.1270F 04	0.5236F 00	0.3523F 03					-0.1042E-C8			
0.120CF 04	0.1047F 01	0.2790E 03					-0.9906E-09			
0.12005 04	0.1571F 01	0.2188E C3					-0.8329E-C9			
0.1200F 04	0.2094F 01	0.1815F 03					-0.6062E-C9			
0.1200F 04	0.2618F 01 0.3142F 01		-0.1465E-03				-0.3540E-C9			-0.2257E-10
0.1200F 04	0.3147F 01 0.3665F 01						-0.1243E-09			-0.1202E-11 0.2116E-10
0.1200F 04	0.4189F 01		-0.1346F-02				0.4423E-10			
0.1200F 04	0.4712F 01						0.1430E-09		0.2558E-10	
0.1200F 04	0.5236F 01						0.1032E-03		-0.2162E-10	
0.1200F 04	0.5759F C1						-0.6393E-C9			

```
0.1600F 04 0.5236F 00 0.1937E 03 0.2740E-02 0.2968E-02 -0.1675E-02 -0.3527E-03 -0.6576E-C9 -0.3463E-09 -0.2776E-10 -0.5071E-11
           0.1047E 01 0.1558F 03 0.2604E-02 0.3186E-02 -0.1158E-02 -0.9431E-03 -0.6946E-09 -0.2990E-09 -0.1927E-10 -0.1351E-10
                                  0.1966F-02 0.3147E-02 -0.4398E-03 -0.1236E-02 -0.6326E-C9 -0.2166E-09 -0.8255E-11 -0.1763E-10
                      0.1193F 03
           0.2094E 01 0.9272E 02
                                 0.1140E-02 0.2787E-02 0.3104E-03 -0.1163E-02 -0.5105E-09 -0.1238E-09 0.2972E-11 -0.1650E-10
                                                        0.9071E-03 -0.7525E-03 -0.3607E-09 -0.3544E-10 0.1183E-10 -0.1060E-10
           0.2618F 01
                      0.7699E 02 0.3615E-03
                                             0.2141E-02
                                                        0.1294E-02 -0.1235E-03 -0.2138E-C9 0.3594E-10 0.1631E-10 -0.1671E-11
           0.3142F C1 0.7175E 02 -0.2096E-03
                                             0.1344E-02
           0.3665F 01 0.7251E 02 -0.5174E-03 0.5683E-03
                                                         0.1133E-02 0.5492E-03 -0.9372E-10 0.8103E-10 0.1551E-10 0.7845E-11
                                                                                            C.9701E-10 0.9824E-11
           0.4189E 01 0.7564E 02 -0.5974E-03 -0.5894E-04 0.7235E-03 0.1082E-02 -0.1041E-10
0.1600F 04
           0.4712F 01 0.7908E 02 -0.5239E-03 -0.4910E-03 0.9059E-04 0.1328E-02 0.3974E-10 0.8763E-10 0.9009E-12
           0.5236F 01 0.8226E 02 -0.3632E-03 -0.7318E-03 -0.5912E-03 0.1216E-02 0.6536E-10
                                                                                            0.5942E-10 -0.8795E-11
           0.5759F 01 0.8534E 02 -0.1640E-03 -0.7929E-03 -0.1137E-02 0.7687E-03 0.7396E-10 0.1917E-10 -0.1662E-10 0.1071E-10
0.2000F 04 0.5236F 00 0.1210F 03 0.1264E-02 0.2306F-02 -0.1202E-02 -0.2894E-03 -0.3923E-09 -0.1868E-09 -0.1645E-10 -0.4344E-11
           0.1047F 01 0.1025E 03 0.1655E-02 0.2633E-02 -0.8478E-03 -0.6408E-03 -0.5017E-09 -0.2149E-09 -0.1153E-10 -0.7995E-11
                                 0.1427E-02 0.2630E-02 -0.3755E-03 -0.8268E-03 -0.4957E-09 -0.1766E-09 -0.5568E-11 -0.9887E-11
           0.1571E 01 0.7982E 02
           0.2094F 01 0.6037E 02
                                 0.9615E-03 0.2381E-02 0.1189E-03 -0.7871E-03 -0.4303E-C9 -0.1179E-09 0.4502E-12 -0.9263E-11
                                 0.4644E-03 0.1932F-02 0.5197E-03 -0.5323E-03 -0.3351E-09 -0.5718E-10 0.5272E-11 -0.6243E-11
           0.2618F 01 0.4732F 02
0.700nF 04 0.3142F 01 0.4064E 02 0.6301E-04 0.1374E-02 0.7321E-03 -0.1333E-03 -0.2338E-C9 -0.5693E-11 0.7869E-11 -0.1634E-11
0.2000F 04 0.3665E 01 0.3855E 02 -0.1864E-03 0.8145E-03
                                                         0.7100E-03 0.3006E-03 -0.1442E-C9 0.2949E-10 0.7748E-11 0.3341E-11
                                                         0.4675E-03 0.6518E-03 -0.7570E-10 0.4596E-10 0.5075E-11 0.7364E-11
          0.4189F 01 0.3895F C2 -0.2883E-03 0.3401E-03
           0.4712F 01 0.4034E 02 -0.2799E-03 -0.7649E-05 0.7576E-04 0.8244E-03 -0.2915E-10 0.4553E-10 0.6542E-12 0.9349E-11
          0.5236F 01 0.4198F 02 -0.2028E-03 -0.2221E-03 -0.3556E-03 0.7699E-03 -0.9505E-12 0.3226E-10 -0.4267E-11 0.8725E-11
          0.5759E 01 0.4365E 02 -0.9186E-04 -0.3098E-03 -0.7075E-03 0.4989E-03 0.1319E-10 0.1093E-10 -0.8317E-11 0.5586E-11
                                 0.9526E-03 0.2116E-02 -0.6535E-03 -0.5022E-03 -0.3588E-09 -0.1388E-09 -0.7453E-11 -0.5766E-11
0.2400F 04 0.1047F C1 0.7278E 02
0.2400F 04
           0.1571F 01 0.5901F 02
                                  0.1006E-02 0.2231E-02 -0.3182E-03 -0.6173E-03 -0.3944E-09 -0.1375E-09 -0.3848E-11 -0.6514E-11
           0.2094F 01 0.4512F 02
                                  0.7654F-03 0.2082E-02 0.3397E-04 -0.5886E-03 -0.3651E-C9 -0.1035E-C9 -0.2306E-12 -0.6019E-11
                                  0.4435F-03 0.1761E-02 0.3247E-03 -0.4135E-03 -0.3038E-09 -0.6133E-10 0.2708E-11 -0.4205E-11
           0.2618F 01 0.3450F 02
                                                        0.4873E-03 -0.1364E-03 -0.2314E-C9 -0.2274E-10 0.4371E-11 -0.1474E-11
          0.3142E 01 0.2800E 02 0.1554E-03
                                             0.1346E-02
                                             0.9159E-03 0.4874E-03 0.1692E-03 -0.1627E-C9 0.5686E-11 0.4453E-11 0.1494E-11
           0.3665F 01 0.2491F 02 -0.4323E-04
                                             0.5372E-03
                                                        0.3321E-03 0.4217E-03 -0.1063E-C9 0.2134E-10 0.3028E-11 0.3943E-11
           0.4189F 01 0.2402E 02 -0.1428E-03
           0.4712E 01 0.2476F 02 -0.1613E-03 0.7456E-03 0.6860E-04 0.5533E-03 -0.6480E-10 0.2488E-10 0.5403E-12
           0.5236F 01 0.2496F 02 -0.1252F-03 0.5181E-04 -0.2280E-03 0.5281E-03 -0.3716E-10 0.1889E-10 -0.2296E-11
0.2400F 04 0.5759F 01 0.2582E 02 -0.5971E-04 -0.4695E-04 -0.4746E-03 0.3512E-03 -0.2093E-10 0.6726E-11 -0.4674E-11 0.3294E-11
```

TABLE II. - Concluded. EARTH-PLANET ORBITER TRAJECTORIES

(h) Earth-Pluto orbiter trajectories

TIME	PST	J	AX(N)	AY (0)	AX(T)	AY(T)	(D) TDOX A	(D)TBOYA	(T) TOOXA	AYDOT(T)
C.4000F 03	0.5236F 00	C.9648F 04	0.3063F-01				-0.5273E-C8			
0.4000F 03	0.10475 01	0.9045F 04	0.1952F-01				-0.4090E-C8			
0.4000F 03	0.1571F 01 0.2094F 01	0.8833E 04	0.4336F-02 -0.1102F-01	0.2779F-01 0.2376E-01			-0.2305E-C8			
0.40000 03	0.2618F 01		-0.2262F-01	0.2378E-01			0.2020E-C8			-0.7860E-09
0.40005 03	0.3142F C1		-0.2766F-01		0.2984F-01			0.3476E-C8	0.1712E-08	0.2742E-10
0.40006 03	0.3665F 01		-0.2683F-01		0.2613F-01		0.4244E-C8	0.5074E-C8	0.1499E-08	0.8461E-09
0.4000F 03	0.41895 01	0.1223E 05	-0.2996F-02	-0.2902F-01	0.1590E-01	0.2721E-01	-0.1517E-C8	-0.1735E-08	0.9050E-09	0.1638E-08
0.4000F 03	0.4712F 01	0.1241F 05		-0.3088E-01			-0.2665E-C8		0.3528E-10	0.1887E-08
0.4000F 03	0.52365 01	0.1212F 05		-0.2686F-01			-0.4136E-C8			0.1663E-08
0.4000F 03	n.5759F 01	0.1142F 05	0.3128F-01	-0.1630E-01	-0.2507E-01	0.1711E-01	-0.5259E-C8	-0.7614E-09	-0.1471E-08	0.1036E-08
		•								
0.1000F 04	0.52365 00	0.8024F 03	0.7804F-02	0.4106E-02	-0.4503E-02	-0.1586E-02	-0.1565E-C8	-0.6509E-C9	-0.1094E-09	-0.3179E-10
0.10005 04	0.10475 01	0.6676F 03	0.5905F-02	0.5446F-02	-0.2829E-02	-0.3460E-02	-0.1399E-C8	-0.4564E-09	-0.6964E-10	-0.7560E-10
0.1000F 04	0.1571F C1	0.571 OE 05					-0.1092E-08			
0.1000E 04	0.2094F 01	0.525CF C3		0.5002E-02			-0.6911E-C9			
0.10005 04	0.2618F 01		-0.1686F-02				-0.2621E-C9	0.2102E-09		-0.4910E-10
0.1000F 04	0.3142F 01 0.3665F 01		-0.2974E-02	0.8035F-03		-0.3329E-04		0.4055E-09 0.5184E-09		C.9793E-12 O.5211E-10
Ი. Ი^ᲘԲ 04 Ր. Ი^Ი୮ 04	0.41895 01		-0.3296F-02		0.4023F-02 0.2425F-02		0.3441E-09 0.4495E-09		0.5413E-10	
0.10005 04	0.4712F 01		-0.2426E-02				0.4693E-C9		0.2428E-11	0.1058E-09
0.10006 04	0.5236F 01	0.1117F 04			-0.2470E-02		-0.1011E-C8			0.1299E-09
0.10005 04	0.575)F 01	0.1062F 04			-0.4330E-02		-0.1376E-C8			
0.1000F 04	1.57595 C1	0.1062F C4	0.8001F-02	0.1112F-02	-0.4330E-02	0.3332E-02	-0.1390E-C8	-0.1003E-C8	-0.1080E-09	0.8480E-10
0.1600F 04	0.5236F 00	0.2756F 03	0.3613F-02	0.3277F-02	-0.2010F-02	-0.5453E-03	-0.8143E-C9	-0-4208E-09	-0.3217E-10	-0.7114F-11
0.1600F 04	0.1047F 01	0.2232E 03					-0.8161E-C9			
0.16905 04	0.15715 01	0.1764F 03	0.2229E-02	0.3563E-02	-0.3994E-03	-0.1648E-02	-0.7173E-C9	-0.2270E-09	-0.7628E-11	-0.2308E-10
0.1600F 04	0.20945 01	0.1444F 03		0.3118E-02			-0.5552E-C9			-0.2112E-10
0.1600F 04	0.26185 01	0.1288F 03		0.2296F-02			-0.3656E-C9	_		-0.1295E-10
0.16005 04	0.3142F (I		-0.5457F-03				-0.1855E-C9			-0.9857E-12
0.1600F 04 0.1600F 04	0.3665F 01		-0.8662E-03				3 ~0.4492E-10			0.1148E-10
0.16005 04	0.4189F 01		-0.7435F-03				0.4579E-10 0.9502E-10			
0.10006 04	71.4317 OL	0.1400F 03	, -0•14331 -03	-0.92446-03	0.70301-04	0.17762-02	. 0.99026-10	0.1270L-09	0.00002-12	0.23176-10
0.000					0 141			0.07005	0.10//5	A //F== 1:
0.20005 04	0.5236F 00	0.1707F 03					3 -0.5377E-C9			
0.2000F 04	0.1047# 01 0.1571# 01	0.1416E 03					3 -0.6C64E-C9 2 -0.5703E-C9			
0.2000F 04	C.2094F 01	0.1111F 03					2 -0.5703E-19 3 -0.4748E-09			
0.2000F 04	0.2618F 01	0.8724F 02		0.2059E-02			3 -0.4748E-09			-0.1141E-10
0.2000= 04	0.3142F 01		-0.1118F-03				-0.2247E-09			-0.1157E-11
0.20005 04	0.3665F 01		-0.3847E-03				-0.1184E-C9			
0.20005 04	0.4189F C1	0.6833F 02	-0.4642E-03	0.1030E-03			3 -0.4170E-10			
0.2000F 04	0.4712F 01		-0.4098E-03				0.6728E-11		0.4694E-12	0.1261E-10
0.2000F 04	0.5236F 01		-0.2784E-03				2 0.3324E-10		-0.6029E-11	
0.2000F 04	0.57595 01	0.7604F 02	2 -0.1143E-03	-0.5671E-03	-0.9640E-03	0.6321E-03	3 0.4394E-10	0.1247E+10	-0.1122E-10	0.7053E-11

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0.2400F 04 0.5236F 00 0.1133F 03 0.8112F-03 0.2004F-02 -0.1069F-02 -0.3462E-03 -0.3080E-09 -0.1312E-09 -0.1203E-10 -0.4243E-11
0.2400F 04 0.1047F 01 0.9917F 02 0.1421F-02 0.2507E-02 -0.7344E-04 -0.6307E-03 -0.4555E-C9 -0.1924E-C9 -0.8255E-11 -0.6521E-11
0.2400F 04 0.1571E 01 0.7920F 02 0.1271F-02 0.2532E-02 -0.3012E-03 -0.7802E-03 -0.4623E-09 -0.1638E-09 -0.3763E-11 -0.7752E-11
0.2400F 04 0.2094F 01 0.6139F 02 0.8705F-03 0.2303F-02 0.1464F-03 -0.7266E-03 -0.4083E-09 -0.1117E-09 0.7404E-12 -0.7122E-11
                      0.4907F 02 0.4271F-03 0.1881E-02 0.5032E-03 -0.4801E-03 -0.3241E-09 -0.5620E+10 0.4302E-11 -0.4706E-11
0-2400F 04
           0.2618F 01
           0.3142F 01 0.4250F 02 0.6490F-04 0.1356E-02 0.6847E-03 -0.1074E-03 -0.2321E-09 -0.8623E-11 0.6150E-11 -0.1129E-11
0.2400F 04
                     0.4019F 02 -0.1612F-03 0.8282E-03 0.6514E-03 0.2909E-03 -0.1493E-09 0.2405E-10
                                                                                                      0.5930E-11 0.2669E-11
                     C.4030F 02 -0.2533F-03 0.3808E-03 0.4191E-03 0.6078E-03 -0.8492E-1C 0.3943E-1C 0.3799E-11 0.5690E-11
0.2400F C4
           0.4189F C1
           0.4712E 01 0.4141F 02 -0.2443E-03 0.5346E-04 0.5509E-04 0.7576E-03 -0.4039E-10 0.3914E-10 0.3865E-12 0.7127E-11
           0.5236F 01 0.4282F 02 -0.1727F-03 -0.1470E-03 -0.3395F-03 0.6986E-03 -0.1286E-10 0.2704E-10 -0.3350E-11 0.6573E-11
           0.5759F 01 0.4429F 02 -0.7150F-04 -0.2273F-03 -0.6560E-03 0.4434E-03 0.1406E-11 0.7729E-11 -0.6372E-11 0.4130E-11
0.2809F 04 0.1047F 01 0.7313E 02 0.8380F-03 0.2032E-02 -0.5813E-03 -0.5154E-03 -0.3353E-C9 -0.1276E-09 -0.5620E-11 -0.4922E-11
0.2800F 04 0.1571F 01 0.6647F 02 0.9290F-03 0.2184F-02 -0.2586F-03 -0.6088E-03 -0.3783E-C9 -0.1317E-09 -0.2719E-11 -0.5411E-11
n.28nnF n4 n.2094F n1 0.4776F n2 0.7087F-03 0.2045E-02 0.7599E-04 -0.5662E-03 -0.3532E-C9 -0.1000E-C9 0.1896E+12 -0.4910E-11
0.2800F 04 0.2618F 01 0.3705E 02 0.4053E-03 0.1731E-02 0.3465F-03 -0.3850E-03 -0.2960E-09 -0.5952E-10 0.2517E-11 -0.3337E-11
0.2800F 04 0.3142F 01 0.3075F 02 0.1338F-03 0.1323F-02 0.4900E-03 -0.1101E-03 -0.2273E-09 -0.2229E-10 0.3773E-11 -0.1039E-11
0.2809F 04 0.3665F 01 0.2774F 02 -0.5138E-04 0.9017E-03 0.4757E-03 0.1861E-03 -0.1616E-C9 0.5051E-11 0.3723E-11 0.1411E-11
0.280F 04 0.4189F 01 0.2685E 02 -0.1413F-03 0.5327F-03 0.4253E-03 -0.1073E-09 0.1990E-10 0.2451E-11 0.3388E-11
0.2800F 04 0.4712F 01 0.2706F 02 -0.1538F-03 0.2512E-03 0.5176E-04 0.5437E-03 -0.673CE-10 0.2293E-10 0.3434E-12 0.4377E-11
0.2800F 04 0.5236F 01 0.2772F 02 -0.1150F-03 0.6705F-04 -0.2364E-03 0.5090E-03 -0.4055E-10 0.1674E-10 -0.2002E-11 0.4108E-11
0.2800F 04 0.5759F 01 0.2854F 02 -0.4984F-04 -0.2313F-04 -0.4705E-03 0.3291E-03 -0.2482E-10 0.4765E-11 -0.3925E-11 0.2635E-11
0.3000F 04 0.1047F 01 0.6344F 02 0.5754F-03 0.1771F-02 -0.5198E-03 -0.4811E-03 -0.2797E-C9 -0.9455E-1C -0.4671E-11 -0.4455E-11
                      0.5373E 02 0.7817F-03 0.2026F-02 -0.2387E-03 -0.5497E-03 -0.3426E-C9 -0.1164E-09 -0.2312E-11 -0.4662E-11
0.3000F 04 0.1571F 01
0.3000F 04 0.2094F 01 0.4238F 02 0.6322E-03 0.1931E-02 0.5455E-04 -0.5095E-03 -0.3291E-09 -0.9343E-10 0.7067E-13 -0.4191E-11
0.3000F 04 0.7618F 01 0.3313F 02 0.3830F-03 0.1661E-02 0.2934F-03 -0.3508E-03 -0.2825E-C9 -0.5911E-10 0.1991E-11 -0.2880E-11
0.3000F 04 0.3142F 01
                      0.2710F 02 0.1477F-03 0.1299E-02 0.4225E-03 -0.1105E-03 -0.2228E-C9 -0.2608E-10 0.3045E-11 -0.9870E-12
0.3000F 04 0.3665F 01 0.2395F 02 -0.1939E-04 0.9193E-03 0.4143E-03 0.1495E-03 -0.1640E-09 -0.1012E-11 0.3037E-11 0.1033E-11
0.300 NF 04 0.4189F 01 0.2276F 02 -0.1058F-03 0.5812F-03 0.2767E-03 0.3609E-03 -0.1141E-09 0.1338E-10 0.2028E-11 0.2674E-11
0.3000F 04 0.4712F 01 0.2266E 02 -0.1242F-03 0.3183F-03 0.5075E-04 0.4678E-03 -0.7627E-10 0.1738E-10 0.3279E-12 0.3514E-11
0.3000F 04 0.5236F 01 0.2306F 02 -0.9600E-04 0.1416E-03 -0.1996E-03 0.4415E-03 -0.5023E-10 0.1314E-10 -0.1578E-11 0.3329E-11
0.300nF 04 0.5759F 01 0.2365F 02 -0.4299E-04 0.4902F-04 -0.4045F-03 0.2882E-03 -0.3421E-10 0.3606E-11 -0.3152E-11 0.2158E-11
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C| (INTTO5, FOF. REC= 00000 FIL=

TABLE III. - EARTH-PLANET FLYBY TRAJECTORIES

(a) Earth-Mercury flyby trajectories

TIME	PSI	J	VX(T)	VY(T)	AX (0)	AY (0)	AXDOT(0)	AYDOT(0)	AXDOT(T)	AYDOT(T)
0.2500E 02 0.2500E 02 0.2500E 02 0.2500E 02 0.2500E 02 0.2500E 02 0.2500E 02 0.2500E 02 0.2500E 02 0.2500E 02	G.1571E C1 C.2C94E C1 O.2018E O1 U.3142E U1	0.3069E 0 0.4950E 0 0.7250E 0 0.1022E 0 0.1036E 0 0.1152E 0 0.9622E 0	4 -0.8021E 05 4 -0.9362E 05 14 -0.1116E 06 14 -0.1282E 06 14 -0.1290E 06 15 -0.1290E 06 15 -0.1238E 06 16 -0.1154E 06 17 -0.1154E 06 18 -0.9600E 05 19 -0.8135E 05	0.1064E 05 0.1092E 05 -0.1299E 04 -0.2050E 05 -0.6344E 05 -0.1048E 06 -0.2518E 05 -0.4028E 05 -0.4139E 05	-0.1170E 00 -0.1218E 00 -0.1207E 00 -0.1002E 00 -0.8355E-01 -0.6612E-01	-0.6697E-02 -0.9589E-03 -0.4630E-02 -0.1548E-01 -0.2786E-01 -0.3618E-01 -0.7569E-01 -0.77883E-01 -0.7298E-01	0.29C6E-07 0.3625E-07 0.4618E-07 C.5637E-07 0.64C4E-07 0.6703E-07 0.6648E-07 0.5376E-07 0.3548E-07 0.2872E-07	0.9609E-08 0.4291E-08 0.3022E-08 0.6426E-08 0.1353E-07 0.2099E-07 0.2489E-07 0.3158E-07 0.3022E-07 0.2490E-07	0.2115E-07 0.2746E-07 0.3637E-07 0.4576E-07 0.5359E-07 0.5722E-07 0.5140E-07 0.4942E-07 0.3859E-07 0.2875E-07 0.2174E-07	0.3587E-09 -0.4595E-08 -0.5391E-08 -0.1812E-08 0.8445E-08 0.2711E-07 0.4075E-07 0.4235E-07 0.3831E-07
0.5000E 02 0.5000E 02 0.5000E 02 0.5000E 02 0.5000E 02 0.5000E 02 0.5000E 02 0.5000E 02 0.5000E 02	0.3142E 01 0.3665E C1 0.4189E C1 0.4712E 01 0.5236E C1	0.2146E (0.2929E (0.4720E (0.6681E (0.88755E (0.88746E (0.88372E (0.1303E (03 -0.5376E 05 03 -0.5769E 05 03 -0.6277E 05 03 -0.6551E 05 03 -0.6551E 05 03 -0.6268E 05 03 -0.2661E 05 0.3073E 04 0.3073E 04 0.3073E 05 0.40518E 05 0.40518E 05 0.405747E 05	-0.1487E 05 -0.1943E 05 -0.2989E 05 -0.4533E 05 -0.6246E 05 -0.7580E 05 -0.7943E 05 -0.6994E 05 -0.1929E 05	-0.9788E-02 -0.1454E-01 -0.1920E-01 -0.2264E-01 -0.2430E-01 -0.2434E-01 -0.2340E-01 -0.2204E-01 -0.7640E-02	-0.8926E-02 -0.7C17E-C2 -0.7242E-C2 -0.9070E-C2 -0.1151E-01 -0.1366E-01 -0.1519E-01 -0.1614E-01 -0.2658E-C1	C.2560E-08 G.3734E-08 C.5302E-08 O.6895E-08 C.8125E-08 C.8125E-08 C.8522E-08 C.8552E-08 C.8263E-08 C.2546E-08	0.2293E-08 0.1922E-08 0.1998E-08 0.2543E-08 0.3379E-08 0.4180E-08 0.4676E-08 0.4687E-08 0.3923E-08 0.3556E-08	0.3173E-09 0.1083E-08 0.2323E-08 0.3752E-08 0.5005E-08 0.5083E-08 0.3340E-08 0.7625E-09 0.2340E-08 0.9173E-09	0.3364E-08 0.1727E-08 0.5833E-09 0.1213E-09 0.4853E-09 0.1705E-08 0.3450E-08 0.4996E-08 0.5600E-08 0.8321E-08
0.75CUE U2 0.75CUE 02 0.75CUE C2 0.75CUE C2 0.75CUE 02 0.75CUE 02 0.75CUE 02 0.75CUE C2 0.75CUE C2 0.75CUE 02	0.3142E C1 C.3605E C1 0.4189E C1 0.4712E 01 0.5236E 01	0.8855E 0.5153E 0.5965E 0.9230E 0.1281E 0.1534E 0.1647E 0.1653E 0.1618E	03 -0.4695E 05 02 -0.4624E 05 02 -0.4538E 05 02 -0.4198E 05 02 -0.3368E 05 03 -6.1915E 05 03 0.9043E 03 04.2328E 05 03 0.4301E 05 03 0.5517E 05	-0.2721E US -0.3308E 05 -0.4177E 05 -0.6076E 05 -0.6076E 05 -0.6440E 05 -0.54560E 05 -0.2461E 05	0.2286E-03 -0.2126E-C2 -0.4451E-02 -0.6287E-02 -0.7373E-02 -0.7703E-02 -0.7446E-02 -0.6813E-02 -0.5968E-02	-0.5607E-02 -0.4564E-02 -0.4411E-02 -0.4958E-02 -0.5852E-02 -0.7438E-02 -0.7438E-02 -0.7865E-02	0.3127E-09 0.5276E-09 0.1556E-08 0.2C76E-08 0.2C76E-08 0.2407E-08 0.2541E-08 0.2525E-08 0.2423E-08 0.2286E-08	0.3652E-09 0.4998E-09 0.7345E-09 0.1017E-08 0.1268E-08 0.1421E-08 0.1453E-08 0.1377E-08 0.1209E-08	-0.7595E-09 -0.5795E-09 -0.1928E-09 0.2930E-09 0.7399E-09 0.9953E-09 0.9462E-09 0.5888E-09 0.4439E-10 -0.4433E-09	0.1804E-08 0.1106E-08 0.5740E-09 0.2853E-09 0.2787E-09 0.5234E-09 0.1186E-08 0.1232E-08 0.9420E-09 0.3236E-08
0.1000E 03 0.1000E 03 0.1000E 03 0.1000E 03 0.1000E 03 0.1000E 03 0.1000E 03 0.1000E 03 0.1000E 03	0.3142E C1 0.3665E C1 G.4189E C1 0.4712E C1	0.4329E 0.4329E 0.2191E 0.1910E 0.2582E 0.3467E 0.4172E C.4635E 0.5029E	03 - C. 4333 E	-0.3539E 05 -0.4131E 05 -0.4821E 05 -0.5474E 05 -0.5677E 05 -0.4761E 05 -0.3110E 05 -0.9881E 04	0.3119E-02 0.1580E-02 0.4693E-04 -0.1232E-02 -0.2101E-02 -0.257E-02 -0.257E-02 -0.2352E-02 -0.1953E-02	-0.3131E-02 2-0.2495E-C2 -0.2342E-C2 2-0.2577E-C2 2-0.3031E-02 2-0.3913E-02 -0.4152E-C2 2-0.4218E-02	-0.4708E-09 -0.1223E-09 0.2385E-09 0.5548E-09 0.7865E-09 0.5719E-09 0.5719E-09 0.9253E-09	-0.2354E-09 -0.1009E-09 0.5991E-10 0.2252E-09 0.3645E-09 0.4527E-09 0.4789E-09 0.460E-09 0.3612E-09	-0.7147E-09 -0.5484E-09 -0.3138E-09 -0.7929E-10 0.8623E-10 0.1361E-09 0.6992E-10 -0.6336E-10 -0.1839E-09	0.1156E-08 0.7448E-09 0.4098E-09 0.1926E-09 0.1098E-09 0.1431E-09 0.2355E-09 0.3089E-09 0.2958E-09 0.1636E-09 0.1951E-08

```
0.1250E U3 0.5236E C0 0.1527E 03 -U.4022E U5 -0.3603E 05 0.4940E-02 -0.2050E-C2 -C.87CCE-09 -0.5832E-09 -0.6617E-09 0.8077E-09
U-1250E U3 0-1047E G1 0-9563E U2 -0-3403E 05 -U-4141E 05 0-3970E-02 -0-1425E-02 -G-6798E-09 -0-4680E-09 -0-6575E-09 0-5209E-09
0.1250E 03 0.1571E 01 0.5304E 02 -0.2086E 05 -0.4681E 05 0.2826E-02 -0.1044E-02 -0.4463E-09 -0.3426E-09 -0.5667E-09 0.2777E-09
0.1250E 03 0.2094E 01 0.2647E 02 -0.1754E 05 -0.5198E 05 0.1676E-02 -0.9515E-03 -0.2004E-09 -0.2113E-09 -0.4234E-09 0.1045E-09
0.1250E C3 C.3142E 01 0.9789E 01 0.1013E 05 -0.5586E 05 -0.6466E-04 -0.1406E-C2 C.2C52E-09 0.1841E-10 -0.1395E-09 -0.1171E-10
0.1250€ 03 0.4712E 01 0.1697€ 02 0.5292E 05 -0.2050€ 05 -0.7008E-03 -0.2200E-02 0.4318E-09 0.1190E-09 -0.5704E-10 0.1583E-10
0.1250c 03 0.5236E 01 0.2089E 02 0.5563E 05 0.8907c 03 -0.5646E-03 -0.2253E-02 0.4400E-09 0.8440E-10 -0.6370E-10 -0.4267E-10
C.12562 03 C.5759E 01 C.2702E 02 C.4939E 05 C.2139F 05 -U.3836E-03 -0.2177E-02 C.4478E-09 U.2545E-10 -0.1663E-10 -0.1470E-09
0.1500E 03 0.5236E 00 0.1419E 03 -0.3705E 05 -0.4074E 05 0.4834E-02 -0.6164E-02 -0.8501E-09 -0.6530E-09 -0.5739E-09 0.5902E-09
0.1500E 03 0.1047E 01 0.9634E 02 -0.2905E 05 -0.4605E 05 0.4066E-02 -0.2522E-03 -0.7139E-09 -0.5436E-09 -0.5780E-09 0.3714E-09
C.1500E 03 0.2094E 01 0.3366E 02 -U.9209E 04 -0.5415E 05 0.2250E-02 -U.1524E-04 -0.3621E-09 -0.3171E-09 -0.4135E-09 0.4096E-10
0.1500E 03 0.3665E 01 0.7188E 01 0.3446E 05 -0.4501E 05 0.3358E-03 -0.676CE-C3 C.6893E-10 -0.5909E-10 -0.1081E-09 -0.8384E-10
0.1500E u3 0.4189E C1 0.7168E 01 C.4753E 05 -0.3105E 05 u.8160E-04 -0.9148E-03 0.1445E-09 -0.2092E-10 -0.6033E-10 -0.7624E-10
0.1500E 03 0.4712E C1 0.8640E U1 0.5517E 05 -0.1203E 05 -0.2202E-04 -0.1080E-02 0.1912E-09 -0.7562E-11 -0.3326E-10 -0.7782E-10
0.15CUE 03 0.5236E C1 C.1124E 02 C.5492E 05 0.9320E 04 -0.2886E-04 -0.1154E-C2 C.22C1E-09 -0.1408E-10 -0.5468E-11 -0.9810E-10
0.1500E U3 0.5759E C1 0.1550E C2 0.4598E 05 0.2906E 05 -0.6831E-05 -0.1139E-02 0.2476E-09 +0.3300E-10 0.4997E-10 -0.1343E-09
0.1750E C3 0.5236E C0 C.1303E 03 -0.3370E 05 -0.4478E 05 0.4469E-02 0.3583E-C3 -C.7864E-09 -0.6447E-09 -0.5015E-09 0.4421E-09
0.1750E 03 0.1047E C1 0.9341E 02 -0.2430E 05 -0.4968E 05 0.3855E-02 0.5539E-03 -0.6871E-09 -0.5473E-09 -0.5044E-09 0.2666E-09
U.1750E U3 C.1571E C1 C.62C3E U2 -G.1396E U5 -U.5330E U5 U.3128E-U2 U.65C2E-U3 -U.5593E-U9 -C.4470E-U9 -U.4558E-U9 U.138E-U9
0.1750E 03 0.2094E 01 0.3829E 02 -0.2131E 04 -0.5526E 05 0.2378E-02 0.6175E-03 -0.4181E-09 -0.3484E-09 -0.3731E-09 -0.2390E-11
0.175CE 03 0.2618E C1 C.2231E 02 0.1140E 05 -0.5458E 05 0.1687E-02 0.4672E-03 -0.2796E-09 -0.2572E-09 -0.2759E-09 -0.7665E-10
0.1750t 03 0.3142E C1 0.1284E 02 C.2603E 05 -0.4986t 05 0.1118E-02 0.2415E-C3 -0.1571E-09 -0.1794E-09 -0.1828E-09 -0.1121E-09
0.1750E 03 0.4189E C1 0.6253E C1 0.5117E 05 -0.2458E 05 0.4227E-03 -0.2257E-C3 0.1489E-10 -0.7922E-10 -0.5147E-10 -0.1134E-09
0.1750E 03 0.4712E 01 0.6291E 01 0.5639E 05 -0.4962E 04 0.2646E-03 -0.3983E-03 C.6656E-10 -0.5688E-10 -0.1190E-10 -0.1069E-09
0.1750E 03 0.5759E C1 0.1030E 02 0.4263E 05 0.3499E 05 0.1256E-03 -0.5377E-C3 0.1387E-09 -0.4709E-10 0.7404E-10 -0.1103E-09
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TABLE III. - Continued. EARTH-PLANET FLYBY TRAJECTORIES

(b) Earth-Venus flyby trajectories

TIME	129	J	VX(T)	VY(T)	AX(0)	AY(0)	AXDOT(0)	AYDOT(O)	AXDOT(T)	AYDOT(T)
0.5000E C2 0.5000E 02 0.5000E 02 0.5000E 02 0.5000E 02 0.5000E 02 0.5000E 02 0.5000E 02 0.5000E 02 0.5000E 02 0.5000E 02	0.2618E C1 0.3142E C1 0.3665E C1 0.4189E C1 C.4712E C1 0.5236E C1	0.6092E 02 0.3016E 03 0.7405E 03 0.1497E 04 0.1497E 04 0.1610E 04 0.2905E 04 0.2577E 04 0.1965E 04	3 -0.2807E 05 2 -0.3995E 05 3 -0.5002E 05 3 -0.7075E 05 4 -0.7316E 05 4 -0.7306E 05 4 -0.5289E 05 4 -0.7980E 05 4 -0.4413E 05 4 -0.4413E 05 4 -0.3010E 05	0.8848E U4 0.1009E 05 0.6729E 03 -0.1853E 05 -0.4389E U5 -0.6842E U5 -0.2581E 05 -0.3937E U5 -0.4042E 05	-0.6646E-02 -0.1544E-01 -0.2414E-01 -0.3050E-01 -0.3329E-01 -0.3314E-01 -0.1866E-01 -0.1194E-01 -0.4606E-02	-0.2683E-02 0.2021E-C3 -0.1179E-C2 -0.5779E-C2 -0.1129E-01 -0.1556E-C1 -0.3630E-C1 -0.37C8E-C1 -0.3405E-01	0.29C7E-09 C.23C4E-08 0.5C84E-08 0.7988E-08 C.1C28E-07 C.114CE-07 0.1147E-07 C.5796E-08 C.38C6E-08 O.1613E-08 -C.1271E-10	0.1645E-C8 0.7360E-09 0.7397E-09 0.1771E-08 0.3548E-08 0.5335E-08 0.6391E-08 0.4762E-08 0.5493E-08 0.5493E-08 0.5427E-08	0.5406E-08 0.7160E-08 0.7922E-08 0.7088E-08 0.7046E-08 0.4300E-08 0.1797E-08	
C.1CCOE G3 0.10GOE G3 0.1CCOE G3 0.10GOE G3 0.10GOE G3 0.1GGOE G3 0.1GGOE G3 0.1GGOE G3 0.1GGOE G3 0.1GGOE G3 0.1GGOE G3	0.2618E C1 0.3142E C1 G.3665E C1	C.6701E O. C.1303E C C.6072E C O.2835E O O.5897E O C.8336E O O.9652E C O.1002E C O.6164E O	3 -C.2273E U5 2 -U.2522E U5 2 -C.2899E U5 1 -0.3113E U5 2 -0.2875E 05 2 -0.1999E 05 2 -0.5154E 04 2 -0.5154E U5 3 -0.3710E U5 3 -0.3710E U5 3 -C.2870E U5	-0.1477E 05 -0.1656E 05 -0.2268E 05 -0.3193E 05 -0.4137E 05 -0.4705E 05 -0.4550E 05 -0.3542E 05 -0.2305E 05	0.3748E-02 0.1215E-02 -0.1304E-02 -0.3320E-02 -0.4553E-02 -0.5006E-02 -0.4875E-02 -0.4889E-02 0.6366E-02	-0.2161E-02 -0.1253E-C2 -0.130GE-02 -0.2092E-C2 -0.3223E-C2 -0.43C5E-C2 -0.5122E-02 -0.5632E-C2 -0.10C3E-01	-0.7318E-09 -C.17C7E-09 C.4157E-09 0.9274E-09 0.1272E-08 C.1440E-08 C.1470E-08 C.1422E-08 -0.13C2E-08	-0.2324E-09 -C.6108E-10 0.1892E-09 0.4741E-09 0.7235E-09 0.8791E-09 0.9240E-09 0.8746E-09 -0.5054E-09	-0.5299E-09 -0.2494E-09 0.7855E-10 0.3677E-09 0.5318E-09 0.5116E-09 0.3102E-09 -0.3051E-11 -0.1616E-10	0.9182E-09 0.5006E-09 0.2018E-09 0.6106E-10 0.8814E-10 0.2555E-09 0.4869E-09 0.6738E-09 0.7242E-09 0.2121E-08 0.1824E-08
0.1500E 03 0.1500E 03 0.1500E 03 0.1500E 03 0.1500E 03 0.1500E 03 0.1500E 03 0.1500E 03 0.1500E 03	C.5236E CC 0.1047E G1 C.1571E C1 0.2094E C1 0.2618E 01 G.3142E C1 0.3665E C1 0.4189E C1 C.4712E C1 C.5236E O1 G.5759E C1	0.9368E 0 0.4449E 0 0.1532E 0 0.2973E 0 0.1463E 0 0.4693E 0 0.8905E 0 0.1234E 0 0.1492E 0	0.2568E 05 0.3478E 05 0.3734E 05	-0.2559E 05 -0.2735E 05 -0.3089E 05 -0.3509E 05 -0.3782E 05 -0.3658E 05 -0.2963E 05 -0.1694E 05 -0.7167E 03	0.4538E-02 0.3167E-02 0.1782E-02 0.5927E-03 -0.2697E-03 -0.7746E-03 -0.9730E-03 -0.979E-03	-0.8997E-C4 0.2633E-C3 0.2311E-03 -0.1213E-03 -0.6481E-C3 -0.1193E-02 -0.1646E-02 -0.1959E-C2	-C.8697E-09 -C.6115E-09 -O.3337E-09 -O.7584E-10 0.1299E-09 C.27C1E-09 C.3498E-09 C.3845E-09 C.3927E-09	-0.5281E-09 -0.3825E-C9 -0.2286E-09 -0.8052E-10 0.4344E-10 0.1286E-C9 C.1701E-09 0.1450E-09	-0.4404E-09 -0.3435E-09 -0.2178E-09	0.1495E-10 0.6266E-10 0.1071E-09 0.1224E-09 0.9716E-10
0.20C0E C3 0.20C0E 03	0.1047E 01 0.1571E 01 0.2094E 01 0.2018E 01 0.3142E 01 0.3665E 01 0.4189E 01 0.4712E 01	0.9299E 0 0.2912E 0 0.2912E 0 0.1269E 0 0.4312E 0 0.1123E 0 0.6753E 0 0.1389E 0	0.1329E 05 0.2335E 05 00 0.3214E 05 01 0.3690E 05 01 0.3532E 05	-0.3198E 05 -0.3287E 05 -0.3420E 05 -0.3506E 05 -0.3383E 05 -0.2886E 05 -0.1926E 05 -0.5612E 04	0.4024E-02 0.3134E-02 0.2214E-02 0.1383E-02 0.7247E-03 0.2695E-03 0.2133E-05 -0.1186E-03 -0.11420E-03	0.1119E-02 0.1209E-02	-C.1424E-09 -C.30C8E-10 C.4899E-10 C.10C0E-09 0.1314E-09	-0.5365E-09 -0.4211E-09 -0.3066E-09 -0.2005E-09 -0.1111E-09 -0.4432E-10 -0.2109E-11 0.1799E-10 0.2119E-10	-0.3372E-09 -0.2826E-09 -0.2090E-09 -0.1327E-09 -0.6647E-10 -0.2632E-10 -0.8312E-11 -0.8658E-11	0.1518E-09 0.5332E-10 -0.1275E-10 -0.4449E-10 -0.4669E-10 -0.3022E-10 -0.8824E-11 0.5666E-11

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0.3500E U3
          0.1047E 01
          C. 1571E C1 C.4766E C2
                               C.1072E 05 -0.3711E 05
                                                    0.1787E-02
                                                                0.1975E-02 -C.4296E-09 -0.2604E-09 -0.1374E-09 -0.2402E-10
0.1805E-02 -0.3751E-09 -0.2110E-09 -0.1038E-09 -0.4787E-10
0.3500E t3 t.2618E C1 t.2191E 02 t.2459E 05 -0.2886E 05 0.1110E-02 0.1582E-02 -t.3105E-09 -0.1620E-09 -0.6912E-10 -0.5925E-10
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C.3500t U3 0.4712E C1 0.2552E C1 0.3618E 05 0.1360E 05 0.1905E-03 0.58C9E-03 -C.9C5CE-10 -0.2937E-10 0.1344E-10 -0.2694E-10
0.3500E 03 0.5236E 01 0.1402E 01 0.2840E 05 0.2618E 05 0.9782E-04 0.3936E-03 -0.5722E-10 -0.1504E-10 0.1720E-10 -0.1533E-10
C.3500E U3 0.5759E C1 C.8102E 0G C.1545E 05 0.3517E 05 0.3889E-04 0.2417E-03 -C.3104E-10 -0.5737E-11 0.1748E-10 -0.6118E-11
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(c) Earth-Mars flyby trajectories

TIME	PSI	ŋ	VX(T)	VY(T)	AX (O)	AY(C)	AXDOT(C)	AYDOT(O)	AXDOT(T)	AYDOT(T)
0.50CUE 02 0.5000E 02 0.5000E 02 0.50CUE 02	C.1C47E C1 C.1571E C1 O.2U94E C1 C.2618E C1 C.3142E C1 U.3665E C1 O.4189E C1 U.4712E C1 U.5236c C1	C.2616E 0 C.9382E 0 O.2075E 0 C.3234E C C.3969E C C.4163E 0 C.4085E 0 C.4085E 0 C.4122E 0	3	0.4999E 05 0.5913E 05 0.4689E 05 0.1552E 05 -0.2900E 05 -0.7700E 05 -0.1127E 06 -0.1241E 06 -0.8032E 05	0.2080E-02 -0.1632E-01 -0.3466E-01 -0.4807E-01 -0.5348E-01 -0.5052E-01 -0.5052E-01 -0.3774E-02	0.1311E-01 0.1840E-01 0.1420E-01 0.2375E-02 -0.1154E-01 -0.2073E-01 -0.2489E-01 -0.3452E-01 -0.5110E-01	0.1735E-07 0.1735E-07 0.1701E-07 0.466CE-08 -0.1566E-08	-C.2568E-08 -C.2917E-08 -O.9165E-09 0.3169E-C8 C.7870E-C8 C.1046E-C7 G.1087E-07 C.2260E-07 C.9031E-08	-0.1458E-09 0.4056E-08 0.8284E-08 0.1144E-07 0.1267E-07 0.1119E-07 0.6788E-08 0.1022E-07	-0.3085E-08 -0.4631E-08 -0.4760E-08 -0.1739E-08 0.1830E-08 0.6492E-08 0.1069E-07 0.7961E-08 0.1271E-07
0.1000E U3 0.1000E U3 0.1000E 03 0.1000E U3 0.1000E U3 0.1000E U3 0.1000E U3 0.1000E U3 0.1000E U3	0.1047E 01 0.1571E 01 0.2094E 01 0.2618E 01 0.3142E 01 0.3605E 01 0.4189E 01 0.4712E 01 0.5236E 01	0.6861E 0 C.1771E 0 G.7G26E 0 C.1752E 0 C.2742E 0 C.3354E 0 C.3514E 0 C.3407E 0	3 C.4190E C4 2 -G.8174E 04 2 -C.2522E 05 2 -C.4139E 05 3 -C.5096E 05 3 -C.3594E 05 3 -C.3594E 05 3 -C.3594E 05 0 C.1388E 05 0 C.3648E 05 0 C.1198E 04	0.1250E 05 0.1596E 05 0.9006E 04 -0.6907E 04 -0.2758E 05 -0.4669E 05 -0.5757E 05 -0.5602E 05 -0.4211E 05	0.5638t-02 0.7387E-03 -0.4144E-02 -0.7877E-02 -0.9826E-02 -0.1016E-01 -0.9551E-02 -0.8564E-02 -0.7481E-02	0.9678E-C3 0.245EE-C2 0.1739E-02 -0.6755E-C3 -0.3684E-C2 -0.6224E-C2 -0.7914E-C2 -0.89C3E-C2	-0.1388E-08 -C.35ECE-C9 C.7588E-09 C.1721E-08 0.2324E-08 C.2536E-08 C.2536E-08 0.2391E-08	-0.4104E-09 -0.1950E-C9 0.2586E-09 0.8669E-09 0.1439E-08 0.1785E-08 0.1768E-08 0.1768E-08	-0.5059E-09 0.3063E-10 0.5914E-09 0.1034E-08 0.1235E-08 0.1110E-08 0.6708E-09 0.3864E-10 -0.6175E-09	-0.2447E-09 -0.2798E-09 -0.6376E-10 0.3417E-09 0.8239E-09 0.1210E-08 0.1344E-08 0.1150E-08
0.1500E U3 0.1500E U3	0.1047E 01 C.1571E C1 U.2094E C1 Q.2618E C1 C.3142E C1 C.3605E C1 C.4189E C1 O.4712E C1 C.5236E C1	0.9809E 0 0.2986E 0 0.5011E 0 0.1149E 0 0.3170E 0 0.5149E 0 0.6462E 0 0.7110E 0	C.12 C4E 04 02 -0.5193E 04 12 -0.1451E 05 13 -0.2299E 05 12 -0.2691E 05 12 -0.2372E 05 12 -0.1316E 05 12 -0.1316E 05 12 -0.1328E 05 12 -0.1823E 05 12 -0.2968E 05 13 -0.4142E 04	-0.1751E 04 0.2155E 03 -0.4257E 04 -0.1392E 05 -0.2559E 05 -0.3494E 05 -0.379E 05 -0.3278E 05 -0.2033E 05	0.5530E-02 0.3098E-02 0.6600E-03 -0.1317E-02 -0.2560E-02 -0.3047E-02 -0.3047E-02 -0.2703E-02 -0.2703E-02	0.8170E-C3 0.145E-C2 0.1191E-02 0.2076E-C3 -0.1088E-02 -0.2298E-C2 -0.3211E-02 -0.3797E-C2	0.1192E-08 2-C.7449E-09 0.2549E-09 0.1897E-09 0.5165E-09 0.711E-09 0.711E-09 0.71352E-09	-0.5242E-09 -C.J298E-09 -0.9220E-10 0.1587E-C9 0.3728E-09 0.5068E-09 C.5493E-09 0.5160E-09 0.4271E-09	-0.3600E-09 -0.1898E-09 -0.3264E-11 0.1534E-09 0.2401E-09 0.3328E-09 0.1361E-09 -0.1672E-10 -0.1802E-09	-0.4731E-10 -0.1002E-10 0.9075E-10 0.2156E-09 0.3147E-09 0.3469E-09 0.2941E-09
C.2CCUE U3 0.200UE 03 C.2CCOE 03 0.200UE 03 0.200UE 03 0.2CCUE 03 C.2CCUE 03 C.2CCUE 03 0.2CUUE U3 0.2CUUE U3 0.2CUUE U3 0.2CCUE 03	0.1047E C1 0.1571E C1 0.2694E C1 0.2618E C1 0.3142E C1 0.3665E C1 0.4189E C1 0.4712E C1 0.5236E 01	C.1027E C.4746E C.1530E C.1530E C.2859E C.2897E C.1396E C.1396E C.1840E C.2150E	03	-0.9613E 04 -0.7933E 04 -0.1062E 05 -0.1658E 05 -0.2331E 05 -0.2766E 05 -0.2694E 05 -0.2019E 05 -0.8726E 04	0.4868E-02 0.3345E-02 0.1798E-02 0.4818E-03 -0.4435E-03 -0.9524E-03 5-0.1120E-02 -0.1056E-02 -0.8534E-03	0.1421E-02 0.1684E-03 0.1476E-03 0.8826E-03 0.9859E-04 0-0.6713E-03 0-0.1258E-03 0-0.1737E-03 0-0.1997E-03	2 - G.1007E-08 2 - C.75C5E-09 2 - C.4621E-09 3 - C.1877E-09 4 C.344EE-10 6 G.1665E-09 2 C.3126E-09 2 C.3124E-09 2 C.3224E-09	-0.5503E-09 -0.3909E-09 -0.2247E-09 -0.6624E-10 0.6465E-10 0.1519E-09 0.1913E-09 0.1890E-09	-0.2641E-09 -0.1823E-09 -0.8944E-10 -0.6985E-11 0.4664E-10 0.6054E-10 -0.1530E-10 -0.7419E-10	0.1544E-10 -0.2263E-10 -0.1930E-10 0.1549E-10 0.6416E-10 0.1055E-09 0.1221E-09 0.1058E-09

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0.3000E C3
        0.3665E 01    C.1408E 01    C.1136E 05    -0.4783E 05    O.1604E-03    O.5645E-C3    -0.1016E-09    -0.2232E-10    O.1554E-11    -0.7151E-11
0.3060E 03 0.4712E 01 0.1303E 01 0.2210E 05 -0.5914E 04 -0.1663E-03 -0.1823E-03 0.2585E-10 0.2832E-10 -0.3363E-11 0.1901E-10
C.3000E 03 C.5236E C1 C.2269E 01 0.2252E 05 0.3953E 04 -0.1690E-03 -0.4153E-C3 C.575CE-10 0.2822E-10 -0.1635E-10 0.2025E-10
0.3060E 03 0.5759E C1 0.3214E 01 0.1795E 05 0.1335E 05 -0.1127E-03 -0.5566E-03 0.7564E-10 0.1662E-10 -0.2918E-10 0.1171E-10
C.3500E ∪3 0.5236E CO 0.1075E 03 0.4802E 04 -0.2383E 05 0.3137E-02 0.2287E-02 -0.6516E-09 -0.4447E-09 -0.1479E-09 0.5489E-10
0.3500E 03 0.1047E 01 0.7834E 02 0.5907E 04 -0.1964E 05 0.2775E-02 -0.6197E-09 -0.3795E-09 -0.1289E-09 0.1568E-10
C.35CUE U3 0.1571E C1 C.5175E 02 C.5674E 04 -U.1705E 05 0.2272E-02 0.2175E-C2 -0.546CE-09 -0.3035E-09 -0.1009E-09 -0.1246E-10
0.3500E 03 0.2094E 01 0.3070E 02 0.5577E 04 -0.1621E 05 0.1677E-02 0.1950E-02 -0.4461E-09 -0.2251E-09 -0.6942E-10 -0.2814E-10
0.3506E 03 0.3142E 01 0.7418E 01 0.1015E 05 -0.1620E 05 0.6335E-03 0.1214E-02 -0.2330E-09 -0.8863E-10 -0.1632E-10 -0.2628E-10
0.3500E 03 0.3665E C1 0.2937E 01 0.1487E 05 -0.1410E 05 0.2889E-03 0.8074E-C3 -0.1450E-09 -0.4076E-10 -0.1894E-11 -0.1507E-10
C.3500E U3 0.4189E C1 0.1091E 01 C.1954E 05 -0.9073E 04 0.7190E-04 0.4406E-C3 -C.7687E-10 -0.9017E-11 0.3008E-11 -0.2928E-11
0.3500E C3 0.5236E C1 0.8127E 00 C.2087E 05 0.7912E 04 -0.7248E-04 -0.8198E-04 0.5121E-11 C.1244E-10 -0.7005E-11 0.9294E-11
```

(d) Earth-Jupiter flyby trajectories

TIME	PSI	J	VX(T)	VY(T)	AX (0)	AY(G)	AXDOT(C)	A YDOT (O)	AXDOT(T)	AYDOT(T)
0.2000E 03 0.2000E 03 0.2000E 03 0.2000E 03 0.2000E 03 0.2000E 03 0.2000E 03 0.2000E 03 0.2000E 03 0.2000E 03	C. 1047E C1	0.1657E C 0.1497E C 0.1955E C 0.2592E C 0.3064E C 0.3293E C 0.3365E C 0.1124E C	03	0.1867E 05 -0.1374E 05 -0.4566E 05 -0.6770E 05 -0.7317E 05 -0.7355E 05	-0.6267E-02 -0.5764E-02 -0.4938E-02 0.1065E-01	0.4720E-G2 0.5722E-G2 0.4764E-02 0.2231E-02 -0.88991E-G3 -0.3542E-G2 -0.527CE-02 -0.6254E-G2 -0.7638E-G2	-C.182GE-08 -C.1157E-08 -0.39C3E-09 G.3375E-09 C.8666E-09 C.1121E-08 0.117CE-08 C.113ZE-08 -C.2111E-08	- C.6092E-09 - O.3484E-09 0.6751E-11 0.4235E-09 0.6073E-09 0.1035E-08 0.1071E-08 C.9700E-09 - O.1274E-08	0.4057E-09 0.3612E-09 0.2103E-09 -0.3892E-11 -0.2529E-09	-0.1465E-09 -0.2419E-09 -0.2216E-09 -0.1038E-09 0.7191E-10 0.2567E-09 0.3960E-09 0.4428E-09
0.3000E C3 0.3000E 03 0.3000E 03 0.3000E 03 0.3000E 03 0.3000E 03 0.3000E 03 0.3000E 03 0.3000E 03	0.4189E C1 0.4712E C1 C.5236E C1	0.8457E (0.4703E (0.3977E (0.4972E (0.6399E (0.7559E (0.8331E (0.8888E (0.8888E)))))))))))))))))))))))	03	0.8540E 04 -0.1178E 05 -0.3130E 05 -0.4397E 05 -0.4580E 05 -0.3608E 05	0.5482E-02 0.3407E-02 0.1290E-02 -0.4479E-03 -0.1544E-02 -0.1990E-02 -0.1966E-02 -0.1673E-02 -0.1245E-02	0.3250E-C2 0.3536E-C2 0.3025E-02 0.1867E-02 0.4321E-03 -0.8821E-C3 -0.1859E-02 -0.2481E-C2 -0.2804E-C2	-C.9321E-C9 -O.5694E-O9 -C.2116E-O9 0.7795E-10 0.2641E-O9 0.3560E-O9 0.3862E-O9 C.383GE-O9	-0.5246E-09 -C.3340E-09 -0.1332E-09 0.6074E-10 0.2184E-09 0.3120E-09 0.3342E-09 0.2978E-09 0.2180E-09	-0.1395E-09 -0.6735E-10 0.6290E-11 0.6392E-10 0.9261E-10 0.8669E-10 0.4937E-10 -0.7591E-11 -0.6812E-10	-0.5879E-10 -0.6042E-10 -0.3131E-10 0.1697E-10 0.6907E-10 0.1087E-09 0.1225E-09 0.1047E-09
C.4CGGE C3 O.4CGGE C3 O.4CGGE C3 O.4CGGE C3 O.4CGGE C3 O.4CGGE C3 O.4CGGE C3 O.4CGGE C3 O.4CGGE C3 C.4CGGE C3 C.4CGGE C3	0.4189E C1 0.4712E 01	0.2024E 0.1723E 0.2034E 0.2508E 0.2944E 0.3315E	03 0.1853E 05	0.1783E 05 0.1476E 05 0.4410E 04 -0.9763E 04 -0.2314E 05 -0.3135E 05 -0.3162E 05 -0.2366E 05	0.4062E-02 0.2860E-02 0.1586E-02 0.4847E-03 -0.2870E-03 -0.6967E-03 -0.8124E-03 -0.7332E-03 -0.5400E-03	0.2972E-02 0.2985E-C2 0.2595E-C2 0.1865E-02 0.9756E-03 0.1274E-C3 -0.5500E-03 -0.1288E-02	-0.9328E-09 -C.7645E-09 -C.55CSE-09 -C.3257E-09 -C.1368E-09 -C.1368E-10 0.9423E-10 C.1418E-09 C.1617E-09	-0.4472E-09 -0.31C9E-09 -0.1748E-09 -0.5056E-10 0.4799E-10 0.1100E-09 C.1331E-09 0.1231E-09 0.8783E-10	0.2823E-10 0.2935E-10 0.1678E-10 -0.4848E-11 -0.2893E-10	-0.6181E-11 -0.2548E-10 -0.2880E-10 -0.1823E-10 0.1329E-11 0.2325E-10 0.4054E-10 0.4753E-10 0.4142E-10
0.50C0E 03 0.5C00E 03 0.5C00E 03 0.50C0E 03 0.50C0E 03 0.5CCOE 03 0.5CCOE 03 0.5CCOE 03 0.5CCOE 03	0.5236E CO 0.1047E C1 0.1571E C1 0.2094E C1 0.2618E C1 0.3142E C1 0.3665E C1 0.4189E C1 0.4712E C1 C.5236E C1 0.5759E C1	0.3314E 0.1784E 0.1121E 0.9972E 0.1124E 0.1327E 0.1537E	02	0.1210E 05 0.1025E 05 0.2688E 04 -0.1756E 05 -0.2323E 05 -0.2273E 05 -0.1597E 05	0.3040E-02 0.2310E-02 0.1480E-02 0.7199E-03 0.1462E-03 -0.2034E-03 -0.3547E-03 0.3547E-03 0.2763E-03	0.2816E-02 0.2724E-C2 0.2394E-02 0.1856E-02 0.1213E-02 0.5867E-03 0.6297E-04 -0.3218E-03	-0.7336E-09 -C.6372E-09 -0.4998E-09 -0.3466E-09 -C.2086E-09 -C.9678E-10 -0.3151E-10 -0.3151E-10	-0.3640E-09 -0.2694E-09 -0.1723E-09 -0.8333E-10 -0.1179E-10 0.3598E-10 0.5869E-10 0.5946E-10		-0.5617E-11 -0.1675E-10 -0.1922E-10 -0.1412E-10 -0.3994E-11 0.7721E-11 0.1736E-10 0.2189E-10 0.1972E-10

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U.60COE U3 0.5236E 00 C.1048E U3 0.2647E 05 -0.5438E 04 0.2412E-02 0.2614E-02 -0.5807E-09 -0.3269E-09 -0.5450E-10 0.4581E-11
0.60COE 03
        0.1047E C1 0.7785E 02 Q.1918E U5 0.4268E 04 0.2268E-02 0.2636E-02 -0.59C5E-09 -0.2868E-09 -0.4265E-10 -0.7039E-11
        C.1571E C1 0.5196E 02 0.9023E 04 0.8888E 04 0.1836E-02 0.252CE-C2 -C.5384E-09 -0.2243E-09 -0.2880E-10 -0.1371E-10
C.6COOE C3
0-6000E 03
        0.2618E C1 0.1782E 02 -C.8040E 04 0.2131E 04 0.7338E-03 0.1812E-02 -C.3382E-09 -0.8820E-10 -0.3809E-11 -0.1203E-10
        0.3142E C1 0.1043E 02 -0.1012E 05 -0.5936E 04 0.2959E-03 0.1310E-02 -0.2319E-09 -0.3328E-10 0.3558E-11 -0.5792E-11
C.6COUE 03
0.6000E 03 0.3665E C1 0.7433E 01 -C.6824E 04 -0.1337E 05 0.4348E-05 0.8123E-03 -0.1416E-09 0.5335E-11 0.6131E-11 0.1543E-11
0.60C0E C3 0.4189E C1 0.6923E 01 0.5615E 03 -0.1744E 05 -0.1471E-03 0.3827E-03 -C.7334E-10 0.2638E-10 0.4146E-11 0.7796E-11
0.60C0E 03 0.4712E 01 0.7550E 01 0.9498E 04 -0.1654E 05 -0.1890E-03 0.5243E-04 -0.2633E-10 0.3163E-10 -0.1118E-11 0.1114E-10
0.60C0E 03 0.5236E 01 0.8589E 01 0.1702E 05 -0.1068E 05 -0.1561E-03 -0.17C6E-C3 C.3127E-11 0.2445E-10 -0.7685E-11 0.1054E-10
0.6000E 03 0.5759E 01 0.9785E 01 0.2072E 05 -0.1396E 04 -0.7870E-04 -0.2889E-03 0.1925E-10 0.8590E-11 -0.1341E-10 0.5952E-11
0.8600E 03 U.1047E C1 0.5447E 02 0.2042E 05 0.2233E 04 0.1215E-02 0.2192E-02 -0.3984E-09 -0.1644E-09 -0.2459E-10 -0.8897E-11
C.8000E 03 0.1571E C1 C.4C38E 02 0.1255E 05 0.6223E 04 0.1125E-02 0.2138E-02 -C.3569E-09 -0.1456E-09 -0.1695E-10 -0.1121E-10
0.8000E 03 0.2094E C1 0.2750E C2 0.4807E 04 0.6094E 04 0.8811E-03 0.1952E-02 -0.3574E-09 -0.1115E-09 -0.9649E-11 -0.1130E-10
C.80C0E U3 0.3665E C1 0.7179E 01 -0.1063E 04 -0.7249E 04 0.1268E-03 0.9748E-03 -0.1699E-09 -0.1306E-10 0.2552E-11 -0.2220E-11
0.8000E 63 0.41d9E 01 0.5320E 01 0.3440E 04 -0.9531E 04 0.2793E-05 0.6588E-03 -0.1185E-09 0.3598E-11 0.2288E-11 0.1205E-11
0.800UE 03 0.4712E 01 0.4621E 01 0.8850E 04 -0.8355E 04 -0.5463E-04 0.4003E-03 -0.7513E-10 0.1097E-10 0.3708E-12 0.3370E-11
C.8CCOE L3 0.5236E 01 C.4535E 01 0.1437E U5 0.2736E 04 -0.6176E-04 0.2095E-03 -0.3369E-10 0.4806E-11 -0.4824E-11 0.2354E-11
0.8000E 03 0.5759E C1 0.4747E 01 0.1305E 05 -0.3857E 04 -0.3592E-04 0.8752E-04 -0.5125E-10 0.1065E-10 -0.2329E-11 0.3772E-11
0.1000E 64 0.5236E 00 C.4415E 02 0.2718E 05 ~0.3133E 04 0.1551E-03 0.1323E-02 -C.1750E-09 -0.2534E-10 -0.1918E-10 -0.8166E-11
0.1000E 04 0.1047E 01 0.3958E 02 0.2137E 05 0.2525E 04 0.5738E-03 0.1719E-02 -0.2753E-09 -0.8053E-10 -0.1489E-10 -0.9058E-11
0.1777E-C2 -0.3C17E-09 -0.8781E-10 -0.1022E-10 -0.9563E-11
        G.2094E L1 0.2361E 02 0.8173E 04 0.6201E 04 0.5773E-03
                                                     0.1684E-02 -0.2903E-09 -0.7499E-10 -0.5798E-11 -0.9019E-11
0.1000E 04
C.10C0E 04 0.2618E C1 0.1651E C2 G.3343E 04 0.3906E 04 0.4256E-03
                                                     0.1494E-02 -C.2572E-09 -0.5411E-10 -0.2102E-11 -0.7483E-11
C.10C0E 04 0.3665E C1 0.7677E 01 0.1873E 04 -0.2863E 04 0.1289E-03 0.9884E-03 -0.17C5E-09 -0.1428E-10 0.1809E-11 -0.2735E-11
0.1600E 04 0.4712E C1 0.4422E 01 0.7831E 04 -0.3129E 04 -0.1602E-04 0.5322E+C3 -C.5885E-10 0.5044E-11 0.9420E-12 0.1092E-11
0.1000E 04 0.5759E C1 0.3650E C1 C.10CLE 05 0.5149E 04 -0.2482E-04 0.2525E-C3 -C.5679E-10 0.4168E-11 -0.1884E-11 0.1237E-11
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TABLE III. - Continued. EARTH-PLANET FLYBY TRAJECTORIES

(e) Earth-Saturn flyby trajectories

TIME	124	J	VX(T)	VY(T)	AX (0)	AY(G)	AXDOT(0)	AYDOT(O)	(T) TOOXA	AYDOT(T)
0.4000E U3 0.4000E U3 0.4000E U3 0.4000E U3 0.4000E U3 0.4000E U3 0.4000E U3 0.4000E U3 0.4000E U3 0.4000E U3	0.2618E C1 C.3142E O1 G.3665E C1 U.4189E C1 U.4712E C1 U.5236E C1	0.8322E 03 0.7511E 02 0.8568E 02 0.1010E 03 0.1133E 03 0.1216E 03 0.1279E 03		0.4802E 05 0.4103E 05 0.2010E 05 -0.8639E 04 -0.3693E 05 -0.5661E 05 -0.6193E 05 -0.5123E 05	0.5389E-02 0.3296E-02 0.1145E-02 -0.6162E-03 -0.1702E-02 -0.2100E-02 -0.2013E-02 -0.1665E-02 -0.1193E-02	0.3912E-02 0.4151E-C2 0.3546E-C2 0.2247E-02 0.6473E-C3 -0.8010E-03 -0.1853E-C2 -0.25C1E-C2 -0.2817E-C2	C.3789E-10 C.23C4E-09 O.3247E-09 O.3552E-09 O.3515E-09	-0.4865E-09 -0.2947E-09 -0.9697E-10 0.9125E-10 0.2426E-09 0.3284E-09 0.3410E-09 0.2939E-09 0.2032E-09	-0.9353E-10 -0.3887E-10 0.1600E-10 0.5781E-10	-0.3721E-10 -0.6059E-10 -0.5687E-10 -0.3020E-10 0.9931E-11 0.5158E-10 0.8268E-10 0.9363E-10 0.8009E-10
C.6000E U3 O.66C00E U3 O.66C00E U3 O.66C00E U3 O.66C00E U3 O.66C00E U3 O.60C00E U3 O.60C00E U3 O.60C00E U3	C.3665E C1 C.4189E C1 C.4712E C1 C.5236E O1	0.4379E 0 0.2829E 0 C.2348E 0 0.2461E 0 0.2789E 0 0.3138E 0		0.2239E 05 0.2927E 05 0.2534E 05 0.1223E 05 -0.5950E 04 -0.2372E 05 -0.3577E 05 -0.3847E 05 -0.3088E 05	0.3294E-02 0.2392E-02 0.1382E-02 0.4833E-03 -0.1591E-03 -0.5063E-03 -0.6072E-03 -0.5424E-03	0.3148E-C2 0.3G8CE-C2 0.2684E-02 0.2005E-C2 0.1191E-02 0.4134E-03 -0.2099E-03 -0.6407E-C3 -0.8853E-C3	-C.6188E-10 0.2254E-10 C.7111E-10 0.9437E-10	-0.3660E-09 -0.2566E-09 -0.1457E-09 -0.4525E-10 0.3343E-10 0.8200E-10 0.9895E-10 C.88896E-10 0.5892E-10	-0.4286E-10 -0.2413E-10 -0.5594E-11 0.8976E-11 0.1682E-10 0.1679E-10 0.9625E-11 -0.2221E-11	-0.1122E-10 -0.1944E-10 -0.1937E-10 -0.1219E-10 -0.6117E-12 0.1179E-10 0.2141E-10 0.2536E-10 0.2220E-10
0.80C0E C3 0.80C0E C3 0.8CC0E C3		C.5494E 0 0.3479E 0 C.2156E 0 0.1465E 0 0.1214E 0 0.1206E 0 0.1302E 0 0.1431E 0	3	0.1588E 05 0.2137E 05 0.1885E 05 0.9549E 04 -0.3474E 04 -0.1616E 05 -0.2462E 05 -0.2624E 05	0.2048E-02 0.1667E-02 0.1134E-02 0.6058E-03 0.1863E-03 -0.8156E-04 -0.2061E-03 -0.2217E-03	0.2698E-02 0.2599E-02 0.2309E-02 0.1859E-02 0.1325E-02 0.7998E-03 0.3544E-03 0.2193E-04	-C.141CE-09 -O.73G2E-10 -C.27G4E-10 -C.9141E-12	-0.2533E-09 -0.1973E-09 -0.1314E-09 -0.6823E-10 -0.1652E-10 0.1842E-10 0.3536E-10 0.3638E-10	-0.2478E-10 -0.1535E-10 -0.6278E-11 0.9742E-12 0.5268E-11 0.6103E-11 0.3749E-11 -0.8011E-12	-0.7949E-11 -0.1127E-10 -0.1112E-10 -0.7931E-11 -0.2791E-11 0.2816E-11 0.7340E-11 0.9516E-11 0.8674E-11
	0.2094E 01 0.2618E 01 0.3142E C1 0.3665E C1 0.4189E C1 0.4712E 01 C.5236E C1	0.5895E 0 0.4363E 0 0.2973E 0 0.1936E 0 0.1285E 0 0.5459E 0 0.7878E 0	2	0.1337E 05 0.1778E 05 0.1594E 05 0.8788E 04 -0.1268E 04 -0.1104E 05 -0.1750E 05 -0.1862E 05 -0.1399E 05	0.1227E-02 0.1134E-02 0.8584E-03 0.5352E-03 0.2513E-03 0.4962E-04 -0.6311E-04 -0.1012E-03 -0.8656E-04	0.2263E-02 0.2229E-02 0.2030E-02 0.1769E-02 0.1322E-02 0.9366E-03 0.5848E-03 0.3124E-03	2 -0.3326E-09 2 -0.4135E-09 2 -0.415CE-09 2 -0.3716E-09 2 -0.3248E-09 2 -0.2316E-09 3 -0.1644E-09 5 -0.6954E-10 3 -0.4225E-10	-0.1625E-09 -0.1427E-09 -0.1053E-09 -0.6425E-10 -0.2817E-10 -0.1834E-11 0.1313E-10 0.1754E-10 0.1359E-10	-0. 1568E-10 -0. 1004E-10 -0. 4731E-11 -0. 4606E-12 0. 2210E-11 0. 3018E-11 0. 2085E-11 -0. 8645E-13 -0. 2727E-11	-0.7279E-11 -0.8450E-11 -0.7799E-11 -0.6038E-11 -0.3085E-11 0.1242E-12 0.2790E-11 0.4242E-11

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0.1200E 04 0.1047E C1 0.4476E 02 0.2391E 05 0.1282E 05 0.6617E-03 0.1828E-02 -0.3001E-09 -0.9215E-10 -0.1027E-10 -0.6853E-11
C.1200E 04 0.1571E C1 0.3551E 02 0.1274E 05 0.1624E 05 0.7452E-03 0.1902E-02 -C.33C4E-09 -0.9812E-10 -0.6635E-11 -0.6957E-11
C.126UE 64 0.2694E 61 C.2584E 62 6.1931E 64 0.1469E 65 0.6258E-03 0.1789E-02 -C.3136E-09 -0.7999E-10 -0.3245E-11 -0.6302E-11
0.1260E C4 0.2618E C1 C.1784E C2 -0.0076E C4 0.8861E C4 0.4302E-03
                                                    0.156CE-02 -C.2718E-09 -0.5382E-10 -0.5008E-12 -0.4859E-11
C.1200E 64 G.3665E 61 C.8809E 61 -6.7937E 64 -0.7263E 04 0.8529E-04
                                                    0.9623E-03 -C.1686E-09 -0.8262E-11 0.1910E-11 -0.7519E-12
C.12COE U4 C.4189E C1 U.7OlDE U1 -0.2239E U4 -0.1249E 05 -0.8758E-05 0.6825E-C3 -C.1246E-09 0.4333E-11 0.1481E-11 0.1041E-11
G.120vc 04 0.4712c C1 0.629c C1 0.5482E G4 -0.1339c O5 -0.5038E-04 0.4527E-03 -C.8981E-10 0.9521E-11 0.2726E-12 0.2107E-11
0.1200E 04 0.5230E 01 0.6613E 01 0.1263E 05 -0.9651E 04 -0.5210E-04 0.2835E-03 -0.6461E-10 0.8580E-11 -0.1262E-11 0.2218E-11
0.1260L ∪4 0.2757E C1 0.0086E C1 0.1086E 05 -0.2325E 04 -0.2834E-04 0.1761E-03 -0.4787E-10 0.3391E-11 -0.2609E-11 0.1380E-11
G.1460t t4 C.1647t t1 0.3467t 02 0.2327t 05 0.1352t 05 0.2568E-03 0.1377t-02 -0.2055E-09 -0.3628E-10 -0.6700E-11 -0.6430E-11
0.1400E 04 0.1571E 01 0.2935E 02 0.1326E 05 0.1578E 05 0.4594E-03 0.1604E-02 -0.2654E-09 -0.6270E-10 -0.4361E-11 -0.5921E-11
C.1460E G4 0.2C94E 01 C.2263E 02 G.3728E 04 G.1431E 05 G.4408E-03 G.1574E-02 -0.2672E-C9 -C.5834E-10 -0.2101E-11 -0.5172E-11
G.14CUE 04 0.314ZE C1 0.1178E 02 -0.67C1E 04 0.2384E 04 0.1981E-03 0.1155E-02 -G.2054E-09 -0.2484E-10 0.9668E-12 -0.2534E-11
G.14CGE C4 C.4712E C1 C.5687E C1 0.4757E C4 -0.9571E 04 -0.2826E-04 0.5224E-C3 -C.5565E-10 0.5748E-11 0.4515E-12 0.1132E-11
0.14C0t C4 C.5236E t1 C.5196E G1 t.1034E U5 -0.6540E U4 -0.3626E-04 0.3710E-C3 -C.7689E-10 0.6106E-11 -0.5417E-12 0.1328E-11
C.14CUE 04 U.5759E C1 U.5CC6E 01 U.1347E U5 -U.6049E 03 -C.2359E-04 U.2678E-C3 -C.6C77E-10 C.3101E-11 -0.1436E-11 0.8959E-12
0.16C0E C4 0.1571E (1 0.2456E C2 0.1335E U5 0.1598E O5 0.2460E-03 0.1326E-C2 -0.2129E-09 -0.3460E-10 -0.2779E-11 -0.5107E-11
0.16Cut 04 C.2U44E L1 0.1995E 02 0.4795E 04 0.1439E 05 0.2960E-03 0.1379E-C2 -0.2292E-09 -0.4049E-10 -0.1259E-11 -0.4329E-11
0.1e00E C4 0.3142E C1 C.1133E C2 -C.4842E 04 0.3883E 04 0.1563E-03 0.1116E-C2 -C.1967E-09 -0.2046E-10 0.8702E-12 -0.2189E-11
        0.1600E 04 0.4189E (1 0.6649E 01 -0.9023E 03 -0.5863E 04 0.1402E-04 0.7256E-03 -0.130CE-09 -0.627IE-12 0.1059E-11 -0.1109E-13
0.16CCE U4 0.5230E U1 C.4897E 01 0.8424E 04 -0.4241E 04 -0.2899E-04 0.4156E-C3 -C.8375E-16 0.4731E-11 -0.1627E-12 0.8692E-12
0.1660E U4 C.5759E C1 C.4556E C1 0.1076E 05 0.6119E U3 -0.2195E-U4 0.3224E-C3 -C.6859E-10 0.2895E-11 -0.8056E-12 0.6438E-12
```

TABLE III. - Continued. EARTH-PLANET FLYBY TRAJECTORIES

(f) Earth-Uranus flyby trajectories

TIME	PSI	J	VX(T)	VY(T)	AX (O)	AY(C)	AXDOT(0)	AYDOT(O)	AXDOT(T)	AYDOT(T)
0.4400E 03 0.400E 03 0.400E 03 0.400E 03 0.400E 03 0.400E 03 0.400E 03 0.4400E 03 0.4400E 03 0.4600E 03	0.4189E C1 0.4712E C1 0.5236E C1	C.3926E 0 0.4155E C 0.4661E 0 C.5087E C 0.5312E 0 0.5466E 0 G.1313E 0		0.9381E 05 0.1114E 06 0.960UE 05 0.5217E 05 -0.7795E 04 -0.6756E 05 -0.1108E 06 -0.1254E 06 -0.1252E 06	0.7691E-02 0.3721E-02 -0.3057E-03 -0.3462E-02 -0.5135E-02 -0.5373E-02 -0.4805E-02 -0.3959E-02 0.1008E-01	0.6451E-C2 0.7197E-C2 0.6C87E-C2 0.3421E-O2 0.8816E-C4 -0.2750E-C2 -0.4560E-O2 -0.5549E-C2 -0.36C2E-C2	0.4523E-09 0.7231E-09 0.7959E-09 0.7776E-09 -0.1809E-08	-0.5077E-09 -0.2379E-09 0.6923E-10 0.3995E-09 0.6996E-09 0.8729E-09 0.8779E-09 -0.1481E-08	-0.1318E-09 -0.2704E-10 0.7753E-10 0.1547E-09 0.1853E-09 0.1629E-09 0.9408E-10 -0.2070E-11 -0.1270E-09	-0.1202E-09 -0.1555E-09 -0.1366E-09 -0.7235E-10 0.1679E-10 0.1062E-09 0.1722E-09 0.1952E-09 0.2739E-09
0.80COE 03 0.8000E 03 0.80COE 03 0.80COE 03 0.80COE 03 0.80COE 03 0.80COE 03 0.80COE 03 0.80COE 03 0.80COE 03	0.3142E C1 0.3665E 01 0.4189E C1 C.4712E C1 0.5236E 01	0.6653E 0 0.5104E 0 0.4760E 0 0.5045E 0 0.5511E 0 0.5956E 0 0.6353E 0		0.4276E 05 0.5237E 05 0.4555E 05 0.2462E 05 -0.4293E 04 -0.3301E 05 -0.5346E 05 -0.5987E 05 -0.5032E 05	0.3327E-02 0.2342E-02 0.1236E-02 0.2630E-03 -0.4065E-03 -0.7317E-03 -0.7798E-03 -0.6529E-03 -0.4322E-03	0.3451E-02 0.3398E-C2 0.2949E-02 0.2159E-C2 0.1208E-C2 0.3121E-G3 -0.3844E-C3 -0.8425E-C3 -0.1078E-02	-C.1825E-09 -0.4576E-10 0.4171E-10 C.8896E-10 0.1C89E-09	-0.3484E-09 -0.2329E-C9 -0.1162E-09 -0.1096E-10 0.6993E-10 0.1166E-09 0.1272E-09 0.1075E-09 0.6610E-10	-0.2764E-10 -0.1296E-10 0.1480E-11 0.1250E-10 0.1779E-10 0.1652E-10 0.9414E-11 -0.1367E-11	-0.1354E-10 -0.1890E-10 -0.1749E-10 -0.1030E-10 0.2838E-12 0.1120E-10 0.1941E-10 0.2257E-10 0.1960E-10
C.1000E 04 0.1000E 04 0.1000E 04 0.1000E 04 0.1000E 04 0.1000E 04 0.1000E 04 0.1000E 04 0.1000E 04 0.1000E 04		0.4772E 0 0.3348E 0 0.2733E 0 0.2635E 0 0.2776E 0 0.2991E 0		0.3415E 05 0.4192E 05 0.3664E 05 0.2016E 05 -0.2671E 04 -0.2534E 05 -0.4145E 05 -0.4643E 05 -0.3878E 05	0.2322E-02 0.1798E-02 0.1115E-02 0.4677E-03 -0.1667E-04 -0.2926E-03 -0.3844E-03 -0.2341E-03	0.2976E-C2 0.2889E-02 0.2545E-C2 0.1983E-02 0.1313E-02 0.6663E-03 -0.2369E-03 -0.4432E-03	3 -C.1187E-09 3 -C.4387E-10 3 0.3110E-11 3 C.2868E-10	-0.2703E-09 -0.1987E-09 -0.1190E-09 -0.4487E-10 0.1362E-10 0.5001E-10 0.6308E-10 0.5623E-10 0.3486E-10	-0.1735E-10 -0.9157E-11 -0.1229E-11 0.4890E-11 0.8051E-11 0.7811E-11 0.4524E-11 -0.7396E-12 -0.6449E-11	-0.8279E-11 -0.1088E-10 -0.1011E-10 -0.6407E-11 -0.9282E-12 0.4776E-11 0.9153E-11 0.1099E-10 0.9686E-11
0.1200E U4 0.1200E 04 0.1200E 04 0.1200E 04 0.1200E 04 0.1200E 04 0.1200E 04 0.1200E 04 0.1200E 04 0.1200E 04	0.3142E C1 0.3665E 01 0.4189E C1 0.4712E 01 0.5236E 01	0.1141E (0.1166E (0.1176E (0.1172E (0.1165E (0.1712E (0.1792E (0.1907E (03 0.35898 09	0.5064E 05 0.6193E 05 0.5688E 05 0.3699E 05 0.7611E 04 5 -0.2370E 05 -0.3321E 05 -0.3732E 05 5 -0.3100E 05	5 -0.1016E-02 5 -0.9559E-03 5 -0.7983E-03 -0.5428E-03 -0.1556E-03 5 -0.1967E-03 -0.1414E-03	-0.2863E-03 -0.7845E-03 -0.1183E-02 -0.1487E-02 -0.1678E-03 -0.1671E-03 0.4083E-03 0.9581E-04 -0.9944E-04	3	0.1625E-09 0.1864E-09 0.1881E-09 0.1245E-09 0.1245E-09 0.3402E-10 0.3262E-10	-0.1019E-10 0.1102E-11 0.1242E-10 0.2058E-10 0.2330E-10 0.1973E-10 0.2578E-11 0-0.3476E-12 -0.3589E-11	0.4785E-11 0.6003E-11

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0.1400t 04 0.5236t 00 0.7036t 02 0.4609t 05 0.1529t 05 0.4493t-03 0.1695t-02 -0.2432t-09 -0.7199t-10 -0.1163t-10 -0.4850t-11
0.1400£ U4
       U.1571E C1 C.4642E 02 C.1126E 05 0.3189E 05 0.1019E-02 0.2220E-C2 -0.4C4GE-09 -0.1286E-09 -0.4797E-11 -0.5758E-11
C.1400E 04
        0.2094E 01 0.3291E 02 -0.7341E 04 0.2797E 05 0.7654E-03 0.2037E-02 -0.3664E-09 -0.9380E-10 -0.1521E-11 -0.5165E-11
0.1400E 04
        [.2618E C1 0.2281E 02 -0.2169E 05 0.1628E 05 0.4537E-03 0.1711E-02 -0.3619E-09 -0.5423E-10 0.1046E-11 -0.3599E-11
0.14CUE 04
        0.3142E C1 0.1059E C2 -0.2672E C5 0.1605E 03 0.1815E-03 0.1310E-02 -(.2294E-09 -0.1955E-10 0.2501E-11 -0.1410E-11
        C.36o5E C1 0.1350E L2 -0.2315E U5 -0.1583E U5 -0.5315E-U5
                                                    0.14COE U4
       0.4189E 01 0.1242E 02 -0.1174E 05 -0.2720E 05 -0.1006E-03
                                                    0.5527E-03 -C.1C82E-09 0.1781E-10 0.1679E-11 0.2677E-11
G.1400E 04 G.4712E C1 G.1242E 02 G.4641E 04 -0.3074E 05 -0.1214E-03 G.2822E-03 -G.6875E-10 G.1983E-10 -0.1083E-12 G.3560E-11
0.14CUE C4 0.5759E C1 0.1356E C2 0.305UE U5 -0.1261E 05 -0.3552E-04 0.1051E-C4 -0.2739E-10 0.2351E-11 -0.3771E-11 0.1899E-11
G.1660E C4 0.1C47E C1 0.4862E 02 0.2860E 05 0.2586E 05 0.6176E-03 0.1814E-C2 -C.2562E-09 -0.8788E-10 -0.5913E-11 -0.4860E-11
0.1600E 04 0.1571E C1 0.3906E 02 0.1159E 05 0.2952E 05 0.7423E-03 0.1951E-(2 -0.3390E-09 -0.9858E-10 -0.3492E-11 -0.4723E-11
G.160vE 04 U.2018E C1 0.2047E 02 -C.1718E 05 0.1550E 05 U.3948E-03 0.1590E-02 -C.2769E-09 -0.5002E-10 0.6004E-12 -0.2940E-11
0.1606E 04 0.3665E C1 0.1163E 02 -0.1951E 05 -0.1262E 05 0.3629E-04 0.9325E-C3 -0.1662E-09 -0.2463E-11 0.1835E-11 0.2600E-12
C.16CGE U4 U.4189E C1 0.1014E 02 -0.9839E 04 -0.2258E 05 -0.4954E-04 0.6325E-03 -0.1157E-09 0.9241E-11 0.1214E-11 0.1565E-11
C.1600E C4 C.4712E C1 0.9653E C1 0.3644E 04 -0.2574E 05 -0.775?E-04 0.3944E-C3 -0.8425E-10 0.1260E-10 0.4104E-13 0.2242E-11
C.1660E C4 0.5236E C1 C.9691E 01 0.1094E 05 -0.2122E 05 -0.6421E-04 0.2284E-C3 -0.5543E-10 0.9381E-11 -0.1308E-11 0.2130E-11
0.1600E 04 0.5759E 01 0.9971E 01 0.2619E 05 -0.1021E 05 -0.2728E-04 0.1334E-03 -0.4378E-10 0.1964E-11 -0.2420E-11 0.1263E-11
0.2000E 04 0.1571E C1 0.2863E 02 0.1126E 05 0.2731E 05 0.3309E-03 0.1462E-02 -C.2395E-09 -0.4644E-10 -0.1759E-11 -0.3523E-11
0.2000E 04 0.3142E 01 0.1294E 02 -0.1674E 05 0.3432E 04 0.1553E-03 0.1158E-02 -0.1995E-09 -0.2194E-10 0.9549E-12 -0.1157E-11
0.2000t 04 0.3665E C1 0.1000E 02 -0.1487E 05 -0.7884E 04 0.5606E-04 0.9197E-03 -0.1622E-09 -0.7929E-11 0.1085E-11 -0.2008E-12
0.206UE C4
       0.41d9E 01 0.8258E C1 - C.7584E 04 - O.1598E 05 - O.8477E-05 0.6943E-C3 - C.1276E-09 0.1313E-11 0.7887E-12 0.5776E-12
C.2CCCE C4 C.4712E C1 0.7340E C1 C.2727E 04 -0.1870E 05 -0.3736E-04 0.5050E-C3 -C.551CE-10 C.5330E-11 0.1912E-12 0.1020E-11
0.20CUE U4 0.5236E C1 0.6920E U1 C.1291E 05 -0.1536E 05 -0.3804E-04 0.363CE-03 -C.7748E-10 C.4888E-11 -0.5135E-12 0.1043E-11
0.2000E 04 0.5759E C1 0.6772E 01 0.1989E 05 -0.6954E 04 -0.2080E-04 0.2763E-C3 -0.6239E-10 0.1383E-11 -0.1109E+11 0.6604E-12
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TABLE III. - Continued. EARTH-PLANET FLYBY TRAJECTORIES

(g) Earth-Neptune flyby trajectories

TIME	P S 1	J	VX(T)	(T)YV	(0) XA	AY(G)	AXDOT(0)	AYDOT(O)	AXDOT(T)	AYDOT(T)
0.4000E C3 0.4000E C3 0.4000E C3 0.4000E C3 C.4000E C3 0.4000E C3 0.4000E C3 0.4000E C3 0.4000E C3	C.1C47E C1 O.1571E C1 C.2C94E C1 O.2618E C1 U.3142E C1 U.3665E C1 C.4189E C1 U.4712E C1 U.5236E C1	C.130GE 0 G.1131E 0 G.1097E 0 U.1167E 0 U.1271E 0 U.1342E 0 U.1367E 0 U.2530E 0 G.2479E 0	4	0.1552E 06 0.1822E 06 0.1573E 06 0.8761E 05 -0.7404E 04 -0.1023E 06 -0.1716E 06 -0.22119E 06 -0.1858E 06	0.9994E-02 0.3954E-02 -0.2153E-02 -0.6855E-02 -0.9142E-02 -0.9141E-02 -0.8111E-02 0.9163E-02 0.1262E-01	0.9618E-C2 0.1693E-C1 0.9248E-C2 0.5063E-C2 -0.3949E-C3 -0.4809E-02 -0.7339E-C2 -0.9122E-C2 -0.8163E-C2	0.1856E-09 0.9161E-09 0.1250E-08 0.1281E-08 -0.1561E-08 -0.2334E-08	-0.5205E-09 -0.1916E-09 0.2187E-09 0.7103E-09 0.1223E-08 0.1550E-08 0.1571E-08 -0.1981E-08 -0.1607E-08	-0.1838E-09 -0.2062E-10 0.1422E-09 0.2613E-09 0.3064E-09 0.2675E-09 -0.5872E-11 -0.1802E-09	-0.2193E-09 -0.2693E-09 -0.2337E-09 -0.1262E-09 0.1984E-10 0.1652E-09 0.2728E-09 0.4191E-09 0.3711E-09
0.8000E 03 0.8000E 03 0.8000E 03 0.8000E 03 0.8000E 03 0.8000E 03 0.8000E 03 0.8000E 03	0.4712E 01 0.5236E 01	0.1801E 0 0.1400E 0 0.1262E 0 0.1299E 0 0.1401E 0 0.1479E 0 0.1573E 0	3	C.7283E 05 C.8717E 05 U.7560E 05 O.4178E 05 -0.4721E U4 -0.5105E U5 -0.8451E 05 -0.9585E 05 -0.8178E 05	0.4355E-02 0.2761E-02 0.1067E-02 -0.3504E-03 -0.1241E-02 -0.1569E-02 -0.1488E-02 -0.1184E-02 -0.7760E-03	0.4195E-C2 0.4259E-C2 0.3656E-C2 0.3656E-C2 0.2483E-C2 -0.1C49E-C2 -0.1224E-C2 -0.1224E-C2 -0.1EC5E-C2	0.7475E-10 C.1714E-09 C.2113E-09 0.2182E-09	-0.3916E-09 -0.2306E-09 -0.7094E-10 0.7421E-10 0.1862E-09 0.2460E-09 0.2481E-09 0.2030E-09 0.1239E-09	-0.3266E-10 -0.1125E-10 0.9992E-11 0.2586E-10 0.3268E-10 0.2918E-10 0.1666E-10 -0.1359E-11 -0.1999E-10	-0.2371E-10 -0.3109E-10 -0.2782E-10 -0.1554E-10 0.1859E-11 0.1944E-10 0.3242E-10 0.3713E-10 0.3198E-10
C.10C0E C4 C.10G0E 04 C.10C0E U4 O.10C0E U4 O.10C0E C4 O.10C0E C4 O.10C0E C4 C.1CCUE C4 C.1CCUE C4 C.1CCUE U4 C.1CCUE U4 C.1CCUE U4 C.1CCUE U4 C.1CCUE U4 C.1CCUE U4	0.2094E 01 0.2618E C1 0.3142E C1 0.3665E C1 0.4189E C1 0.4712E C1 C.5236E C1	0.1627E C 0.1161E C 0.8440E C 0.6884E C 0.6863E C 0.7814E C 0.8227E C	03	0.5759E 05 0.6924E 05 0.6024E 05 0.3348E 05 -0.3407E 04 -0.4017E 05 -0.6668E 05 -0.7560E 05 -0.6432E 05	0.3203E-02 0.2243E-02 0.1149E-02 0.1853E-03 -0.4719E-03 -0.4719E-03 -0.8058E-03 -0.6593E-03 -0.4230E-03	0.3547E-02 0.3494E-02 0.3032E-02 0.2218E-02 0.1236E-03 -0.3125E-03 -0.8577E-03	8 -C.5C71E-10 6 C.37C2E-10 8 C.84GCE-10 C.1C34E-09	-0.3306E-09 -0.2176E-09 -0.1028E-09 0.5596E-12 0.7956E-10 0.1240E-09 0.1317E-09 0.1089E-09 0.6442E-10	-0.1975E-10 -0.8266E-11 0.3027E-11 0.1155E-10 0.1544E-10 0.1406E-10 0.8022E-11 -0.9033E-12 -0.1026E-10	-0.1246E-10 -0.1631E-10 -0.1476E-10 -0.8591E-11 0.2420E-12 0.9240E-11 0.1595E-10 0.1850E-10
C.1200E 04 0.1200E 04 C.12C0E C4 0.12C0E 04 0.12C0E 04 0.12C0E 04 0.12C0E 04 0.12C0E 04 0.1200E 04 0.1200E 04 0.1200E 04	0.2094E C1 C.2618E C1 0.3142E C1 0.3665E C1 0.4189E C1 C.4712E C1 0.5236E O1	0.0C47E (0.4591E (0.4591E (0.4020E (0.3993E (0.4202E (0.4468E (0.4732E (0.472E (0.4		0.4825E 05 0.5793E 05 0.5053E 05 0.2839E 05 0.2168E U4 0.03263E 05 0.05459E 05 0.06197E 05 0.6197E 05	0.2380±-02 0.1808±-02 0.1071±-02 0.3810±-03 -0.1230±-03 -0.3944±-03 -0.4648±-03 -0.3995±-03 -0.2581±-03	0.3102E-C2 0.3C24E-C3 0.2657E-C3 0.2657E-C3 0.2646E-C3 0.1313E-C3 0.61CGE-C3 0.4663E-C4 -0.337GE-C3	2 -C.2213E-09 3 -C.11CEE-09 4 -0.336CE-10 3 C.1342E-10 3 0.3775E-10	-0.2706E-09 -0.194IE-09 -0.1098E-09 -0.3195E-10 0.2873E-10 0.651IE-10 0.7582E-10 0.6485E-10 0.3842E-10	-0.1321E-10 -0.6199E-11 -0.6174E-12 -0.5803E-11 -0.8305E-11 -0.7736E-11 -0.4447E-11	-0.7968E-11 -0.1008E-10 -0.9147E-11 -0.5573E-11 -0.4409E-12 0.4819E-11 0.8790E-11 0.1038E-10 0.9084E-11

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0.16CvE 04 0.5236E 00 0.86ClE 02 0.5736E 05 0.2242E 05 0.6987E-03 0.1932E-02 -0.2949E-09 -0.1080E-09 -0.9952E-11 -0.3877E-11
0.16Cvt 04 0.1571E C1 0.5582E C2 0.1083E 05 0.4523E 05 0.1148E-02 0.2395E-02 -0.442CE-09 -0.1415E-C9 -0.3621E-11 -0.5298E-11
0.1660t 04 0.2094E C1 0.4610t C2 -C.1449E 05 0.3947E 05 0.8121E-03 0.2174E-02 -0.3925E-09 -0.9724E-10 -0.5078E-12 -0.4722E-11
0.160ut 04 0.3665E C1 0.1992E 02 -0.3541E 05 -0.2271t 05 -0.8053E-04 0.8568E-03 -0.1561E-09 0.1582E-10 0.3083E-11 0.1487E-11
U.1660b b4 0.4189E (1 0.1941b 02 -0.1916E 05 -0.3915E 05 -0.1688E-03 0.4613E-03 -0.9691E-10 0.2795E-10 0.1841E-11 0.3284E-11
0.1660E 04 0.4712E C1 0.1993E 02 0.3377E 04 -0.4473E 05 -0.1706E-03 0.1692E-03 -0.5548E-10 0.2724E-10 -0.1714E-12 0.4083E-11
C.16CUE 04 0.5236E 01 0.2085E 02 0.2588E 05 -0.3786E 05 -0.1176E-03 -0.1265E-04 -C.2945E-10 0.1707E-10 -0.2361E-11 0.3661E-11
0.1600E 04 0.5759E 01 0.2191E 02 0.4208E 05 -0.2028E 05 -0.3858E-04 -0.9022E-04 -0.1558E-10 0.1461E-11 -0.4095E-11 0.2095E-11
C.2000E 04 0.1047E 01 0.4935E 02 0.3219E 05 0.3536E 05 0.4928E-03 0.1654E-02 -0.2701E-09 -0.7388E-10 -0.3862E-11 -0.3791E-11
C.2000t 04 0.1571E 01 0.4068E 02 0.1110E 05 0.3902E 05 0.6856E-03 0.1918E-02 -C.3291E-09 -0.9416E-10 -0.2135E-11 -0.3561E-11
0.20CUL U4 0.2094E C1 0.3074E C2 -C.95C2E 04 0.3383E 05 0.5686E-03 0.1826E-C2 -C.316EE-09 -0.7597E-10 -0.4664E-12 -0.3053E-11
0.2000E u4 0.3665E C1 0.1394E 02 -C.2738E 05 -0.1639E 05 0.1566E-04 0.9185E-03 -0.1649E-09 -0.1190E-11 0.1597E-11 0.4447E-12
0.2000E 04 0.4712E 01 0.1213E 02 0.2790E 04 -0.3426E 05 -0.8367E-04 0.3826E-03 -0.8416E-10 0.1260E-10 0.1100E-13 0.1943E-11
0.2000E 04 0.5236E C1 0.1222E 02 C.2039E 05 -0.2898E 05 -0.6470E-C4 0.2220E-C3 -C.5990E-10 0.8725E-11 -0.1101E-11 0.1800E-11
0.2000E 04 0.5759E C1 C.1254E 02 C.33C0E 05 -0.1522E 05 -0.2416E-04 0.1345E-03 -C.4480E-10 0.8338E-12 -0.1994E-11 0.1058E-11
C.2460E 04 C.5236E CC 0.8886E 01 0.2491E 05 0.1813E 05 0.3299E-04 0.2051E-C2 -C.4665E-1C -0.1012E-10 -0.1206E-11 -0.7223E-12
0.2460b 04 0.1647E 01 0.8991E 01 0.1286E 05 0.2872E 05 0.4450E-04 0.2363E-03 -0.4483E-10 -0.1263E-10 -0.7207E-12 -0.1289E-11
C.24CUE C4 0.1571E C1 C.31C2E C2 0.1037E 05 0.3598E 05 0.3453E-C3 0.1452E-C2 -0.2431E-09 -C.5347E-10 -0.1188E-11 -0.2710E-11
0.240UE 04 (.2094E 01 0.2493E 02 -0.6839E 04 0.307lE U5 0.3717E-03 0.1537E-02 -0.2585E-09 -0.5525E-10 -0.2504E-12 -0.2214E-11
0.24CUE U4 0.2618E C1 C.19CIE 02 -0.1976E 05 0.190IE 05 0.2700E-03 0.1394E-C2 -C.2374E-09 -0.4033E 10 0.5179E-12 -0.1548E-11
C.24C0b U4 0.3665E C1 0.1157E 02 -0.2243E 05 -0.1199E 05 0.4081E-04 0.9116E-C3 -C.1619E-C9 -0.7458E-11 0.9970E-12 0.6991E-13
0.2400E 04 0.4189E 01 0.9909E 01 -0.1226E 05 -0.2320E 05 -0.2249E-04 0.6745E-03 -0.1260E-09 0.2003E-11 0.6719E-12 0.7128E-12
C.24CUE 04 0.4712E C1 0.91C1E 01 0.2098E 04 -0.2725E 05 -0.4687E-04 0.4796E-C3 -C.9672E-10 0.5662E-11 0.9694E-13 0.1050E-11
0.2400t 04 0.5236E 01 0.8786E 01 0.1648E 05 -0.2309E 05 -0.4180E-04 0.3378E-C3 -C.7498E-10 0.4518E-11 -0.5518E-12 0.1011E-11
C.2400E 04 0.5759E 01 0.8726E 01 0.2675E 05 -0.1192E 05 -0.1924E-04 0.2499E-03 -C.6C18E-10 0.2278E-12 -0.1081E-11 0.6178E-12
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TABLE III. - Concluded. EARTH-PLANET FLYBY TRAJECTORIES

(h) Earth-Pluto flyby trajectories

TIME	IZY	J	VX(T)	VY(T)	AX (0)	AY (C)	AXDOT(C)	AYDOT(0)	AXDOT(T)	AYDOT (T)
0.4000E U3 0.4000E 03 0.4000E 03 0.4000E 03 0.4000E 03 0.4000E 03 0.4000E 03 0.4000E 03 0.4000E 03	0.5236E CU C.1647E C1 O.1571E C1 O.2C94E C1 C.2618E C1 G.3142E C1 U.3665E C1 O.4189E C1 C.4712E C1 O.5236E O1 O.5759E C1	0.2241E 04 0.2036E 04 0.2015E 04 0.2133E 04 0.2287E 04 0.2379E 04 0.2379E 04 0.3857E 04 0.3786E 04	-0.2217E 06 -0.1275E 06 -0.4896E 04 0.1250E 06	0.2082E 06 0.2434E 06 0.2102E 06 0.1181E 06 -0.7203E 04 -0.1324E 06 -0.2243E 06 -0.2728E 06 -0.2385E 06	0.1190E-01 0.4083E-02 -0.3810E-02 -0.9840E-02 -0.1264E-01 -0.1243E-01 -0.1108E-01 0.9339E-02	0.1247E-C1 0.1427E-01 0.1209E-01 0.6483E-C2 -0.7429E-03 -0.6496E-02 -0.9540E-02 -0.1348E-C1 -0.1173E-C1	-0.2594E-08 -C.1756E-08 -0.7135E-09 0.3536E-09 C.13C7E-08 0.1683E-08 0.1679E-08 -0.22C6E-08 -C.2696E-08	0.9515E-09 0.1677E-08 0.2175E-08 0.2221E-08 -0.2063E-08 -0.1644E-08	-0.2313E-09 -0.1716E-10 0.1965E-09 0.3525E-09 0.4106E-09 0.3577E-09 0.2078E-09 -0.5893E-11 -0.2285E-09	-0.3064E-09 -0.3694E-09 -0.3196E-09 -0.1745E-09 0.2127E-10 0.2157E-09 0.3601E-09 0.5184E-09 0.4575E-09
0.1000E 04 0.1000E 04 0.1000E 04 0.1000E 04 0.1000E 04 0.1000E 04 0.1000E 04 0.1000E 04 0.1000E 04	C.5236E CO U.1047E C1 C.1571E C1 U.2C94E C1 C.2618E C1 C.3142E C1 U.3665E C1 U.4712E C1 C.4712E C1 C.5236E C1 U.5759E C1	0.1333E C3 C.1181E 03 0.1184E 03 0.1255E 03 C.1333E 03 0.1397E 03 C.1452E C3	0.5880E 05 C.7153E 04 -0.4429E 05 -0.8196E 05 -0.9602E 05 -0.8297E 05 -0.4657E 05 0.3218E 04 0.5296E 05	0.8088E 05 0.4522E 05 -0.3794E 04 -0.5269E 05 -0.8811E 05 -0.1004E 06 -0.8588E 05	0.3815E-02 0.2507E-02	0.3990E-02 0.3953E-C2 0.3441E-02 0.2411E-02 0.1156E-02 -0.4741E-C5 -0.8666E-03 -0.1396E-02 -0.1633E-02	-0.97C6E-09 -0.8211E-09 -0.6C61E-09 -0.3666E-09 -0.1481E-09 -0.1262E-10 -0.1565E-09 -0.1565E-09 -0.1634E-09	0.1429E-09 0.1943E-09 0.1971E-09 0.1599E-09 C.9416E-10	-0.2216E-10 -0.7657E-11 0.6690E-11 0.1740E-10 0.2201E-10	-0.1700E-10 -0.2179E-10 -0.1945E-10 -0.1102E-10 0.8606E-12 0.1285E-10 0.2172E-10 0.2498E-10 0.2156E-10
0.16C0E 04 0.16C0E 04 C.16C0E 04 0.16C0E 04 0.16C0E 04 0.16C0E 04 C.16C0E 04 C.16C0E 04 C.16C0E 04 0.16C0E 04	C.5236E CO G.1C47E O1 G.1571E C1 U.2094E C1 G.2618E O1 C.3142E C1 G.3665E G1 C.4189E C1 O.4712E C1 C.5236E O1 O.5759E C1	0.3984E 02 0.3351E 02 0.3170E 02 0.3226E 02 0.3371E 02 0.3539E 02	0.4363E 05 0.1033E 05 0.1033E 05 0.2256E 05 0.4678E 05 0.5028E 05 0.62705E 05 0.3194E 05 0.3348E 05	0.5029E 05 0.5929E 05 0.5169E 05 0.2965E 05 -0.6828E 03 -0.3097E 05 -0.5294E 05 -0.6056E 05 -0.5167E 05	0.1707E-02 0.1412E-02 0.9137E-03 0.4083E-03	0.2733E-02 0.2652E-C2 0.24G3E-02 0.1918E-02 0.1333E-02 0.7630E-03 0.2934E-03 -0.3759E-C4 -0.2273E-C3	-0.5300E-09 -0.5124E-09 -0.4381E-09 -0.3367E-09 -0.2318E-09 -0.1412E-09 -0.7371E-10 -0.2927E-10 -0.3596E-11	0 -0.2104E-09 0 -0.1643E-09 0 -0.1028E-09 0 -0.4280E-10 0 .5549E-11 0 .3606E-10 0 .4732E-10 0 .4201E-10 0 .2484E-10	-0.7561E-11 -0.3579E-11 0.2576E-12 0.3179E-11 0.4603E-11 0.4315E-11	-0.6215E-11 -0.5558E-11 -0.3472E-11 -0.5351E-12 0.2465E-11 0.4740E-11 0.5681E-11 0.5009E-11
0.2000E 04 0.2000E 04 0.2000E 04 0.2000E 04 0.2000E 04 0.2000E 04 0.2000E 04 0.2000E 04 0.2000E 04	0.2618E C1 0.3142E C1 0.3665E C1 0.4189E C1 0.4712E C1 0.5236E C1	0.5154E 02 0.3837E 02 0.2844E 02 0.2239E 02 0.1949E 02 0.1860E 02 0.1874E 02 0.1932E 02	2 -C.2100E 05 2 0.2779E 04 2 0.2663E 05	0.4968E 05 0.4318E 05 0.2539E 05 0.1052E 04 -0.2323E 05 6-0.4088E 05 -0.4711E 05 -0.4018E 05	0.9285E-03 0.6925E-03 0.3911E-03	0.2202E-C2 0.2C35E-O2 0.1707E-O2 0.1298E-O2 0.8847E-C3 0.5282E-O3 0.2609E-C3	-0.3910E-09 -0.3593E-09 -0.2580E-09 -0.2273E-09 -0.1613E-09 -0.1078E-09 -0.6906E-10	0.2000E-10 0.2054E-10	-0.2244E-11 -0.1812E-12 0.1408E-11 0.2227E-11 0.2161E-11 0.1301E-11 -0.7430E-13 -0.1562E-11	-0.3858E-11 -0.3370E-11 -0.2213E-11 -0.6393E-12 0.9661E-12 0.2203E-11 0.2757E-11 0.2480E-11

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G.2400E 04 0.1C47E C1 0.4551E C2 0.3340E 05 0.4220E 05 0.2009E-03 0.1332E-02 -C.2C11E-09 -0.3526E-10 -0.2542E-11 -0.3238E-11
0.24C0E 04 0.1571E C1 0.3914E C2 0.1067E 05 0.4432E 05 0.5674E-03 0.1793E-C2 -0.300EE-09 -0.8267E-10 -0.1388E-11 -0.2779E-11
0.2400E 04 0.2618E 01 0.2292E 02 -C.2847E 05 0.2300E 05 0.3229E-03 0.1527E-02 -0.2623E-09 -0.4627E-10 0.7733E-12 -0.1585E-11
G.240UE 04 0.3142E 01 0.1769E 02 -C.3543E 05 0.2522E 04 0.1464E-03 0.1228E-02 -C.2135E-09 -0.2189E-10 0.1284E-11 -0.6098E-12
0.24CUE 04 0.3665E C1 0.1465E C2 -0.3119E 05 -0.1786E 05 0.1580E-04 0.9130E-C3 -0.1641E-09 -0.3273E-11 0.1278E-11 0.3754E-12
0.2400E 04 0.4189E C1 0.1319E 02 -0.1728E 05 -0.3272E 05 -0.5544E-04 0.6297E-C3 -0.1213E-09 0.7337E-11 0.8048E-12 0.1144E-11
0.240uE 04 0.5236E C1 0.1269E 02 0.2184E 05 -0.3253E 05 -0.5736E-04 0.2537E-C3 -0.6468E-10 0.6913E-11 -0.8352E-12 0.1395E-11
C.24C0E U4 0.5759E C1 0.1291E 02 C.3603E 05 -0.1753E 05 -0.2064E-04 0.1694E-C3 -C.45E3E-10 -0.5192E-13 -0.1519E-11 0.8233E-12
0.2800E 04 0.1571E C1 0.3C66E C2 C.5584E 04 0.4140E C5 0.2811E-03 0.1402E-02 -C.2261E-09 -0.4727E-10 -0.7877E-12 -0.2191E-11
0.2800E 04 0.2094E 01 0.2514E 02 -0.9490E 04 0.3503E 05 0.3362E-03 0.1493E-02 -0.2489E-09 -0.5345E-10 -0.7547E-13 -0.1761E-11
0.2800E 04 0.3142E 01 0.1518E 02 -0.3000E 05 0.3748E 04 0.1307E-03 0.1147E-02 -0.1977E-09 -0.2293E-10 0.8498E-12 -0.5425E-12
0.286Ut 04 0.4189E C1 0.1069E 02 -0.1487E C5 -0.2686E 05 -0.2471E-04 0.6698E-C3 -0.1256E-09 0.8259E-12 0.5646E-12 0.6422E-12
G.2800E 04 0.4712E 01 G.9881E G1 G.1642E C4 -0.3165E 05 -0.4638E-04 0.48C3E-C3 -C.9726E-10 0.4440E-11 0.7345E-13 0.9077E-12
0.2800E 04 0.5236E 01 0.9556E 01 0.1825E 05 -0.2710E 05 -0.4009E-04 0.3431E-03 -0.7609E-10 0.3382E-11 -0.4710E-12 0.8614E-12
0.2860E 04 0.5759E C1 0.9480E C1 0.3026E 05 -0.1450E 05 -0.1754E-04 0.2587E-03 -0.6162E-10 -0.7144E-12 -0.9097E-12 0.5235E-12
0.3000E 04 0.2094E 01 0.2301E 02 -0.8822E 04 0.3394E 05 0.2680E-03 0.1377E-02 -0.2297E-09 -0.4227E-10 -0.1552E-13 -0.1559E-11
0.30C0E 04 0.2618E C1 0.1820E 02 -0.2222E 05 0.2110E 05 0.2132E-03 0.1292E-02 -0.2193E-09 -0.3373E-10 0.4567E-12 -0.1073E-11
0.3u0uE 04 0.31+2E C1 0.1427E 02 -0.2797E 05 0.4301E 04 0.1195E-03 0.1107E-C2 -0.1513E-09 -0.2001E-10 0.7223E-12 -0.5073E-12
C.3000t C4 0.3665E C1 0.1156E 02 -0.2484t 05 -0.1232E 05 0.3662E-04 0.8885E-C3 -0.1580E-09 -0.7732E-11 0.7276E-12 0.5127E-13
         0.4189E C1 0.9925E C1 -C.14C1E 05 -0.2449E 05 -0.1649E-04 0.6790E-C3 -C.1264E-09 0.3718E-12 0.4906E-12 0.4917E-12
        0.4712E C1 0.9041E 01 0.1318E 04 -0.2907E 05 -0.3812E-04 0.5033E-03 -0.9999E-10 0.3729E-11 0.8968E-13 0.7217E-12
         0.3000E 04 0.5759E C1 0.8443E 01 0.2789E 05 -0.1331E 05 -0.1714E-04 0.2891E-03 -0.6569E-10 -0.3071E-12 -0.7178E-12 0.4301E-12
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